

Wallerawang Ash Dam Area Annual Environmental Management Report April 2018 – March 2019

### Wallerawang Ash Dam Areas Annual Environmental Management Report

Name of Operation	Wallerawang Ash Dam Areas
Name of Operator	EnergyAustralia NSW
Development Consent / Project Approval #	07_0005
Environment Protection Licence (EPL) #	766
Water Access Licence (WAL) #	27428
Water Supply and Water Use Approval #	10CA117220
AEMR start date	1 <sup>st</sup> April 2018
AEMR end date	31 <sup>st</sup> March 2019

I, Ben Eastwood, certify that this report is a true and accurate record of the compliance status of Wallerawang Ash Dam Areas for the period 1<sup>st</sup> April 2018 to 31<sup>st</sup> March 2019 and that I am authorised to make this statement on behalf of EnergyAustralia NSW.

Note:

The Annual Review is an 'environmental audit for the purposes of section 122B (2) of the Environmental Planning and Assessment Act 1979. Section 122E provides that a person must not include false or misleading information (or provide information for inclusion in) an audit report produced to the Minister in connection with an environmental audit if the person knows that the information is false or misleading in a material respect. The maximum penalty is, in the case of a corporation, \$1 million and for an individual, \$250,000.

The Crimes Act 1900 contains other offences relating to false and misleading information: section 192G (Intention to defraud by false or misleading statement – maximum penalty 5 years' imprisonment); sections 307A, 307B and 307C (False or misleading

applications/information/documents – maximum penalty 2 years' imprisonment or \$22,000, or both).

Name of authorised reporting officer	Ben Eastwood
Title of authorised reporting officer	NSW Environment Leader
Signature of authorised reporting officer	Benttoget
Date	027.6.2019

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# **1.** Summary of compliance

The Wallerawang Ash Dam Areas consist of the Kerosene Vale Ash Repository Stage 2 and Sawyers Swamp Creek Ash Dam (SSCAD). The Wallerawang Ash Dam Area (WADA) Annual Environment Management Report (AEMR) has been prepared pursuant to Schedule 2, Condition 7.3 of the Project Approval 07\_0005. The AEMR has been prepared in accordance with the NSW Government's *Post-approval requirements for State significant mining developments Annual Review Guideline* dated October 2015.

A summary of the Wallerawang Ash Dam Area compliance achieved during the reporting period is provided in Table 1. Any non-compliance during the reporting period is briefly detailed in Table 2, with an extended review of compliance with the Conditions of Approval (CoA) presented in Appendix A.

#### Table 1: Statement of Compliance During 2018-19 Reporting Period

Were all conditions of the relevant approval(s) complied with?		
Project Approval #07_0005 NO		
Environment Protection Licence #766	YES	
Water Access Licence #27428	YES	
Water Supply Work and Water Use Approval #10CA117220	Water Use Approval YES	

#### Table 2: Details of Non-Compliance during 2018-19 Reporting Period

Relevant Approval	Condition No.	Summary of Condition	Compliance Status	Comment	Section where addressed within AEMR
PA 07_0005	2.1	Ash re-use	Low	The goal of 40% ash reuse was not achieved by 31 December 2013, as required.	Section 11
EPL 766	NA	NA	NA	NA	NA
27428	NA	NA	NA	NA	NA
10CA117220	NA	NA	NA	NA	NA

In assessing compliance with CoAs the key for compliance assessment provided in Table 3 was used, in accordance with the NSW Government's Independent Audit Guideline.

Risk Level	Colour Code	Description	
High		Non-compliance with potential for significant environmental consequences, regardless of the likelihood of occurrence.	
Medium		<ul> <li>Non-compliance with:</li> <li>Potential for serious environmental consequences, but is unlikely to occur; or</li> <li>Potential for moderate environmental consequences, but is likely to occur.</li> </ul>	
Low		<ul> <li>Non-compliance with:</li> <li>Potential for moderate environmental consequences, but is unlikely to occur; or</li> <li>Potential for low environmental consequences, but is likely to occur.</li> </ul>	
Administrative non- compliance		Only to be applied where the non-compliance does not result in any risk of environmental harm (e.g. submitting a report to government later than required under approval conditions).	
Compliant		The intent and all elements of the requirement of the regulatory approval have been complied with.	

#### **Table 3: Compliance Status Key**

An acceptable standard of environmental performance has been achieved during the reporting period as evidenced by the following:

- One non-compliance recorded during the reporting period relating to ash reuse.
- Noise from the Kerosene Vale Ash Repository site was inaudible at sensitive receivers during the reporting period.
- Air quality monitoring results relating to activities at the Wallerawang Ash Dam Area were below the Operational Environment Management Plan (OEMP) assessment criteria for depositional dust gauges located in Wallerawang and Lidsdale townships.
- There were no surface water discharge events during the reporting period.
- There were no incidents that caused or threatened material harm to the environment.
- There were no community complaints received relating to the management of the Wallerawang Ash Dam Area.

# 2. Introduction

#### 2.1 Background

The Wallerawang Ash Dam Area (WADA) includes the Kerosene Vale Ash Repository Stage 2 (KVAR) and Sawyers Swamp Creek Ash Repository. The WADA is owned and operated by EnergyAustralia NSW and is located approximately 2.5 kilometres north-east of Wallerawang Power Station and approximately 10 kilometres north-west of the city of Lithgow, which is 150 kilometres west of Sydney (Figure 1). KVAR is situated in the centre of the Sawyers Swamp Creek (SSC) catchment and receives rainfall runoff from the surrounding areas.

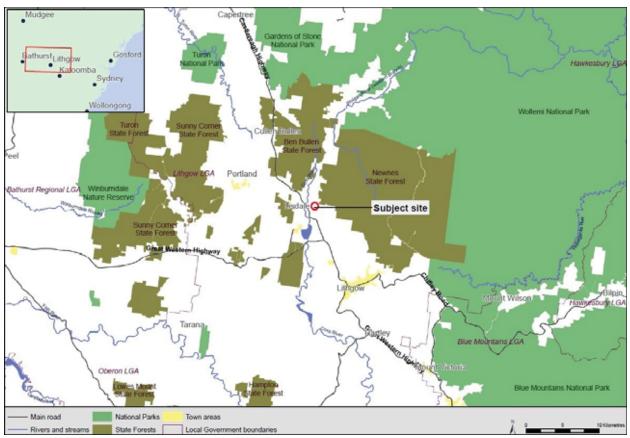


Figure 1: Regional context map

The original ash placement operations were at the Kerosene Vale Ash Dam (KVAD). The void was filled with ash transported from the Wallerawang Power Station as slurry (i.e. wet ash placement). When the KVAD was full, it was capped with a clay capping and then ash placement operations began at the Sawyers Swamp Creek Ash Dam (SSCAD), which saw wet ash placement take place from 1980 to 2003.

The need to further develop the KVAR area in order to maintain power-generation operations at Wallerawang Power Station was identified in 2001. The existing wet ash storage area (i.e. SSCAD) was approaching its design capacity. The placement of dry ash at the KVAR was identified as a viable figure. The extent of both stages is outlined in Figure 2.

Conversion from wet to dry ash placement aimed to minimise environmental and social impacts potentially resulting from heavy metal accumulation. Key benefits of a dry ash handling facility included:

- The potential for ash to be beneficially reused in its dry form;
- An approximate 80% decrease in the water required to transport ash;
- Discharges to the Coxs River are decreased in the long term;
- The SSCAD can be progressively rehabilitated; and
- There would be a decreased flood risk for Kerosene Vale, Lidsdale and surrounding areas (Hyder Consulting, 2001)

In 2002, Project Approval was granted by the Minister of Planning to change from wet to dry ash-producing activities and to use the Kerosene Vale Ash Repository (KVAR) area for dry ash storage. On 26 November 2008, Project Approval was granted by the Minister of Planning for the extension of the existing KVAR area to permit the continued disposal of ash generated by the Wallerawang Power Station under Section 75J of the *Environmental Planning and Assessment Act 1979*. The KVAR Stage 1 placement works were completed and capped in February 2009. The KVAR Stage 2 placement works commenced soon after in April 2009 (Aurecon, 2011).

The original ash placement strategy, as outlined within the Operation Environmental Management Plan (OEMP) (Parsons Brinckerhoff, 2008b), was as follows:

- Stage 2A as an extension of Stage 1;
- Stage 2B to allow time for the re-alignment of Sawyer's Swamp Creek and for material to be obtained from the pine plantation area to reinforce the stabilisation berm to the north of KVAR Stage 1; and
- Stage 2C as a final ash placement area once reinforcements of a proposed stabilisation berm with creek realignment had been carried out.

Since the first AEMR was submitted in 2011, the ash placement strategy for Kerosene Vale Stage 2 Ash Repository has been updated to reflect changes from the three-stage process outlined above, to a two-staged approach. This change in strategy was in response to Centennial Coal relinquishing their right to extract coal from the areas of mining interest within the KVAR Stage 2 proposal (Figure 2).

In January 2014, Wallerawang Power Station's Unit 7 was removed from service and deregistered from the market; whilst in March 2014, Unit 8 was placed in long term storage. However, in November 2014, EnergyAustralia NSW announced that Unit 8 was to be removed from service and deregistered from the market. Wallerawang Power Station ceased energy production in April 2014 and is currently being decommissioned and dismantled.

The bulk transport and disposal of ash to the WADA subsequently ceased following the closure of the Wallerawang Power Station. The WADA is currently being managed in a care and maintenance arrangement. Small volumes of ash will be disposed when required during the demolition of the Wallerawang Power Station. Preliminary plans are being developed for the deconstruction and rehabilitation (DDR) of the entire operational facility at Wallerawang, including the ash placement areas.

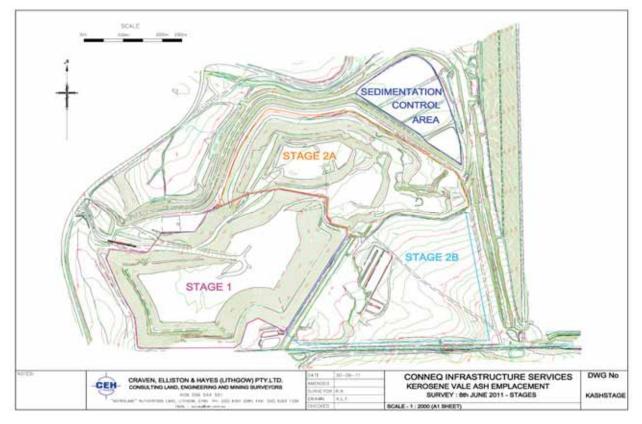


Figure 2: Revised ash placement strategy for KVAR- Stages 1, 2A and 2B

#### **2.2 Purpose of the AEMR**

This Annual Environmental Management Report (AEMR) has been prepared in order to satisfy Condition 7.3 of the Project Approval 07\_0005 (DP&I, 2008). This report covers the operations and environment and community performance of the Wallerawang Ash Dam Area from April 2018 and March 2019 (reporting period).

The AEMR has been prepared in accordance with the NSW Government's *Post-approval requirements for State significant mining developments Annual Review Guideline* dated October 2015.

#### 2.3 **Project contacts**

The contact details for the Wallerawang Ash Dam Areas (WADA) are listed in Table 4.

#### Table 4: Kerosene Vale Ash Repository Contact

Contact Person	Position	Telephone
Mr Ben Eastwood	NSW Environment Leader & KVAR Environment Representative	(02) 6354 8111

# **3.** Consents, Leases and Licences

This AEMR has been prepared to address the conditions of the project approval and the Statement of Commitments for the reporting period. The operation of the WADA project operates in accordance with the following statutory authorities (Table 5):

Approval/Lease/Licence	Issue Date	Expiry Date	Details/Comments
Project Approval 07_0005	29 Jul 2005 (Renewed 26 Nov 2008) 9 Aug 2018 (Mod 1)	26 Nov 2013	Granted by Minister for DoP, Section 75J of the EP&A Act.
Environment Protection Licence (EPL) No. 766	20 Dec 2017	20 Dec (Annual Anniversary Date)	Granted by NSW Environment Protection Authority
Water Access Licence No. 27428	01 July 2001	-	Granted by DPI Water, under the <i>Water</i> <i>Management Act 2000</i>
Water Supply Work and Water Use Approval 10CA117220	01 July 2001	30 Jun 2031	Granted by DPI Water, under the <i>Water</i> <i>Management Act 2000</i>

#### Table 5: Key Consents, Leases, Licences and Permits

On the 22 December 2017, EnergyAustralia NSW submitted an application to DPE for the modification of project approval 07\_0005 under section 75W of the Environmental Planning and Assessment Act (EP&A Act). The application sought approval for the importation of clean fill from offsite sources in NSW to be used in the capping and rehabilitation of the Wallerawang Ash Dam Area. The Operational Transport Management Plan and supporting Statement of Environmental Effects was placed on public exhibition. The Operational Transport Management Plan was approved on the 21 November 2018 in the current reporting period.

#### **3.1 Operations Environmental Management Plan**

The Operations Environmental Management Plant (OEMP) provides the framework to manage the environmental aspects associated with the operation of the WADA. The OEMP outlines the requirements associated with the project as stipulated in the relevant provisions of the Project Approval 07\_0005 administered by the NSW Department of Planning and Environment, the Environment Protection Licence 766 (EPL) administered by the NSW Environment Protection Authority (EPA), and the Statement of Commitments (SoC) presented in the Submissions Report (Parsons Brinckerhoff, 2008b).

The scope of the OEMP covers operations involving the movement and placement of ash, water and sediment pond from Wallerawang Power Station (WWPS) to the WADA. The OEMP was reviewed by EnergyAustralia NSW during the 2017-18 reporting period to ensure that it reflects the current extent of activities. The OEMP has been prepared in consultation with the EPA, WaterNSW, DPI-Water, DPI-Fisheries. The OEMP was submitted to the DPE on the 4 August 2017 and approved on 21 November 2018.

#### **3.2 Construction Environmental Management Plan**

A Construction Environmental Management Plan (CEMP) for KVAR Stage 2B was developed in consultation with EnergyAustralia NSW's Western Environment Section and approved by the DP&I in August 2011. The CEMP meets the requirements of CoA's 6.2 and 6.3, providing the framework to manage the environmental aspects associated with construction works during KVAR Stage 2B operations. The CEMP has been written to address the requirements associated with the project as stipulated in the relevant provisions of the Project Approval 07\_0005 issued by the DPE.

# 4. Operations during reporting period

Due to the closure of Wallerawang Power Station, WADA has been placed in care and maintenance.

To ensure ongoing compliance when in care and maintenance, EnergyAustralia NSW has engaged a contractor to undertake regular, ongoing maintenance activities. The contractor primarily maintains surface water management structures, water sprays for dust suppression and any other works required. There was no ash delivered or reused during the reporting period. The total ash footprint has remained the same from the previous reporting period and no additional capping or rehabilitation activities were completed. A summary of activities during the reporting period is provided in. (Table 6).

Activity	Previous reporting period	This reporting period	Next reporting period
Ash delivered to site (T)	0	0	0
Ash reused (T)	0	0	0
Total Ash Footprint (ha)	37.1	37.1	37.1
Area of repository capped (ha)	33.4	33.4	33.4

#### Table 6: Operations Summary

#### 4.1 Normal operating hours

The normal hours of operation for the Project are between 7 am and 10 pm Monday to Sunday, in accordance with Condition 2.8. Operations outside these hours are defined as abnormal or emergency operating conditions and are subject to specific requirements (Section 4.2).

No works occurred at KVAR outside the normal operating hours during the reporting period.

#### 4.2 Abnormal or emergency operating conditions

Conditions under which operations outside the normal hours of operation can occur have been specified in the Project Approval (CoA 2.10) and can be described as follows:

- Where it is required to avoid the loss of lives, property and/or to prevent environmental harm
- Where a breakdown of plant and/or equipment at the repository or the Wallerawang Power Station can affect or limit the capacity of ash storage at the power station itself outside the normal operating hours
- Where a breakdown of an ash haulage truck(s) prevents haulage during the operating hours stipulated under '*Normal Conditions'* combined with insufficient storage capacity at the Wallerawang Power Station to store ash outside of the normal operating hours
- In the event that the National Electricity Market Management Company (NEMMCO), or a person authorised by NEMMCO, directs EnergyAustralia NSW (as a licensee) under the National Electricity Rules to maintain, increase or be available to increase power generation for system security and there is insufficient ash storage capacity at the Wallerawang Power Station to allow for the ash to be stored.

Under these circumstances, EnergyAustralia NSW is required to notify the OEH, formerly DECC, and nearby sensitive receivers prior to any emergency ash haulage or placement operations, as well as the Secretary of the DPE, formerly DoP, within 1 week after the emergency operations have occurred.

No operating conditions have occurred outside the normal operating hours during the reporting period.

#### 4.3 **Construction activities**

No construction activities were carried out during the reporting period.

#### 4.4 Wallerawang DDR Works

There is a three-phase plan for the closure of the Wallerawang Power Station that involves the decommissioning, deconstruction and rehabilitation (DDR) of the site including the ash repository and SSCAD.

EnergyAustralia NSW staff met with representatives from the Department on 18 October 2017 to provide an update on the Decommissioning, Demolition and Rehabilitation (DDR) of the Wallerawang Power Station, including the closure and rehabilitation of the KVAR. It is not proposed to develop a Closure and Rehabilitation Plan for KVAR or SSCAD in isolation at this time without considering the adjacent sites. EnergyAustralia NSW will keep the Department informed of its progress regarding the development of the Closure and Rehabilitation Plan for KVAR, Sawyers Swamp Creek Ash Dam and adjacent ancillary infrastructure areas.

The NSW Environment Protection Licence (EPL 766) will continue to cover the activities associated with the Closure of Wallerawang power station and the ash placement areas. As detailed in Section 3, the EPL and Project Approval has been modified within the reporting period to enable the import of Virgin Excavated natural material (VENM) and Excavated natural material (ENM) onto the premises for land rehabilitation purposes. The VENM and ENM importation project will allow for the completion of capping and rehabilitation of the uncapped sections of KVAR and SSCAD.

Care and maintenance activities will continue to be undertaken in accordance with the Project Approval and Environmental Protection Licence. Monitoring will be undertaken to ensure compliance with relevant air and noise emission levels. The management of environmental aspects, including groundwater, surface water and landscape aspects of KVAR, will continue to be controlled and monitored to ensure regulatory compliance is achieved.

## 5. Actions required from previous AEMR review

In a letter dated 4 July 2018, the DPE stated it was generally satisfied that the 2017-18 Annual Review adequately addressed the relevant requirements of the Project Approval. There were seven actions requested by DPE, which are summarised below in Table 7.

Item	Action required from previous Annual Review	Requested by	Action taken	Where discussed in AEMR
1	<b>Dust Gauges</b> Provide clarification that only seven of the dust gauges (DDGs) are listed under the Operational management Plan (OEMP) and are used for compliance.	DPE	Dust gauges used for site monitoring as required by the OEMP are shown on Figure 3.	Section 6.4.1.2
2	<b>Dust Gauges</b> Provide further information regarding the potential influence of bushfires on DDG results and why regional bushfires may not be influencing all DDGs or provide alternative explanations (eg. Based on visual assessment at time of collection, microscopic analysis) for identified peaks.	DPE	Analysis of air quality performance using graphs is detailed in 6.4.2.2.	Section 6.4.2.2
3	<b>Figure</b> Include DG29 on Figure 3	DPE	Added DG 29 into Figure 3	Figure 3
4	Table Include a table as per Table 7 in the Post approval requirements for State significant mining development – Annual Review Guideline dated October 2015 for water take under WAL 27428	DPE	Refer to Table 12	Section 8.1.2

Table 7:	Actions	required	from	last AEMR
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2018	-	2019

Item	Action required from previous Annual Review	Requested by	Action taken	Where discussed in AEMR
5	Discussion Include in discussion against predictions in the EIS for groundwater and surface water results	DPE	The Aurecon assessment notes that due to the complexity of current and historic land use activities, including local chitter deposits, pumping and discharge regimes for the KVAD and SSCAD, it is not conclusive to directly attribute water quality impacts observed in groundwater in Bore D5 solely to a single source such as the KVAR. Aurecon has concluded KVAR is currently not having a measurable impact on surface water quality in Sawyers Swamp Creek at the surface water monitoring site (WX7).	Section 7.1 Section 7.2
6	Explanation Provide an explanation regarding the changes in active disturbances and land being prepared for rehabilitation as noted in the email dated 4 July 2018, and ensure that this is corrected in Section 4 and Table 12 of the Annual review	DPE	Rehabilitation Summary table has been included in Table 13 with the Current Status for the reporting period. Discussion has been noted in Section 8.	Section 4 Section 8 Table 13
7	Website In accordance with Condition 5.1.b of the approval, the Water Access Licence will be made a available on the following website	DPE	The Water Access Licence is available vie the EA website at: <u>https://www.energyaustralia.co</u> <u>m.au/about-us/energy-</u> <u>generation/mt-piper-power-</u> <u>station/mt-piper-and-</u> <u>wallerawang-water-data</u>	Section 9.4

# 6. Environmental management and performance

Environmental monitoring for the WADA and specifically for the KVAR Stage 2 operations is designed to comply with the regulatory requirements specified in Section 3 of this AEMR, and also to provide an ongoing analysis of the condition of the environment surrounding the site. Environmental monitoring is performed as part of the monitoring program at the sites indicated shown in Figure 3. The results are used as indicators of the effectiveness of the environmental controls, and as guidelines for the management and maintenance of key environmental procedures.

Detailed procedures outlining the environmental monitoring responsibilities of key stakeholders and the impacts to be mitigated can be found within the individual sub-plans of the OEMP, and include:

- Operational Noise and Vibration Management Sub-Plan
- Surface Water Quality Sub-Plan
- Groundwater Management Sub-plan
- Air Quality Management Sub-plan
- Landscape and Revegetation Sub-Plan
- Waste Management Sub-plan

A summary of the environmental management measures and associated performance is provided in Table 8. Detailed discussions of the key environmental performance indicators are presented in the sections below (6.1 - 6.6, 7.1 - 7.2).

Performance against environmental monitoring and compliance requirements are provided by Lend Lease as a monthly Client Service Report and through external consultant and internal data and reports. Summaries of these reports are provided in the sections below (6.1 - 6.6, 7.1 - 7.2) and in Appendices B, C & D.

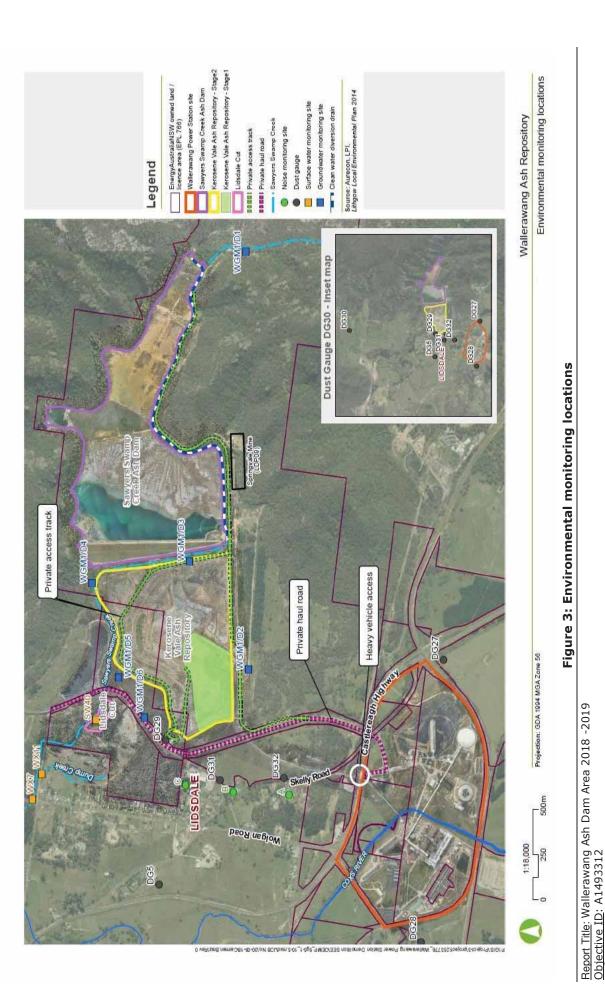
Aspect	Approval Criteria	EA Prediction	Performance during reporting period	Trends / Management Implications	Management Actions
Noise	Site 1 – Site 3 Criteria 40 dB(A) LAeq	Site 1 33 Site 2 33 Site 3 31 dB(A) LAeq	Site 1 Nil detected Site 2 Nil detected Site 3 Nil detected	NA – no operational noise generated.	Nil additional management actions required
Ecological	Minimal impacts on ecology of Sawyers Swamp Creek following its realignment.	Potential impacts associated with realignment of Sawyers Swamp Creek	Sawyers Swamp Creek was not realigned therefore no ecological monitoring is required.	NA – Sawyers Swamp Creek was not aligned.	Nil additional management actions required
Air Quality	Maximum total deposited dust 4 g/m <sup>2</sup> /month annual	Annual average of 3.5 g/m <sup>2</sup> /month deposited dust	Annual average range 0.5 to 3.5 g/m <sup>2</sup> /month deposited dust	Annual average dust levels show a slight increasing trend.	Nil additional management actions required.
Waste	Waste disposal to reflect EPL 766.	Wastes disposed of accordingly.	Nil waste disposed of at the Repository during the reporting period.	Decrease in waste disposed of at the repository.	Nil additional management actions required.
Heritage	Minimal impact on heritage values of the area.	Heritage impacts considered to be minimal and are manageable with appropriate and well- established procedures.	No additional heritage sites were identified.	No additional heritage sites have been identified throughout KVAR operation.	Nil additional management actions required.

#### **Table 8: Environmental Performance**

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Wallerawang Ash Dam Area

2018 - 2019



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#### 6.1 Ash delivery and placement

Due to the closure of Wallerawang Power Station, no ash has been placed at KVAR Stage 2 within the reporting period.

In a survey performed in February 2018 (Figure 4), the ash footprint areas were as detailed in Table 9.

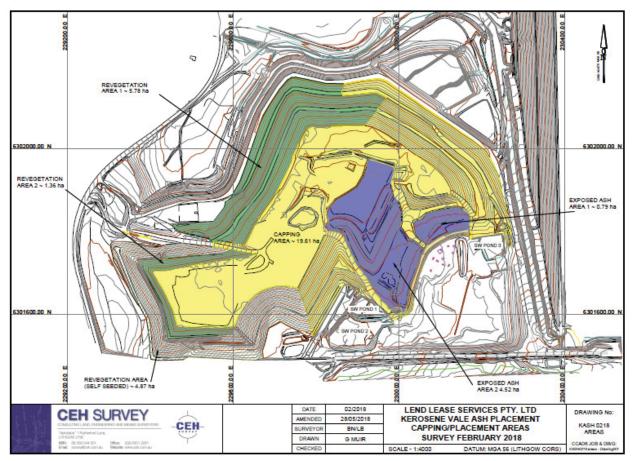


Figure 4: Area of exposed ash remaining at Kerosene Vale Ash Repository Stage 2

Ash Footprint area	Area (ha)
Exposed ash	5.3
Footprint	13.1
Batters	10.0
Laybacks	2.5
Top Level	6.2
<b>Total Ash Footprint</b>	37.1

Operations of the KVAR Stage 2 are considered to have met the following targets of the Ash Delivery and Placement Sub Plan of the OEMP. The management and mitigation measures specified in the OEMP were assessed to be compliant.

#### 6.2 **Operational Noise Monitoring**

#### 5,2.1 Environmental Management

The KVAR Stage 2 Operational Noise and Vibration Management Plan (ONVMP) has been developed in accordance with Condition 6.5 of Project Approval 07\_005 for the KVAR Stage 2 area.

The Operational Noise and Vibration Management Plan identifies measures to minimise and mitigate noise impacts on surrounding land uses from the proposed works. The level of noise generated during the proposed works program will depend on the location of the receiver, the type and duration of works and intervening topography, and existing building structures between the noise emission source and receiver.

The residential community of Lidsdale is located to the west of the private haul road and ash repository site. The following residential properties, located within 300m from the haul road, have been identified as the nearest potentially affected sensitive receivers to noise from the repository site:

Sensitive Receiver	Distance to Haulage Road (m)
60 Skelly Road	300
10 Skelly Road	270
21 Neubeck Street	145

#### Table 10: Representative noise measurement locations

During the reporting period compliance monitoring was conducted during the early morning and evening periods as per the requirements outlined in the ONVMP. The applicable operational noise criteria are outlined in the Project Approval (No. 07\_0005), the Environment Protection Licence (EPL) No. 766, the OEMP and the ONVMP. The criteria are summarised as follows:

The cumulative operational noise from the ash placement area and ash haulage activity shall not exceed a  $L_{Aeq}$  (15 minute) of 40 dBA at the nearest most affected sensitive receiver during normal operating hours as defined in condition 2.8.

This criterion applies under the following meteorological conditions:

- a) Wind speeds up to 3 m/s at 10 meters above ground; and/or
- b) Temperature inversion conditions of up to 3°C/100 m and source to receiver gradient winds of up to 2 m/s at 10 m above ground level

#### 6.2.2 Environmental Performance

Due to the closure of Wallerawang Power Station, no fly ash trucks have been hauling to the ash placement area. Minor earthworks and maintenance activities at the ash placement area were the only activities undertaken that have the potential to cause noise impacts to sensitive receivers.

Aurecon conducted operational noise monitoring for the Stage 2 KVAR located in Wallerawang NSW. The noise measurements were carried out at the three affected sensitive receivers' locations on Sunday 17 June 2018 and Monday 18 June 2018 plus Sunday 28 October 2018 and Monday 29 October 2018, in the early morning and evening in accordance with the KVAR Stage 2 ONVMP. The primary contributor to the background and ambient noise levels at all measurement locations was the traffic noise on the nearby public roads. Aurecon has determined Stage 2 KVAR operations is compliant with the Conditions of Approval.

Based on site observations and information reviewed, potential noise impacts from the operation and maintenance of the KVAR Stage 2 are considered to have been effectively mitigated and managed. There were no noise complaints received for the KVAR during the reporting period.

#### §.2.3 Reportable Incidents

No reportable incidents have been recorded against operational noise for the reporting period.

#### 5.2.4 Further Improvements

There were no exceedances of the operational noise criteria during the reporting period, as such there are no further improvements required.

EA will review the scope of the noise monitoring assessment commensurate with the level of activity while the site is in care and maintenance. Any review will be undertaken to ensure compliance with the Project Approval.

#### 6.3 Ecological Monitoring

EnergyAustralia NSW has determined that there is no longer any need to realign SSC. Therefore, ecological monitoring as required under CoA 3.7 is not required.

#### 6.4 Air Quality Monitoring

#### 5,4.1 Environmental Management

The Site Management Plan (Lend Lease, 2012) for KVAR Stage 2 operations contains an Implementation Strategy in accordance with the Air Quality Monitoring Program, which is outlined in the OEMP. The strategy includes specific site management pertaining to the transport and emplacement of ash, managing dust within the ash repository using an extensive sprinkler system and water cart applications, and continuous monitoring for dust/airborne particulates.

Dust management at KVAR is included in the responsibilities of all activities, including:

- Wash-down of security roadways, haul road/s and vehicle access roads;
- Use of perimeter sprays at the ash placement area;
- Mobile sprinkler system;
- Ash placement operations;
- Final and temporary capping of ash; and
- General maintenance of the ash placement area (Lend Lease, 2012).

#### 6.4.1.1 Dust suppression – KVAR sprinkler system

Water application (measured in sprinkler hours) is based on wind velocity, humidity and temperature. The water used for dust suppression in KVAR is sourced from the Sawyer's Swamp Creek Ash Dam return water system. This maximises the recycling of water for dust suppression, no additional clean water is used in this application.

The updated Repository Management Plan (Lend Lease, 2012) provides a guide for sprinkler hours at an optimum of 4 hours per day during low evaporation at less than 3 mm per day to ensure that a target of 5 mm by irrigation application is not exceeded (Table 11).

Water use guidelines	Water use guidelines
>25° >20km/hr (10hrs/day)	15° <20km/hr (<4 hours/day)
15-24° <20km/hr (8 hrs/day)	
15° <20km/hr (4 hours/day)	
Evaporation 3-7 mm per	Evaporation < 3 mm per
day	day
Oct, Nov, Dec, Jan, Feb, Mar,	April, May, June, July, Aug, Sept

 Table 11: Guide for sprinkler hours

#### 5.4,1.2 Dust deposition monitoring

Air quality is monitored at the seven depositional dust gauges listed within the OEMP and results are reviewed to ensure compliance with the Project Approval conditions relating to air quality. These gauges are situated close to residential areas outside of the WADA (Figure 3). Data collection commenced in March 2009, with results recorded on a monthly basis with colour and textural observations. Data from these gauges provide an indicative assessment of potential air quality impacts from WADA. It should be noted that the levels at these locations includes dust from all land use practices in the local area and not only from WADA.

#### 6.4.2 Environmental Performance

#### 6.4.2.1 Dust suppression – KVAR sprinkler system

Figure 5 reflects the relationship between sprinkler application and evaporation to identify that the target or maximum application rates for irrigation at 5 mm / day was achieved for the majority of the reporting period. Net irrigation was calculated by subtracting the daily evaporation from the daily sprinkler irrigation.

Sprinkler application rates did reach above the maximum target between July 2018 and August 2018. These irrigation rates track with high evaporation rates resulted in a net irrigation rate below the maximum application rate for irrigation.

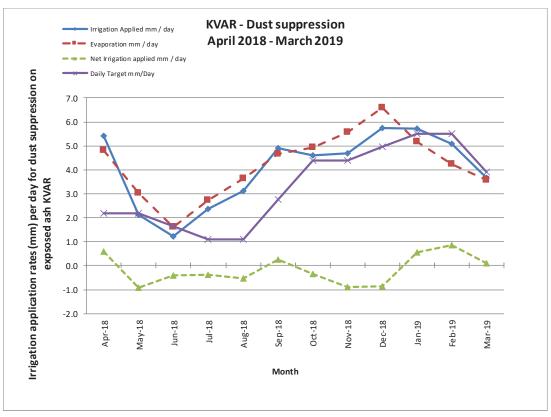


Figure 5: Efficacy of irrigation operations April 2018– March 2019

#### 5.4.2.2 Dust deposition monitoring

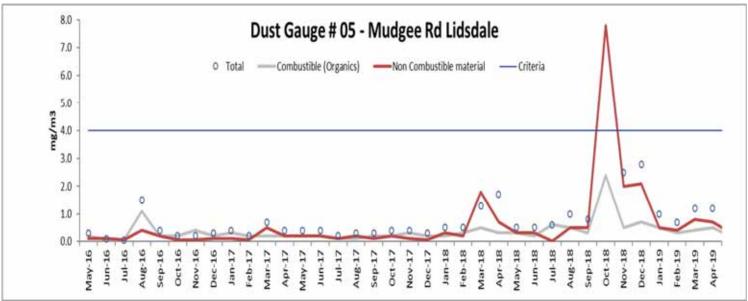
Dust gauge data from the 2018-19 reporting period of KVAR Stage 2 operations confirm that air quality emissions have complied with compliance criteria. No additional air quality control measures have been implemented beyond the existing effective practices.

Annual average depositional dust data for each of the seven OEMP dust deposition gauges are presented over the previous three-year period is presented in Figure 6 to Figure 12.

In examination of the historical data indicates a slight decrease in the depositional dust concentrations at the KVAR during the period April 2016 to Mar 2017, with an increase during the current reporting period. Operations at Wallerawang and in turn Kerosene Vale Ash Repository, ceased in April 2014, with a reduction in depositional dust concentrations reflected during the Care and Maintenance phase (2014 onwards). Depositional dust results are shown to be considerably lower than the concentrations predicted in the Environmental Assessment (predicted annual average of  $3.5 \text{ g/m}^2/\text{month}$  deposited dust).

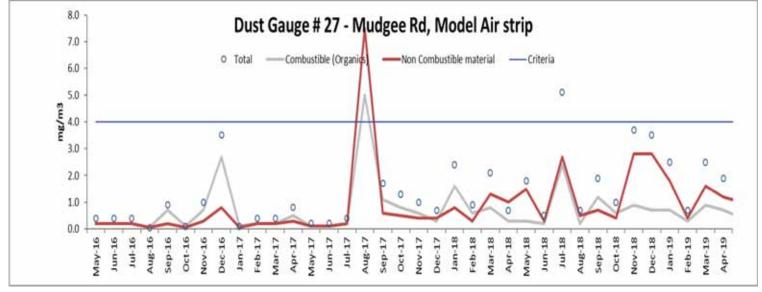
Historical high depositional dust gauge readings have generally been isolated events and are often associated with elevated combustible material which indicates possible insect activity or other similar type interference. Elevated results typically occur over the warmer months. It is possible that hazard reduction burns, and state-wide dust events may influence these results as well. The WADA is in care and maintenance with minimal activity and vehicle movements. There is no ongoing trend that indicates the WADA is impacting air quality in the local area.

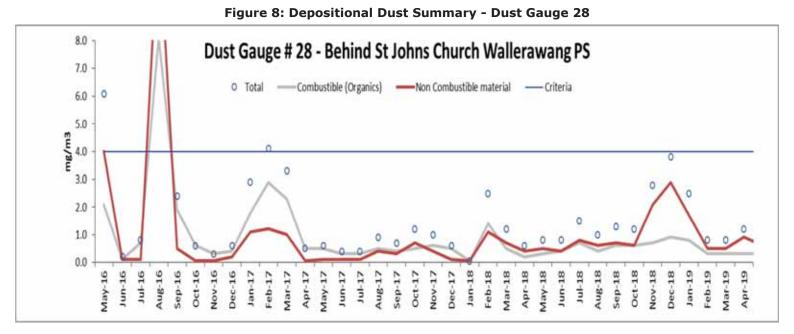
The peak observed in dust residue in Dust Gauge 5 (DG5) in October 2018 (Figure 6) was not related to works at WADA. There were no activities being carried out at the time and the predominant wind direction for December was from the south-west towards the WADA. There was a known state-wide dust storm experienced in October 2018 (OEH, 2018) which may have contributed to an elevated reading. It should be noted that there is an elevated peak in combustible material which indicates there may have been increased insect activity at the gauge which would have contaminated the result. Other contributions may be attributed to known state wide dust storms during October 2018 - December 2018. The elevated and isolated result for October 2018 at DG5 is not considered to be representative sample of emissions from WADA. There is no ongoing trend that reflects a degradation of air quality that can be attributed to WADA. The elevated result in October 2018 – December 2018 is an isolated occurrence, which is not typical for or considered representative for this site.



#### Figure 6: Depositional Dust Summary - Dust Gauge 5

Figure 7: Depositional Dust Summary - Dust Gauge 27





The elevated level of combustable material recorded at DG29 in October 2018 is not attributable to activities at WADA as air quality emmissions from WADA are non-combustable material. This is reflective of either increased insect activity or additional plant related material that has found its way into the gauge. This is typical of the external influences which can influence depositional dust gauge results.

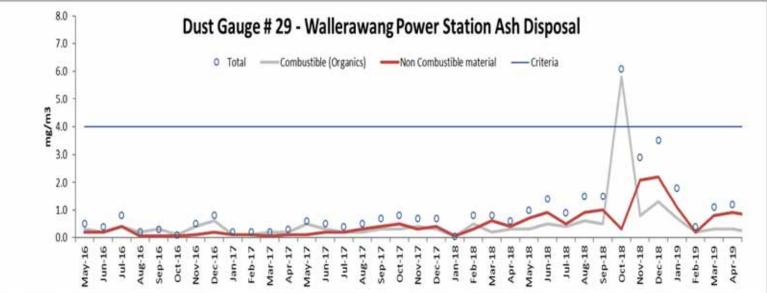


Figure 9: Depositional Dust Summary - Dust Gauge 29

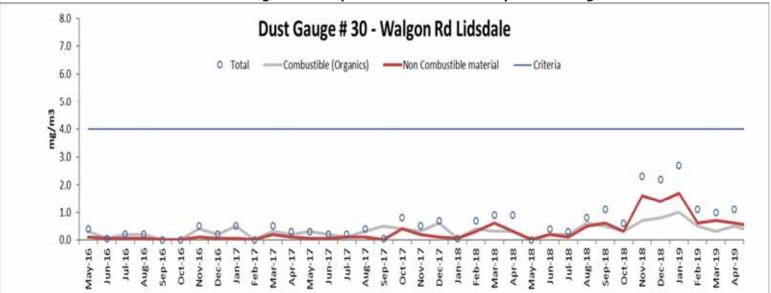
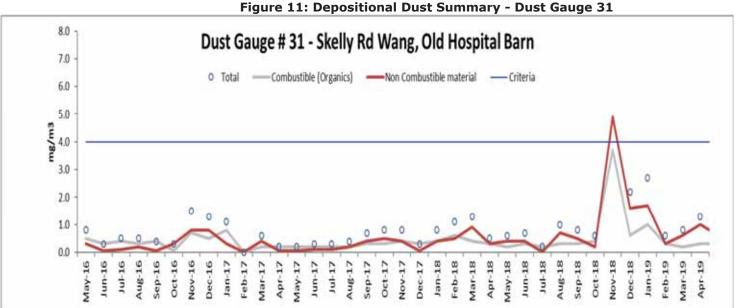
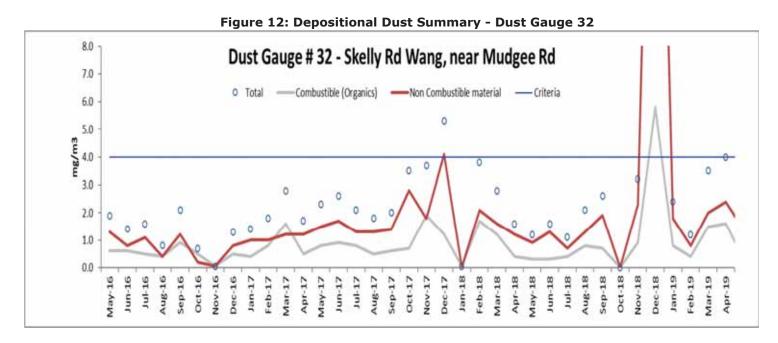


Figure 10: Depositional Dust Summary - Dust Gauge 30

The peak observed in Dust Gauge 31 (Figure 11) in December has elevated combustible and non-combustible material. This is very uncharacteristic for this gauge as elevated levels above 4.0 mg/m3 have not occurred at this site in the past three years. The dominant wind direction in December 2018 was from the south west towards the WADA indicating that the elevated result is from an external source. There is a strong correlation between the increased combustible and non-combustible material indicating that the result was potentially influenced by insect activity or another external factor. The contribution of air quality emissions by WADA is discussed in detail below.





The peak observed in Dust Gauge 32 in December 2018 is unusual for this location and has concentrations well above any other gauge recorded for this month. The highly elevated result is indicative of the result being directly contaminated by a very localised source. The January result is not consistent with previous years. There is a strong correlation with increase combustible and non-combustible material which suggests the gauge was influenced by something other than the WADA.

The elevated results recorded between October 2018 to January 2019 do not appear to relate to activities at the WADA for the following reasons:

- There were no activities occurring at WADA in regard to construction activity or ash transport as the site is currently in care and maintenance;
- The dust suppression systems were operating and functional during December;
- There were no community complaints of visible dust leaving the site during the month;
- There was a general increase in depositional dust across all gauges for October 2018 through to January 2019;
- The predominant wind direction during the summer months was from the South West. This indicates that the sources of the peaks are unlikely to be attributed to WADA.
- There were state wide dust storms observed during the summer months as reported by the Office of Environment and Heritage (OEH 2018/19);
- The samples collected during this period reported having fine brown dust, insects, organic matter and coarse brown dust;
- The peaks are isolated, one-off events for individual gauges;
- There is no obvious trend from the monitoring network that indicates regional air quality is diminishing because of WADA.

Having reviewed available information and data and from site inspections, the requirements for air quality emissions and management as described under the OEMP were compliant through the 2018-19 reporting period. These results confirm that the control measures in place at the WADA are effective in controlling air emissions.

#### **6.4.3** Reportable Incidents

No reportable incidents have been received in relation to air quality management for the reporting period.

#### هَ، الله Further Improvements

Investigate if methods are available to minimise bugs infestation and vandalism (e.g. stealing or breaking) to dust gauge bottles, particularly gauges located near residential areas.

#### 6.5 Waste Management

#### 5,5,1 Environmental Management

Waste disposal practices at the WADA are managed in accordance with Environmental Protection Licence 766 and the Waste Management Sub-Plan (OEMP Section 6.9). Waste materials are assessed, classified, managed and disposed of in accordance with Environmental Guidelines: Assessment, Classification and Management of Liquid and Non-Liquid Wastes (EPA, 1999).

EnergyAustralia NSW and associated contractors are not to cause, permit or allow any waste generated outside the ash repository to be received at the ash repository for storage, treatment, processing, reprocessing or disposal, including no wastes other than those as stated on the licence approval to be kept on the site. Waste generated by site personnel shall (including maintenance wastes such as oils and greases) are collected on a regular basis to be recycled or disposed of to an appropriate facility.

Staff and contractors involved in the WADA are made aware of the waste management procedures as outlined in the OEMP sub-plan. Waste-related documents and records reflect adherence to these protocols, thereby providing the foundations for a transparent approach to waste management. The OEMP provides further guidance and detail on specific waste streams and applicable management measures (OEMP Section 6.9).

#### 5.2 Environmental Performance

Nil wastes were placed at the Kerosene Vale Ash Repository during the reporting period. The activities at the WADA were deemed to have met the OEMP targets for waste management for the 2018-19 year. In addition, no non-conformances were identified and the OEMP requirements with respect to waste management were found to be complied with.

#### S.S. Reportable Incidents

No reportable incidents have been recorded against waste management for the reporting period.

#### 5.5.4 Further Improvements

No further improvements have been identified for the next reporting period.

#### 6.6 Heritage Management

#### 5,6.1 Environmental Management

The OEMP provides guidance surrounding the management methods required to comply with CoA's 2.37-2.38 regarding the protection of Aboriginal and non-indigenous heritage sites. Specifically, this is addressed in the Ash delivery and placement sub-plan.

The Environmental Assessment performed by Parsons Brinckerhoff (2008a) for KVAR Stage 2 included a preliminary archaeology and heritage assessment. The assessment concluded that the KVAR Stage 2 works pose no threat to the Aboriginal archaeological or heritage values and would not result in any further impact on Aboriginal archaeological potential. Based on these findings, the following statements of commitment, in regards to heritage sites, were made:

- Disturbance to the western portion of the ash repository shall be limited to reduce the potential for inadvertent disturbance of the Aboriginal heritage values of the area.
- In the event that any heritage sites or items be discovered during operation, all works likely to affect the area are to cease immediately. The EnergyAustralia NSW Environmental representative is to be notified immediately and relevant stakeholders including the OEH Regional Archaeologist, the Bathurst Local Aboriginal Land Council, or the NSW Heritage Office, so that an appropriate course of action can be determined.

All construction and earthworks personnel are informed on their obligations in respect of the protection of Aboriginal and non-indigenous heritage sites and items as part of the site induction.

#### 6.6.2 Environmental Performance

No known Aboriginal and non-indigenous heritage sites were impacted during the reporting period and no additional sites were discovered or identified.

#### 6.6.3 Reportable Incidents

No reportable incidents have been recorded against heritage management for the reporting period.

#### 5.5.4 Further Improvements

No further improvements have been identified for the next reporting period.

# 7. Water management

Water for operations at Kerosene Vale Ash Repository, is extracted from onsite storages or taken from the Fish River in accordance with Water Access Licence 27428 (WAL) and Water Supply Works and Water Use Approval 10CA117220. Table 12 includes details of the water taken under the WAL for operations during the previous water year (i.e. 1 July 2018 – 30 June 2019).

Water Licence #	Water Sharing Plan, source and management zone	Entitlement (ML)	Passive take /inflows (ML)	Active pumping (ML)	TOTAL
27428	Water Sharing Plan for Greater Metropolitan Region – Unregulated River Water Sources Upper Nepean and Upstream Warragamba Rivers Water Source Wywandy Management Zone	23,000	0	0	0

#### 7.1 Groundwater Monitoring

#### **7.1.1** Environmental Management

The groundwaters of the Kerosene Vale Ash Repository area are monitored regularly to determine the extent of impacts, if any, of KVAR Stage 2 operations on regional waters, and to examine the movement of water beneath the site and through the catchment.

The OEMP (Parsons Brinckerhoff, 2008b) includes a Groundwater Management Plan for KVAR and adjacent KVAD (Kerosene Vale Ash Dam). The focus of the Management Plan was to understand water quality impacts on the immediate area and the influence of regional groundwater on the stability of the KVAR Stage 2 operations, due to the placement of the site over the reclaimed ash dam.

On site, dry ash placement management has mainly involved limiting rainfall infiltration and reducing seepage from KVAD into the local groundwater. The effectiveness of these activities was demonstrated by improved water quality in the local groundwater during Stage I placement, from 2003 to 2006, before the toe drains of the Ash Dam became blocked (Aurecon, 2011).

The blocked toe drains of KVAD were cleared in February 2010, and further monitoring of groundwater levels within the Ash Dam and KVAR Stage 2 were instigated. This included subsurface investigations.

Subsurface investigations and subsurface drainage work (for seepage collection) and installation of additional water monitoring points (Figure 13) have provided for management and assessment of water levels beneath the Stage 1 repository (Golder Associates, 2013).

The groundwater monitoring network includes six regional bores – WGM1/D1 (32), WGM1/D2 (33), WGM1/D3 (34), WGM1/D4 (35), WGM1/D5 (36) and WGM1/D6 (37) (Figure 13). Additional sites sampling the local Kerosene Vale Ash Dam and Repository (KVAD/R) seepage and SSCAD, offer further information in regard to the local groundwater quality under SSCAD, KVAD and the KVAR.

Annual Environmental Management Report

Wallerawang Ash Dam Area

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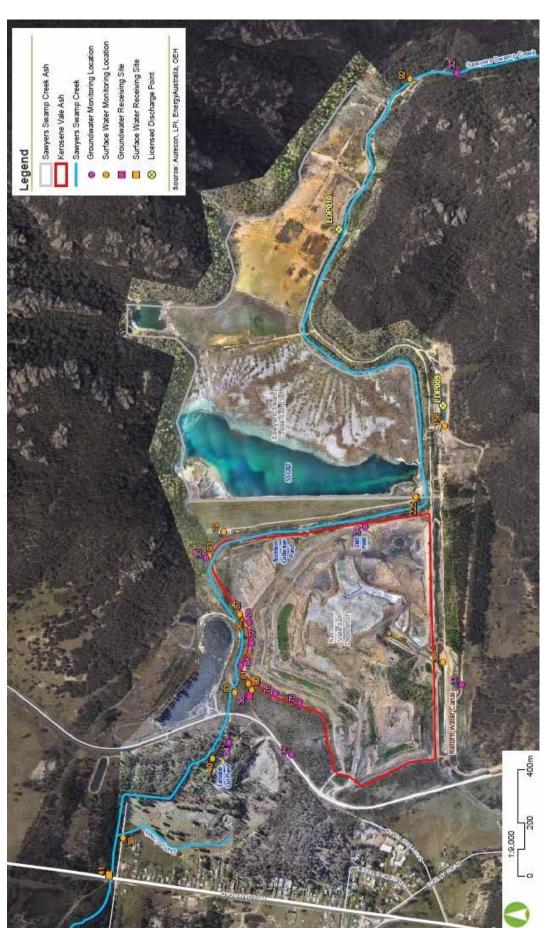


Figure 13: Surface and groundwater monitoring sites for SSCAD and KVAR

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#### 7.1.2 Environmental Performance

EnergyAustralia NSW engaged independent specialist consultants Aurecon to undertake a detailed Water Quality Assessment for the April 2018 to March 2019 reporting period for the Wallerawang Ash Dam Area (Aurecon 2019). In summary, the groundwater assessment found that there have been no significant effects of the KVAR dry ash placement area on the local groundwater aquifers during the reporting period. The Water Quality Assessment is provided in full in Appendix D.

The Aurecon report indicates the 95th percentile concentrations of water quality parameters within groundwater bore D5 (site 36) currently exceeds the selected Water Quality Goal Values (WQGVs) for Al, B, Cd, Cr, Cu, Fe, Hg, Mn, Ni, Pb and Zn (Table 4-4 Appendix D). A number of these exceedances could potentially be attributed to background levels including pH, Al, Cr, Cu, and Pb, as historically they exceeded the WQGV above the ash repository area at site WGM1/D1 (site 32). The results are reflective of water quality contributions from current and historic land use practices.

The groundwater data obtained has been graphed to identify water quality at seepage detection bore D5 (Figure 14). Time series graph for indicator parameters show that concentrations of Mn, B, and Ni decrease initially following completion of Stage 1 dry ash emplacement in the KVAR (February 2009), and again in Feb 2010 following the unblocking of the toe drains. The trend of decreasing concentrations is interrupted in July 2013, following commencement of discharge from Springvale Mine to Sawyers Swamp Creek at LDP009. It is observed that concentrations of key parameters fluctuate significantly following July 2013, with stable to rising trends for key parameters.

Due to the complexity of current and historic land use activities, including local chitter deposits, pumping and discharge regimes for the KVAD and Swayers Swamp Creek Ash Dam, it is not conclusive (based on the data set available) to directly attribute water quality impacts observed in groundwater in Bore D5 solely to a single source such as the KVAR.

The planned cessation of water discharge from Springvale Mine licenced discharge point 9 into Sawyers Swamp Creek in June 2019 will change the hydraulic characteristics of the Wallerawang Ash Dam Area. These changes will potentially be evident in the 2019/20 reporting period.

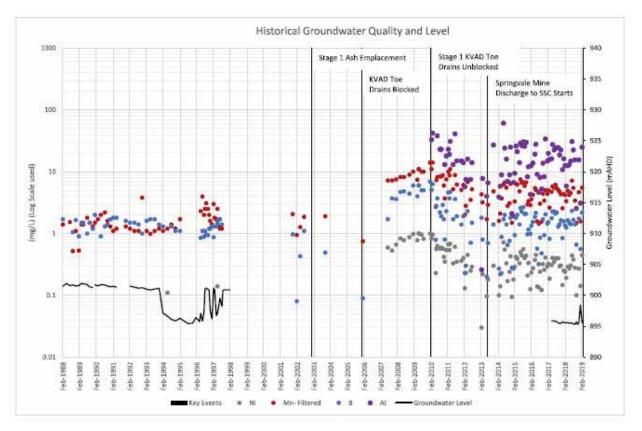


Figure 14: Historical trend of water quality within groundwater bore D5

#### 7.1.2.1 Lidsdale Cut

The Lidsdale Cut mine void pond acts as a collection basin for KVAD groundwater seepage. Groundwater seepage is directed to Lidsdale Cut through a series of drainage lines and sediment ponds. This includes rainfall infiltration through the KVAR dry ash placement and surface water runoff which is collected in pits.

EnergyAustralia NSW has been managing the water level within the Lidsdale Cut pond by pumping the level down to between 0.4 to 0.6 m above the bottom of the pond, generally in response to rainfall (Figure 15)

Previous Water Quality Assessments (Aurecon, 2015) have indicated that there have been increases in trace metal concentrations within the pond when the water level is pumped down. It is understood that water with elevated metals reports to Lidsdale cut from other sources when the water level is low. Aurecon (2015) recommended Lidsdale Cut be maintained at a higher water level to minimise trace metal release from pyrites in the adjacent coal waste/chitter.

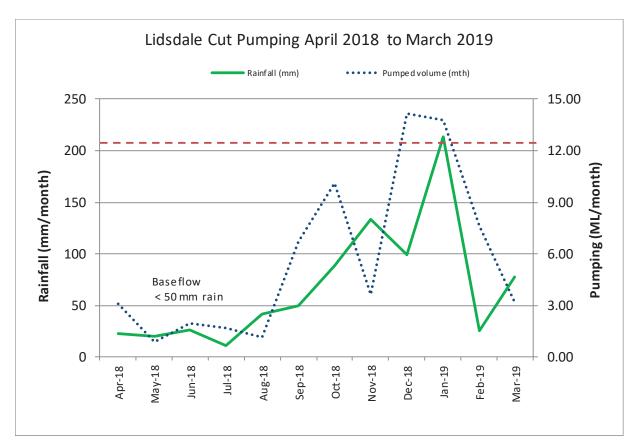


Figure 15: Rainfall compared to the amount pumped from Lidsdale Cut

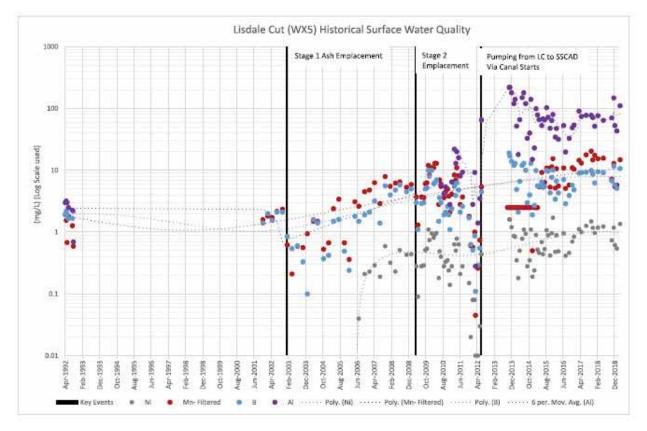


Figure 16: Historical trend for water quality within Lidsdale Cut Pond

Copyright EnergyAustralia NSW 2019. All rights reserved. Page | 31 There have been increases in trace metal concentrations within the Lidsdale Cut monitoring site. Lidsdale cut forms part of the water management system at WADA. Water in Lidsdale Cut is not discharged to the environment and is recycled onsite. (Figure 16)

With the exception of iron and fluoride, water quality concentrations within Lidsdale Cut Pond are comparable to those recorded within KVAR/D, which is indicative of the current drainage system of the KVAD/R toe drains draining to Lidsdale Cut (Appendix D Tables 4-2 and 4-4). This is supported by the highly acidic pH recorded within Lidsdale Cut samples, which are indicative of potential leachate from an acidic fly ash.

## 7.1.2 Reportable Incidents

No reportable incidents have been recorded against groundwater management for the reporting period.

## 7.1.4 Further Improvements

Further hydrogeological investigations would be required as part of the Closure & Rehabilitation of the WADA.

## 7.2 Surface Water Quality Monitoring

## 7.2.1 Environmental Management

The surface waters of Kerosene Vale are mostly comprised of runoff generated within the ash repository site. All runoff from KVAR is restricted from entering SSC and is contained for reuse for the conditioning of ash and dust suppression. The CoAs stipulate that a monitoring program must be implemented to record and observe water quality and potential impacts from repository operations on regional surface waters. This monitoring included a program following the realignment of SSC - however, as the creek has not been realigned, this aspect of monitoring is no longer necessary.

The design concept for managing surface water for the repository is outlined in the Repository Management Plan (Lend Lease, 2012), and based on reducing water pooling or ponding on exposed ash benches and eliminating flow from these areas over batters managed by controlled outflow structures.

The Operational Environment Management Plan for WADA requires sampling within SSC at four locations, this includes: two (2) on SSC, one (1) on Dump Creek to the northwest of the repository, and one (1) in SSC Ash Dam. The purpose of the surface water monitoring program is to ensure operations are not impacting on catchment surface waters, and to comply with Section 120 of the *Protection of the Environment Operations Act 1997*.

Sampling has been undertaken at Site ID numbers 38, 39, 40 and 41 since January 2003.

## 7.2.2 Environmental Performance

As stated in Section 7.1.2, Aurecon were engaged to undertake a detailed Water Quality Assessment for surface water in the KVAR Stage 2 area for the April 2018 to March 2019 reporting period (Aurecon, 2018). In summary, the assessment found that there have been no significant effects of the KVAR dry ash placement area on the local surface water receiving site during the reporting period. The Water Quality Assessment is provided in full in Appendix D.

To assess the impacts, if any, of the KVAR dry ash placement during the reporting period on the surface water receiving site at WX7, the other potential sources of water quality and trace

metal inputs to the creek need to be considered. Figure 17 shows trends in indicator parameters for WX7 since 1991 to 2018. A comparison of parameters for other relevant surface water sites located in the area surrounding KVAR for the reporting period and since 1991 are provided in Appendix D Table 4-2 and Table 5-1, respectively.

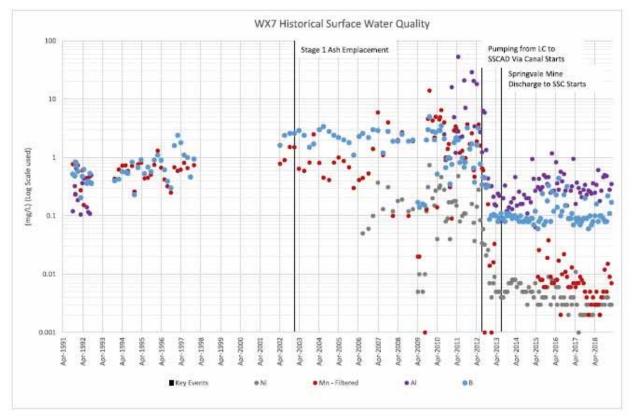


Figure 17: Historical Trend for water quality at Sawyers Swamp Creek at WX7.

The assessment of surface water quality found that:

Concentrations of overall conductivity and sulphate have gradually increased in parallel to one another until early 2010, when sulphate concentrations and other key water quality parameters began to decline (Figure 17). However, this declining trend ceased around July 2013, at which point Springvale Mine commenced discharging from their Licence Discharge Point (LDP09) dominating the water quality of WX7.

The water quality at WX7 continues to meet the local/ANZECC (2000) guideline goals for the majority of analytes, with the exception of arsenic and molybdenum (Appendix D Table 4-2). Arsenic and molybdenum were slightly above the ANSECC guideline and is consistent with the results measured at the upstream monitoring sites on SSC (Appendix D Table 4-2). As these concentrations differ to those of Kerosene Vale Ash Dam or Repository (KVAD/R) Seepage (Appendix D Table 4-2), it is likely that these are associated with other land use practices in the area and are not directly related to KVAD/R.

When compared to Dump Creek and Springvale Mine Water discharge, the water quality and trace metal concentrations in Sawyers Swamp Creek at WX7 is similar to that recorded for the Springvale Coal Mine water discharge point. Springvale Coal Mine commenced discharging water into SSC in February 2009. Approximately 20 ML of water per day is discharged by the mining operations into Sawyers Swamp Creek. The water quality in SSC being dominated by discharges from Springvale Coal Mine must be considered when assessing potential surface water impacts from KVAR against relevant ANZECC guidelines.

Based on site observations and information reviewed, potential surface water impacts from the operation of the WADA have been effectively mitigated and managed as anticipated within the Environmental Assessment (Parsons Brinckerhoff, 2008a).

Operations of the KVAR Stage 2 are considered to have met the target of zero environmental incidents relating to pollution of waters at SSC. Hydrological monitoring has been determined by EnergyAustralia NSW that it is no longer required as there is no longer any need to realign SSC. As such, hydrological monitoring as required under CoA 3.6 is not required.

## 7,2,3 Reportable Incidents

No reportable incidents have been recorded against surface water management for the reporting period.

## 7.2.4 Further Improvements

Continue monthly water quality monitoring at the EnergyAustralia NSW routine surface water monitoring sites in accordance with the approved OEMP.

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## **7.3 Erosion and Sediment Control**

## 7,3.1 Environmental Management

The management, collection and monitoring of surface water to ensure site runoff is undertaken as part of the operational and development activities of the WADA and is addressed within the surface water quality sub-plan of the OEMP. Site specific management practices are used to prevent site runoff from exposed ash surfaces from entering Sawyers Swamp Creek. Site surface water management measures include:

- Sediment and erosion controls:
  - Works in disturbed areas restricted during heavy rainfall events;
  - Operations-related earthworks not undertaken within 50m of Sawyers Swamp Creek where reasonable and feasible;
  - Cleared vegetation is mulched, chipped or re-used onsite for sediment filter fences or other uses, where appropriate.
- Development of a retention basin (or use of the existing basin) to capture site surface water runoff;
- Placement of ash with designated slopes to direct water to retention areas;
- Diversion of clean water away from disturbed areas to existing surface water drains and Sawyers Swamp Creek to provide environmental flows (Figure 18); and
- Capping and revegetating completed areas to enable the diversion of clean water to site drainage systems.

An additional clean water detention pond (SW Pond 3) was excavated in the already disturbed area of exposed soil at the north-eastern corner of KVAR Stage 2B in the 2015-16 reporting period to provide additional storage capacity (Figure 18).

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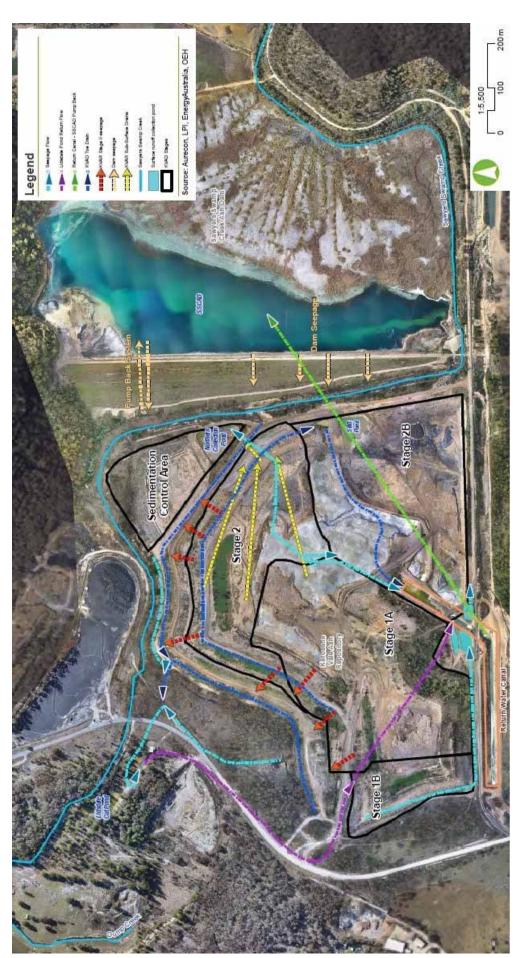


Figure 18: Existing site water drainage system

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## 7.3.2 Environmental Performance

The KVAR site (50.7 ha) is dominated by two water catchments: one reporting to the north and one reporting to the south. Both catchments have been designed to hold sediment laden water during operations and will capture clean water as per the water management plan for the final landform design. The northern catchment has a plan area of 28.5 ha and the southern catchment has a plan area of 19.7 ha, including the 7.2 ha of not-completed final excavation area for KVAR Stage 2B.

During the reporting period, rainfall runoff flows directed to the north reported into the North Holding Pond. Outflow from the North Holding Pond was managed via a pump-back system to the Sawyers Swamp Creek Ash Dam, with water from this pond also used for dust suppression irrigation and as a water cart fill point. Other flows from the North Holding Pond were directed into the collection system which reports to Lidsdale Cut and subsequently gets pumped back to the Southern water management area (now referred to as the transfer pond), for pumping back to Sawyers Swamp Creek Ash Dam.

At commencement of the ash placement operation, any water pumped to the Southern water management area (at the return water canal) was re-directed to the Wallerawang Power Station Caustic Injection Ponds. However, the need to pump back to the power station was eliminated with the clean out of the collection ponds within the Southern water management area. The current internal storage capacity in this southern area is SW Pond 1 capacity 4,766 cubic metres (4.7 ML) and SW Pond 2 capacity 6,515 cubic metre (6.5 ML).

The sediments in the Return Water Canal and collection ponds were removed during the previous reporting period, with disposal of the removed sediments at Sawyers Swamp Creek Ash Dam. The pump-back of the water from the Southern Water Management Area to the Sawyers Swamp Creek Ash Dam is now reinstated.

## 7.3.3 Reportable Incidents

No reportable incidents have been recorded against erosion and sediment control for the reporting period

## **7.3.4** Further Improvements

Implement effective sediment and erosion control measures and undertake any rehabilitation works in accordance with approved management plans.

## 8. Landscape and Revegetation

## 8.1.1 Environmental Management

The scope of landscape and revegetation environmental management is provided in the Site Repository Plan (Lend Lease, 2012) and in the Landscape and Revegetation sub-plan of the OEMP. The Landscape and Revegetation plan is based on an overall requirement to integrate the ash repository into the existing landscape.

As the repository takes shape, landscape and revegetation works occur along the batters only, with an opportunity to plant the top surface arising as part of the final site requirements. As such, revegetation occurs intermittently, constrained by seasonality and the development of the repository.

## 8.1.2 Environmental Performance

The status of rehabilitation is shown graphically in Figure 19. This provides a more accurate representation of rehabilitated areas. This primarily accounts for the changes in the land area types detailed in Table 13 when compared to areas reported in previous years.

Area Type	Previous Rep	orting Period	This Report	ting Period	Next Repor	ting Period
	Apr 2017-	Mar 2018	Apr 2018-	Mar 2019	Apr 2019-	Mar 2020
	SSCAD*	KVAR	SSCAD	KVAR	SSCAD	KVAR
Total Footprint	0.0	50.7	79.7	50.7	79.7	50.7
Total Active Disturbance	0.0	37.7	79.7	43.7	79.7	43.7
Land Being prepared for rehabilitation	0.0	33.9	22.1	40.3	22.1	40.3
Land under active rehabilitation	0.0	12.0	0.0	7.0	0.0	7.0
Completed rehabilitation	0.0	0.0	0.0	0.0	0.0	0.0

\*SSCAD was included following modification of Project Approval in November 2018

Approximately 7.0 ha have had topsoil applied and have been seeded and is actively growing. and is considered to be land under active rehabilitation Table 13 and Figure 19. Approximately 5 ha of previously rehabilitated land has been disturbed to accommodate changes to the final landform dur to the cessation of power generation at the Wallerawang Power Station.

Additionally, 3.4 ha require remedial soil cover of between 1-2 m placement to reach final form and grade and a further 10.1 ha requires a dress soil cover of approximately 0.5 - 1 m before topsoil can be applied for revegetation.

2018 - 2019



Figure 19: Current status of rehabilitation at Kerosene Vale Ash Repository

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Report Title: Wallerawang Ash Dam Area 2018 -2019 Objective ID: A1493312 Landscaping and revegetation at the KVAR for the 2018-19 reporting period has been limited to maintaining the previous planting and weed management for blackberry, thistle and pampas grass colonisation. Successful spraying campaign was completed on February 2019.



Plate 1: Kerosene Vale Ash Repository Stage 1 rehabilitation works [view east] (planted August 2014, photo taken 18 June 2019)

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Plate 2: Kerosene Vale Ash Repository Stage 1 rehabilitation works (planted August 2014, photo taken 18 June 2019)

Annual Environmental Management Report Wallerawang Ash Dam Area 2018 - 2019

The Department of Planning and Environment granted Modification 1 to Project Approval 07\_0005 in August 2018 for the import of capping material from areas outside of the Lithgow local government area to the Wallerawang Ash Dam Area. Capping material to be used for this will be sourced from various locations across NSW and will comprise virgin excavated natural material (VENM) and excavated natural material (ENM).



Plate 3: Excavated area of KVAR Stage 2B requires a reinstated soil profile.

The site requires soil placement within a 'capping and rehabilitation program' to cover a plan area of 20.7 ha (excluding the exposed ash area that is not capped and water management areas). The amount of capping material required is estimated to be in the order of 207,000 m3.

Final rehabilitation progress is subject to decisions about the water management design (including management of acidic groundwater pumped-back from Lidsdale Cut); the potential for accessing the ash for manufacturing; the availability and access to engineering fill, topsoil and the organic amendments needed to complete the planting works.

As indicated in Table 14, the majority of the OEMP requirements with respect to landscaping/revegetation were found to be satisfactory or not applicable as ash has yet to reach the design RL (940 m AHD). However, the interim landscaping/revegetation activities undertaken are considered to be in line with the relevant OEMP target, given the project's progress to date.

Performance	Completion Criteria*	Current Status
Indicator		(Reporting Period)
Visual impact	Measures to reduce the visual impact implemented as soon as practical.	Satisfactory – Batters located closest to residents have been revegetated.
	Ash Placement will be concentrated on the Eastern face of the KVAR Stage 2 ash repository in order to shield the residents from future ash placement activities.	Not Applicable – Ash placement no longer performed due to decommissioning of Wallerawang Power Station.
Capping	Ash to be capped to a depth of 0.75 m and contour ripped to preclude soil movement during rainfall or other erosion events.	<b>Satisfactory</b> – No soil loss or erosion identified in capped areas.
	Capping shall be conditioned to facilitate revegetation, which may include the use of cover crop grasses.	<b>Satisfactory</b> – Virgin Excavated Natural Material (VENM) or Excavated Natural Material (ENM) used for capping and conditioned using a mix of oats and rye-corn.
Revegetation	Develop a broad acre planting strategy on slopes at a 1 to 4 ratio.	<b>Satisfactory</b> – As detailed in the Repository Management Plan (Lend Lease, 2012).
	A developed revegetation procedure in place and implemented.	<b>Satisfactory</b> Procedure detailed in the Repository Management Plan (Lend Lease, 2012).
	Grass cover revegetation to include perennial grasses.	Satisfactory – Perennial grasses planted include Couch, Phalaris and Poa.
	Planting of shrubs and trees undertaken using tube stock of local provenance tree species to be performed after establishment of perennial grasses.	Satisfactory – Red Stringy Bark, Narrow-leaved Peppermint, Western Scribbly Gum, Silver Wattle and Red Stem Wattle tube stock planted in August 2014.
	Plant establishment (trees and shrubs) to minimise soil loss and erosion.	<b>Satisfactory</b> – No soil loss or erosion identified in revegetated areas.
Irrigation	Irrigation undertaken at establishment and as required thereafter.	<b>Satisfactory</b> – Irrigation performed through the use of water cart sprays and sprinklers already installed on and around Kerosene Vale Ash Repository.
Animal Control	Threats to vegetation such as grazing by animals managed accordingly.	Satisfactory – No evidence of animal grazing on revegetated areas.
Rehabilitation	All new batters rehabilitated as soon as practicable.	Not Applicable – No new batters have been developed.
	All areas of ash placement that have reached RL 940 m to be rehabilitated or in the process of rehabilitation as per revegetation plan.	<b>Ongoing</b> - 13.5 ha for require remedial soil cover or a dress soil cover, prior to planting. Stage 2 is 6.1 ha require remedial soil cover
* Completion Criteria	taken from the OEMP Landscape and Re-vegetat	ion Plan

### **Table 14: Rehabilitation Status Summary**

Annual Environmental Management Report Wallerawang Ash Dam Area 2018 - 2019

### **8.1.3** Reportable Incidents

No reportable incidents have been recorded against landscape and revegetation management for the reporting period.

### **8.1.4** Further Improvements

Progress development of the closure and rehabilitation management plan for KVAR. Control the spread of invasive weed species including blackberry and pampas grass.

## 9. Community

## 9.1 **Community Engagement**

During the reporting period Community Reference Group meetings were held on 30 July 2018, 2 October 2018, 3 December 2018 and 25 February 2019. The Community Consultative Committee comprises representatives from the local community and EnergyAustralia NSW. The Committee meets on a quarterly basis to discuss matters relating to operations at Mt Piper and Wallerawang Power Stations, including activities at the ash repositories. The Community Consultative Committee minutes are made publicly available via the Mt Piper and Wallerawang Community page on the Company's website <u>www.energyaustralia.com.au</u>.

## 9.2 Community Contributions

Wallerawang Power Station and the associated Kerosene Vale Ash Repository has contributed to the economy of the district and State through the purchase of materials and services from local and regional suppliers, and by direct and indirect employment. EnergyAustralia NSW continues to support a number of community groups and organisations through in-kind support and financial sponsorship programs. During the reporting period, EnergyAustralia NSW had the opportunity to support up to 60 different community organisations and events during the reporting period. A comprehensive list of these organisations and events are included in Appendix F.

## 9.3 Community complaints

No Complaints were received in the reporting period.

EnergyAustralia NSW maintains a 24-hour hotline for the public to report incidents, complaints or enquiries with contact details available on the EnergyAustralia website. EnergyAustralia NSW records the details of all complaints received in a Complaints Register.

The Contract Administrator, Site Manager and the Environment Representative ensure that the community relations protocols are communicated to all project personnel involved in the complaints process and that appropriate training covering the protocols is established in site inductions.

The key elements of the on-site complaints' management protocol include:

- All persons wishing to register a complaint to operations personnel will be politely directed to the Support Services Leader, in line with EnergyAustralia NSW's existing complaints procedure.
- The Support Services Leader will deal with the complaint and take down particulars of the complaint as per the criteria listed on the complaints register. Action will then be taken to resolve the issue whilst ensuring that all correspondence relating to the issue is documented. All attempts will be made to resolve the issue on the same day, however if this is not possible, the complainant will be updated regularly on the progress of the matter where practical.

## 9.4 Website Information

A project specific webpage has been developed to keep the broader community up to date with recent activities at the Kerosene Vale Ash Repository in accordance with Schedule 5, Condition 5.1 of the Project's Conditions of Approval. Copies of the following documents are made publicly available on the EnergyAustralia website:

https://www.energyaustralia.com.au/about-us/energy-generation/wallerawang-powerstation-closure/kerosene-vale-ash-repository

- Environment Assessment
- Project Approval 07\_0005
- Construction Environment Management Plan
- Operation Environmental Management Plan
- Annual Environmental Management Reports

https://www.energyaustralia.com.au/about-us/energy-generation/wallerawang-powerstation-closure/wallerawang-epa-reports

- Environment Protection Licence 766
- Pollution Incident Response Management Plan

https://www.energyaustralia.com.au/about-us/energy-generation/mt-piper-powerstation/mt-piper-and-wallerawang-community

Community Consultative Committee Minutes

https://www.energyaustralia.com.au/about-us/energy-generation/mt-piper-powerstation/mt-piper-and-wallerawang-water-data

- Water Access Licence
- Water Supply Work and Water Use Approval

## **10. Independent Audit**

There was no independent environmental audit undertaken during the reporting period. There is no requirement under Project Approval 07\_0005 to perform an independent audit on the KVAR Stage 2 activities. Despite this, KVAR Stage 2 is subject to EnergyAustralia NSW's internal environmental audit and inspection schedule.

## **10.1** Internal Environmental Audits & Inspections

Environmental audits and inspections are undertaken by the Environment representative and Site Manager, in accordance with the program outlined in Table 15. The inspections assist to identify areas where improvements to the environmental performance of the KVAR Stage 2 activities can be achieved. Further detail is provided in section 3.7 of the OEMP. Reports from inspections undertaken are submitted to and reviewed by EnergyAustralia NSW monthly, with all areas discussed in detail during regular client/contractor meetings.

Potential impact	Locations	Technique	Frequency	Reporting	Responsibility
General	All KVAR Stage 2	Site	Daily	Daily site environmental checklists	Contractor
Environmental Impacts	operational areas	environmental inspections	Monthly	Monthly site environmental checklists	Environmental representative

### Table 15: Environmental inspection program

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## **11. Incidents and non-compliances during the reporting period**

As the WADA is in care and maintenance there is limited vehicle and people movements at the site. As such the potential for environmental incidents and non-compliances is substantially reduced.

During the 2018-19 reporting period, there was one instance of non-compliance in relation the project approval 07\_005 Condition 2.1. The goal of 40% ash reuse was not achieved by 31st December 2013, with a total of only 0.32% ash reuse occurring from Wallerawang Power Station by the end of 2013. In March 2014, when it was announced that Wallerawang Power Station was being put out of service, the ash reuse from Wallerawang had remained at 0.32%.

Ash utilisation has been an ongoing program for the power station. Since then, more research and development of products and potential markets have been performed by external third parties. Generally, the major limitation to further market development is a lack of rail, building and industrial infrastructure, particularly for the storage of ash at Wallerawang. Despite this EnergyAustralia NSW is supporting a number of initiatives that are looking to utilise the stored ash.

There were no reportable incidents, official cautions, warning letters, penalty notices or prosecution proceedings by any regulatory body during the reporting period.

There were no environmental incidents recorded during the 2018-19 reporting period.

## **12.** Activities to be completed in the next reporting period

WADA will continue under care and maintenance arrangements. Activities to be completed in the next reporting period will include:

- Environmental compliance monitoring for air quality, noise emissions and water quality;
- Water management works including the maintenance of sediment and erosion control structures;
- Dust suppression activities to minimise potential air quality impacts from WADA;
- Minor earthworks including road maintenance and drain works as required;
- Ash management works as required to stabilise slopes and minimise potential impacts;
- Environmental assessments and other specialist studies to inform the development of the final closure and rehabilitation plan. These may include additional groundwater, surface water and ecological assessment as required.

EnergyAustralia NSW will be assessing the repurposing of the Wallerawang Power Station which may include the WADA. This assessment is ongoing and will form part of the final closure and rehabilitation plan. It should be noted that a development application may be required to be submitted to either the Lithgow Shire Council or the DPE. EnergyAustralia NSW will consult with the relevant regulatory authority at the appropriate time as required.

## **12.1 Environmental Management Targets and Strategies** for the Next Year

Environmental measures to be implemented in the 2019-20 reporting period are detailed in Table 16.

Environment Management Area	Target / Strategy	Timeframe
Noise	Maintain compliance	Annual
Air Quality	Maintain compliance	Monthly
Water Quality	Continue water quality monitoring at the licenced ground and surface water sites	Monthly, until advised otherwise.
	Continue water quality monitoring in Lidsdale Cut Pond to see if concentrations reach equilibrium	Monthly, until advised otherwise.
Erosion & Sedimentation	Implement effective sediment and erosion control measures and undertake any rehabilitation works in accordance with approved management plans.	Annual
Landscape & Revegetation	Control the spread of invasive weed species in particular pampas grass.	Annual

 Table 16: Measures to be implemented in the Next Reporting Period

## **13. References**

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- Conneq. (2011). *Kerosene Vale Stage 2B Construction Environment Management Plan.* Conneq Industrial Infrastructure (Australia) Pty Ltd.
- DMC. (2010). *Fly Ash: Strategy Development for Aggregates and Other Bulk Use Applications.* DMC Advisory Pty Ltd, NSW.
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- Parsons Brinckerhoff. (2008a). *Kerosene Vale Stage 2 Ash Repository Area Environmental Assessment.* Parsons Brinckerhoff Australia Pty Ltd, NSW.
- Parsons Brinckerhoff. (2008b). *Kerosene Vale Stage 2 Ash Repository Operation Environmental Management Plan.* Parson Brinckerhoff Australia Pty Ltd, NSW.
- Parsons Brinckerhoff. (2009). *Stage 2 Kerosene Vale Ash Repository Operational Noise Review.* Parsons Brinckerhoff Australia Pty Ltd, NSW.

Annual Environmental Management Report Wallerawang Ash Dam Area 2018 - 2019

## **14. Glossary of Terms**

AEMR	Annual Environmental Management Report
СЕМР	Construction Environmental Management Plan
СоА	Condition of Approval (also known as MCoA – Minister's CoA)
DDR	Decommissioning, Deconstruction & Rehabilitation
DE	Delta Electricity
DECC	Department of Environment & Climate Change
DoP	Department of Planning
DPE	Department of Planning and Environment (formerly DP&I / DoP)
DP&I	Department of Planning and Infrastructure
EPL	Environment Protection Licence
KVAD	Kerosene Vale Ash Dam
KVAD/R	Kerosene Vale Ash Dam and Repository
KVAR	Kerosene Vale Ash Repository
LG	Lithgow Mercury
mAHD	Metres Australian Height Datum
NEMMCO	National Electricity Market Management Company
OEH	Office of Environment & Heritage (formerly DECC)
OEMP	Operation Environmental Management Plan
ONVMP	Operational Noise and Vibration Management Plan
RL	Relative Level
SSC	Sawyers Swamp Creek
SSCAD	Sawyers Swamp Creek Ash Dam

Annual Environmental Management Report Wallerawang Ash Dam Area 2018 - 2019

## Appendix A Detailed review checklist and Recommendations for Conditions of Approval

Wallerawang Ash Dam Area

2018 - 2019

## **Administrative Conditions**

**Terms of approval** 

Minister's Condition of Approval 1.1
The proponent shall carry out the project generally in accordance with the: a) Major Project Application 07_0005; b) Kensene Vale - Stade 2 Ash Renository Area (two volumes) - Environmental Assessment, prenared by Parsons Brinckerhoff and
<i>dated 1 April 2008;</i> Kerosene Vale – Stage 2 Ash Repository Area – The conditions of this approval.
<i>Compliance Assessment Observations and Comments</i> Based on the review undertaken, the KVAR Stage 2 operations have been carried out in accordance with the above requirements.
Compliance Assessment Finding – Compliant
Minister's Condition of Approval 1.2
<ul> <li>In the event of an inconsistency between:</li> <li>a) The conditions of this approval and any document listed from condition 1.1a) - 1.1c) inclusive the conditions of this approval shall prevail to the extent of the inconsistency; and</li> <li>b) Any of the documents listed from the condition 1.1a) - 1.1c) inclusive, the most recent document shall prevail to the extent of the inconsistency inclusive, the most recent document shall prevail to the extent of the inconsistency.</li> </ul>
<b>Compliance Assessment Observations and Comments</b> No inconsistencies were observed between the documents listed above during implementation of the project or during the course of the review of operations in preparing this AEMR.
Compliance Assessment Finding – Compliant

Wallerawang Ash Dam Area

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Minister's Condition of Approval 1.3

The proponent shall comply with the reasonable requirements of the Director-General arising from the Department's assessment of:

a) Any reports, plans or correspondence that are submitted in accordance with this approval; and

b) The implementation of any actions or measures contained in these reports, plans or correspondence.

**Compliance Assessment Observations and Comments** 

In a letter dated 4 July 2018, the DPE made seven comments in regard to the 2017-18 AEMR. The response to these actions is provided within Table 7. Table 7, Section 5 of this report. No further requests from the Secretary of the DPE were received in the 2017-18 reporting period.

Compliance Assessment Finding – Compliant

## Limits of approval

Minister's Condition of Approval 1.4

This approval shall lapse five years after the date on which it is granted, unless the works that are the subject of this approval are physically commenced on or before that time.

**Compliance Assessment Observations and Comments** 

The Project Approval for KVAR Stage 2 is dated 26 November 2008, indicating a 26 November 2013 lapse date. Works on the KVAR Stage 2B project commenced June 2013, well before the 'deadline' date.

Compliance Assessment Finding – Compliant

## **Statutory requirements**

Minister's Condition of Approval 1.5

to the project. No condition of this approval removes the obligation for the Proponent to obtain, renew or comply with such licences, permits The Proponent shall ensure that all licences, permits and approvals are obtained as required by law and maintained as required with respect or approvals.

**Compliance Assessment Observations and Comments** 

The project complies with the requirements of EnergyAustralia NSW's EPL 766. (See Table 1).

Compliance Assessment Finding – Compliant

Report Title: Wallerawang Ash Dam Area 2018 -2019 Objective ID: A1493312

Wallerawang Ash Dam Area

2018 - 2019

## **Specific Environmental Conditions**

Ash management

Minister's Condition of Approval 2.1

The Proponent shall prepare a long-term ash-management strategy including a program for investigation and assessment of alternative ash management measures with a goal of 40% reuse of ash by 31 December 2013. The report shall be submitted to the Director-General within six months of the commencement of operations. The Proponent shall report on the status and outcomes of its investigations to the Director-General every two years from the commencement of the operation of the project, unless otherwise agreed by the Director-General.

# **Compliance Assessment Observations and Comments**

EnergyAustralia NSW commissioned the report Fly Ash: Strategy Development for Aggregates and Other Bulk Use Applications (DMC, 2010). The reports were submitted to DP&I in September 2011.

the end of 2013. In March 2014, when it was announced that Wallerawang Power Station was being put out of service, the total ash reuse from Wallerawang Ash reuse progress is communicated via the Lend Lease Monthly Compliance Report and tracked in EnergyAustralia NSW's Annual Sustainability Report. The goal of 40% ash reuse was not achieved by 31st December 2013, with a total of only 0.32% ash reuse occurring from Wallerawang Power Station by had remained at 0.32%.

However, ash utilisation has been an ongoing program for the power station. Since then, more research and development to develop markets have been ത performed, rather than to solely focus on servicing established market opportunities. Generally, the major limitation to further market development is lack of rail, building and industrial infrastructure, particularly for the storage of ash at Wallerawang.

Compliance Assessment Finding – Non-Compliant

Minister's Condition of Approval 2.2

Proponent shall undertake revised staging of ash placement activities as described in the document referred to in condition 1.1c) of this To facilitate assessment of the viability of coal resources in the project area and provide a finite opportunity for their extraction, the approval

# **Compliance Assessment Observations and Comments**

Centennial Coal declined to extract the coal resources in the project area.

Ash will not be placed over the coal resource in the project area as a result of the non-operational status of Wallerawang Power Station, which is finite opportunity.

As outlined in this report, the pine plantation area now constitutes KVAR Stage 2B.

Compliance Assessment Finding - Compliant

## Noise impacts

<u>Report Title</u>: Wallerawang Ash Dam Area 2018 -2019 <u>Objective ID</u>: A1493312

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Construction activities associated with the project shall only be undertaken during the following hours:

- a) 7:00 am to 6:00 pm, Mondays to Fridays, inclusive;
  - b) 8:00 am to 0:00 pm or Saturdays to microsystems
    - b) 0.00 and to 1.00 pm on Saturday, and
       c) At no time on Sundays or public holidays.

# Compliance Assessment Observations and Comments

A CEMP was prepared for the works associated with the development of KVAR Stage 2B in preparation for ash placement and included a Construction Noise Management Plan and Noise Monitoring Program. This was submitted to DP&I in August 2011 and approved on the 16<sup>th</sup> December 2011.

No construction activities have occurred during the reporting period.

Compliance Assessment Finding – Not Applicable

## Minister's Condition of Approval 2.4

Monday to Saturday and 2:00 pm to 5:00 pm Monday to Friday. The Proponent shall not undertake such activities for more than three Activities resulting in impulsive or tonal noise emission (such as rock breaking or rock hammering) shall be limited to 8:00 am to 12:00 pm, continuous hours and must provide a minimum one-hour respite period.

**Compliance Assessment Observations and Comments** 

No activities resulting in tonal or impulsive noise emission have occurred during the monitoring period.

Compliance Assessment Finding - Not Applicable

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Report Title: Wallerawang Ash Dam Area 2018 -2019 Objective ID: A1493312

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The hours of construction activities specified under condition 2.3 of this approval may be varied with the prior written approval of the Director-General. Any request to alter the hours of construction specified under condition 2.3 shall be:

- a) Considered on a case-by-case basis;
- b) Accompanied by details of the nature and need for activities to be conducted during the varied construction hours; and
- Accompanied by any information necessary for the Director-General to reasonably determine that activities undertaken during the varied construction hours will not adversely impact on the acoustic amenity of sensitive receivers in the vicinity of the site. ົບ

# **Compliance Assessment Observations and Comments**

There has been no requirement to vary hours of construction during the reporting period, as no construction activities have taken place.

Compliance Assessment Finding - Not Applicable

Minister's Condition of Approval 2.7

The construction noise objective for the proponent is to manage noise from construction activities (as measured by LA10 (15minute) descriptor) so as not to exceed the background  $L_{A90}$  noise level by more than 10dB(A) at any sensitive receiver.

Construction Noise Management Plan (as referred under condition 6.3B) of this approval). The Proponent shall implement all reasonable Any activities that have the potential for noise emissions that exceed the objective must be identified and managed in accordance with the and feasible noise mitigation measures with the aim of achieving the construction noise objective.

**Compliance Assessment Observations and Comments** 

No construction activities with the potential to exceed background noise levels were undertaken during the reporting period.

Compliance Assessment Finding – Not Applicable

Wallerawang Ash Dam Area

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Operational activities associated with the project shall only be undertaken from 7:00am to 10:00pm Monday to Sunday.

**Compliance Assessment Observations and Comments** 

Lend Lease have advised that no operational activities have taken place during or outside the hours designated above.

Aurecon reported that: "No ash truck movements were noticed during the entire noise survey.

Compliance Assessment Finding - Compliant

Minister's Condition of Approval 2.9

of the logistical arrangements for ash haulage and placement to determine the feasibility of reducing the hours of operation. If, as a result of the review, it is determined that ash haulage and placement times can commence later and/or finish earlier, the Proponent shall aim to Within six months of commencement of operation of the project the Proponent shall prepare and submit to the Director-General a review observe the reduced hours whenever possible.

**Compliance Assessment Observations and Comments** 

The review was conducted within six months of commencement of operations and submitted to the DP&I on the 26th April 2012. The review determined that ash haulage and placement times could not commence later or finish earlier. This review was not submitted to the Director-General.

Compliance Assessment Finding - Compliant

<u>Report Title</u>: Wallerawang Ash Dam Area 2018 -2019 <u>Objective ID</u>: A1493312

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Minister's Condition of Approval 2.10

Operations outside the hours stipulated in condition 2.8 of this approval are only permitted in the following emergency situations:

- a) Where it is required to avoid the loss of live, property and/or to prevent environmental harm; or
- b) Breakdown of plant and/or equipment at the repository or the Wallerawang Power Station with the effect of limiting or preventing ash storage at the power station outside the operating hours defined in condition 2.8; or
- A breakdown of an ash haulage truck(s) preventing haulage during the operating hours stipulated in condition 2.8 combined with insufficient storage capacity at the Wallerawang Power Station to store ash outside of the project operating hours; or ົບ
- In the event that the National Electricity Market Management Company (NEMMCO), or a person authorised by NEMMCO, directs the Proponent (as a licensee) under the National Electricity Rules to maintain, increase or be available to increase power generation for system security and there is insufficient ash storage capacity at the Wallerawang Power Station to allow for the ash to be stored. q

In the event of conditions 2.10b) or 2.10c) arising, the Proponent is to take all reasonable and feasible measures to repair the breakdown in the shortest time possible.

**Compliance Assessment Observations and Comments** 

Lend Lease have advised that no operational activities have taken place outside the hours.

Compliance Assessment Finding - Not Applicable

Wallerawang Ash Dam Area

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Minister's Conditions of Approval 2.11, 2.12, 2.13 and 2.14

2.11- In the event that an emergency situation as referred to under condition 2.10b) or 2.10c) occurs more than once in any two-month period, the Proponent shall prepare and submit to the Director-General for approval a report including, but not limited to:

- a) The dates and a description of the emergency situations;
- b) An assessment of all reasonable and feasible mitigation measure to avoid recurrence of the emergency situations;
- c) Identification of a preferred mitigation measure(s); and
- d) Timing and responsibility for implementation of the mitigation measure (s).

The report is to be submitted to the Director-General within 60 days of the second exceedance occurring. The Proponent shall implement all reasonable and feasible mitigation measures in accordance with the requirements of the Director-General.

2.12- The Proponent shall notify the DECC prior to undertaking any emergency ash haulage or placement operations outside of the hours of operation stipulated in condition 2.8 of this approval and keep a log of such operations. 2.13- The Proponent shall notify the Director-General in writing within seven days of undertaking any emergency ash haulage or placement operations outside of the hours of operation stipulated in condition 2.8 of this approval.

6.5a) of this approval) prior to 8.00pm where it is known that emergency ash haulage or placement operations will be required outside of 2.14- The Proponent shall notify nearby sensitive receivers (as defined in the Operational Noise Management Plan required under condition the hours of operation stipulated in condition 2.8 of this approval.

**Compliance Assessment Observations and Comments** 

No emergency situations have occurred during the reporting period.

Compliance Assessment Finding - Not Applicable

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Report Title: Wallerawang Ash Dam Area 2018 -2019 Objective ID: A1493312

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Minister's Condition of Approval 2.15

The cumulative operational noise from the ash placement area and ash haulage activity shall not exceed an L<sub>Aeq (15 minute)</sub> of 40 dB(A) at the nearest most affected sensitive receiver during normal operating hours as defined in condition 2.8 of this approval. This noise criterion applies under the following meteorological conditions:

a) Wind speeds up to 3m/s at 10 metres above ground; and/or

b) Temperature inversion conditions of up to  $3^{\circ}C/100m$  and source to receiver gradient winds of up to 2m/s at 10m above ground level. This criterion does not apply where the Proponent and the affected landowner have reached a negotiated agreement in regard to noise, and a copy of the agreement has been forwarded to the Director-General and the DECC.

# **Compliance Assessment Observations and Comments**

EnergyAustralia NSW has not entered into any agreements regarding noise from KVAR with any potentially affected landholders, nor had any noise related Measured noise levels during September 2017 indicate KVAR Stage 2 operations are compliant with operational noise criteria (Aurecon, 2017)

complaints regarding the KVAR Stage 2 project. (See Section 6.2).

Compliance Assessment Finding - Compliant

Minister's Condition of Approval 2.16

installation of residential class mufflers, engine shrouds, body dampening, speed limiting, fitting of rubber stoppers to tail gates, limiting The Proponent shall implement measures to ensure noise attenuation of trucks. These measures may include, but are not limited to, the use of compression breaking, and ensuring trucks operate in a one-way system at the ash repository where feasible.

**Compliance Assessment Observations and Comments** 

Lend Lease has engaged a fleet of Mercedes-Benz Actros trucks which are compliant with the noise emission standards outlined above. No compression braking is used on the repository, trucks are well maintained with engines enclosed, mufflers in place, and proceed in a unidirectional format according to enforced speed limits. Minimal ash truck movements have occurred during the reporting period as a result of minimal ash being placed within Kerosene Vale Ash Repository due to the operational status of Wallerawang Power Station.

2018 - 2019

Minister's Condition of Approval 2.17

operative approach for the management and mitigation of noise impacts associated with coal and ash truck movements along the private The Proponent shall liaise with the owner/operator of Angus Place Coal Mine with the aim of preparing a protocol which provides for a cohaul road.

## **Compliance Assessment Observations and Comments**

by truck movement through the monthly meetings and are bound by their Environment Protection Licence 467. Information provided to EnergyAustralia NSW by Centennial regarding potential Angus Place noise impacts associated with coal and ash truck movements underneath this licence included hours of and Centennial includes the restriction of movement of trucks along the haul road between 6pm and 7am daily- trucks are diverted from the haul road passage during these hours as necessary. Centennial Coal reports to EnergyAustralia NSW with any instances that may impact on background noise caused EnergyAustralia NSW regularly liaises with Centennial Coal through monthly fuel supply meetings. The protocol developed between EnergyAustralia NSW operation, noise level limits and pollutants.

In 2015, Angus Place Coal Mine was placed into Care and Maintenance functionality. As a result, no coal truck movements have occurred on the private haul road. In addition, minimal ash truck movements have occurred along the private haul road during the reporting period as a result of minimal ash being placed within Kerosene Vale Ash Repository due to the operational status of Wallerawang Power Station.

Wallerawang Ash Dam Area

2018 - 2019

Minister's Condition of Approval 2.18

Where noise monitoring (as required by conditions 3.2 or 3.3 of this approval) identifies any non-compliance with the operational noise criterion specified under condition 2.15 of this approval the Proponent shall prepare and submit to the Director-General for approval a report including, but not limited to:

- a) An assessment of all reasonable and feasible physical and other mitigation measures for reducing noise at the source including, but not limited to –
- i. Construction of a noise barrier along the haulage road
- ii. Alternative ash haulage routes, and
- iii. Alternative methods of ash conveyance to the repository; and
- b) Identification of the preferred measure(s) for reducing noise at the source;
- c) Feedback from directly affected property owners and the DECC on the proposed noise mitigation measures; and
- d) Location, type, timing and responsibility for implementation of the noise mitigation measure(s).

The report is to be submitted to the Director-General within 60 days of undertaking the noise monitoring which has identified exceedences of the operational noise criterion specified under condition 2.15, unless otherwise agreed to by the Director-General. The Proponent shall implement all reasonable and feasible mitigation measures in accordance with the requirements of the Director-General.

## **Compliance Assessment Observations and Comments**

EnergyAustralia NSW has implemented six-monthly noise monitoring assessments. No non-compliances were identified during the reporting period. Refer to Appendices B for further details.

Wallerawang Ash Dam Area

2018 - 2019

Minister's Condition of Approval 2.19

If, after the implementation of all reasonable and feasible source controls, as identified in the report required by condition 2.18, the noise generated by the project exceeds the criterion stipulated in condition 2.15 at:

- a) Any sensitive receiver in existence at the date of this approval; or
- b) Any residential dwelling for which an approval has been sought or obtained under the Environmental Planning and Assessment Act 1979 no later than six months after the confirmation of operational noise levels;

Upon receiving a written request from an affected landowner (unless that landowner has acquisition rights under condition 2.20 of this approval and has requested acquisition) the Proponent shall implement additional noise mitigation measures such as double glazing, insulation, air conditioning and or other building acoustic treatments at any residence on the land, in consultation with the landowner.

For the purpose of this condition and condition 2.20, confirmation of operational noise levels means:

- a) Completion of the operational noise review required under condition 3.2 this approval; and
- b) Implementation of any source controls, as required under condition 2.18 of this approval, should the operational noise review indicate noise levels in excess of the operational noise criterion specified in condition 2.15; and
  - Monitoring of operational noise levels, as required under condition 3.3b) of this approval, following the implementation of any source controls. ົບ

the Proponent and landowner cannot agree on the measures to be implemented, or there is a dispute about the implementation of these The additional mitigation measures must be reasonable and feasible. If within three months of receiving this request from the landowner measures, then either party may refer the matter to the Director-General for resolution, whose decision shall be final.

# **Compliance Assessment Observations and Comments**

EnergyAustralia NSW has implemented six-monthly noise monitoring assessments. No non-compliances were identified during the reporting period. Refer to Appendices B for further details.

EnergyAustralia NSW has received no written requests from affected landowners regarding noise mitigation measures.

Wallerawang Ash Dam Area

2018 - 2019

Minister's Condition of Approval 2.20

If, after the implementation of all reasonable and feasible source controls, as identified in the report required by condition 2.18, the noise generated by the project exceeds the criterion stipulated in condition 2.15 by more than 5dB(A):

- a) At a sensitive receiver in existence at the date of this approval; or
- Act 1979 prior to the landholder receiving written notification that they are entitled to land acquisition rights, as per condition 2.25 At any residential dwelling for which an approval has been sought or obtained under the Environmental Planning and Assessment of this approval; or (q
- Over 25% or more of the area of a vacant allotment in existence at the date of this approval, and where a dwelling is permissible under the Environmental Planning and Assessment Act 1979 at that date, with the exception of land that is currently used for industrial or mining purposes; ົບ

The Proponent shall, upon receiving a written request for acquisition from the landowner, acquire the land in accordance with the procedures in conditions 2.22 to 2.24 of this approval. Any landowner that has agreed to, or property that has been the subject of, the application of additional noise mitigation measures under condition 2.19 of this approval waives the right to land acquisition.

**Compliance Assessment Observations and Comments** 

EnergyAustralia NSW has received no written or verbal requests from landowners to acquire their land.

Compliance Assessment Finding - Compliant

Minister's Condition of Approval 2.21

The land acquisition rights under condition 2.20 of this approval do not apply to landowners who have sought approval to subdivide their land after the date of this approval, unless the subdivision is created pursuant to condition 2.24 of this approval.

**Compliance Assessment Observations and Comments** 

No landholders have applied for approval to subdivide their land according to the land acquisition rights.

Compliance Assessment Finding - Not Applicable

Report Title: Wallerawang Ash Dam Area 2018 -2019 Objective ID: A1493312

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Minister's Condition of Approval 2.22

Within three months of receiving a written request from a landowner with acquisition rights under condition 2.20 of this approval, the Proponent shall make a binding written offer to the landowner based on:

- a) The current market value of the landowner's interest in the property at the date of this written request, as if the property were unaffected by the project which is the subject of the project application, having regard to the:
- Existing and permissible use of the land, in accordance with the applicable planning instruments at the date of the written request; and
- Presence of improvements on the property and/or any approved building or structure which has been physically commenced at the date of the landowner's written request, and is due to be completed subsequent to that date, but excluding any improvements that have resulted from the implementation of condition 2.19 of this approval; ïi.
- b) The reasonable costs associated with:
- Relocating within the Lithgow local government area, or to any other local government area determined by the Director-General;
- Obtaining legal advice and expert advice for determining the acquisition price of the land, and the terms upon which it is required; and ïi.
- c) Reasonable compensation for any disturbance caused by the land acquisition process.

However, if at the end of this period, the Proponent and landowner cannot agree on the acquisition price of the land, and/or the terms upon which the land is to be acquired, then either party may refer the matter to the Director-General for resolution. Upon receiving such a request, the Director-General shall request the President of the NSW Division of the Australian Property Institute to appoint a qualified independent valuer or Fellow of the Institute, to consider submissions from both parties, and determine a fair and reasonable acquisition price for the land, and/or terms upon which the land is to be acquired.

Within 14 days of receiving an independent valuer's determinations, the Proponent shall make a written offer to purchase the land at a price not less than the independent valuer's determination. If the landowner refuses to accept this offer within six months of the date of the Proponent's offer, the Proponent's obligations to acquire the land shall cease, unless otherwise agreed by the Director-General.

**Compliance Assessment Observations and Comments** 

No landholders have applied for approval to subdivide their land according to the land acquisition rights.

Compliance Assessment Finding - Not Applicable

Report
Management
Environmental
Annual

2018 - 2019

Minister's Conditions of Approval 2.23, 2.24 and 2.25

2.23- The Proponent shall bear the costs of any valuation or survey assessment requested by the independent valuer or the Director-General and the costs of determination referred to above.

associated with obtaining Council approval for any plan of subdivision (where permissible), and registration of the plan at the Office of the 2.24- If the Proponent and landowner agree that only part of the land shall be acquired, then the Proponent shall pay all reasonable costs Registrar-General.

2.25- The Proponent shall provide written notice to all landowners that are entitled to rights under conditions 2.19 and 2.20 within 21 days of determining the landholdings were additional noise mitigation measures or land acquisition apply. For the purpose of condition 2.20b), this condition only applies where operational noise levels have been confirmed in accordance with the definition in condition 2.19.

# **Compliance Assessment Observations and Comments**

No landholders have applied for approval to subdivide their land according to the land acquisition rights.

Compliance Assessment Finding - Not Applicable

## Sawyers Swamp Creek realignment

EnergyAustralia NSW decided upon commencement of the Project that the realignment of SSC was not necessary. Therefore, the CoAs relating to SSC realignment are not applicable. This refers to CoAs 2.26 (a – m), 2.27, 2.28 and 2.29.

## Surface water quality

## Minister's Condition of Approval 2.30

The Proponent shall take all reasonable and feasible measures to prevent discharge of sediments and pollutants from the construction and operation of the project entering waterways.

Note: Section 120 of the Protection of the Environment Operations Act 1997 prohibits the pollution of water except where expressly provided by an Environmental Protection Licence.

# **Compliance Assessment Observations and Comments**

No surface waters from KVAR Stage 2 are allowed to enter the SSC catchment. Measures to prevent surface water discharge include a series of collection ponds on site, with water reticulated around KVAR for the treatment of ash and dust suppression.

Wallerawang Ash Dam Area

2018 - 2019

Minister's Condition of Approval 2.31

Earthworks not associated with the realignment of Sawyer Swamp Creek shall not be undertaken within 50m of the creek where reasonable and feasible.

**Compliance Assessment Observations and Comments** 

A minimum buffer zone of 50m has been maintained along the riparian area of SSC for all operations.

**Compliance Assessment Finding -** Compliant

Minister's Condition of Approval 2.32

3 All equipment, machinery and vehicles associated with the construction and operation of the project shall be operated and maintained in manner that minimises the potential for oil and grease spills/leaks.

## **Compliance Assessment Observations and Comments**

Lend Lease supply Energy Australia NSW with Monthly Client Service Reports detailing site safety, ash placement, operations, environmental and maintenance aspects of site management.

These maintenance records include general operations (truck maintenance and hours, ash analyses, sensor repairs, vent lines, line trips etc.), projects (unit outages, silo repairs and maintenance, valve repairs and maintenance etc.), incidents /near misses, training and safety.

Monthly Client Service Reports may be viewed upon request.

Compliance Assessment Finding - Compliant

<u>Report Title</u>: Wallerawang Ash Dam Area 2018 -2019 <u>Objective ID</u>: A1493312

Wallerawang Ash Dam Area

2018 - 2019

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### Air quality impacts

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operational activities, including wind-blown and traffic generated dust, on the receiving environment. All activities on the site shall be The Proponent shall construct and operate the project in a manner that minimises dust impacts generated by construction works and undertaken with the objective of preventing visible emissions of dust from the site. Should such visible dust emissions occur at any time, the Proponent shall identify and implement all practicable dust mitigation measures, including cessation of relevant works, as appropriate, such that emissions of visible dust cease.

# **Compliance Assessment Observations and Comments**

Dust management within the site is included in the responsibilities of all operations, including:

- Use of perimeter sprays at the ash placement area;
- Water cart (20,000 L) on site during all ash placement operations 8 am to 5 pm Mondays to Sundays;
- Ash placement operations;
- Final capping of ash; and
- General maintenance and rehabilitation of the ash placement area.

## Compliance Assessment Finding - Compliant

### Minister's Condition of Approval 2.34

The Proponent shall ensure that the load carrying compartment(s) of all ash haulage trucks are covered at all times except when loading or unloading ash material.

# **Compliance Assessment Observations and Comments**

No issues with load coverings were recorded for the 2018-19 reporting period.

2018 - 2019

### Lighting emissions

### Minister's Condition of Approval 2.35

The Proponent shall take all practicable measures to mitigate off-site lighting impacts from the project and ensure all external lighting associated with the project complies with Australian Standard AS4282 1997 – Control of the Obtrusive Effects of Outdoor Lighting.

## **Compliance Assessment Observations and Comments**

Lend Lease Work Procedures Manual contains procedures that apply to all personnel and equipment operating at Kerosene Vale, including mobile lighting towers for ash placement operations, and details the responsibilities, application and procedures for using outdoor lighting for the project, within the project area. Lights used to illuminate the tipping area must face south or east, operators must ensure the horizontal distance of the illuminated area is not less than 40m and as access to the repository for ash transport is between 7am and 10pm lights must be extinguished by 10pm. The lights used at KVAR are the HILITE 4000 hired from Coates Hire Operations Pty Ltd. The specification sheets for these lights form part of the Work Procedures Manual for lighting.

Compliance Assessment Finding - Compliant

### **Construction traffic and transport impacts**

### Minister's Condition of Approval 2.36

The Proponent shall ensure that construction vehicles associated with the project:

- a) Minimise the use of local roads (though residential streets and town centres) to gain access to the site;
- b) Adhere to any nominated haulage routes identified in the Construction Traffic Management Plan as referred to in condition 6.3a) of this approval; and
  - Adhere to a Construction Vehicle Code of Conduct prepared to manage driver behaviour along the local road network to address traffic impacts (and associated noise) along nominated haulage routes. ົບ

# **Compliance Assessment Observations and Comments**

A Construction Traffic Management Plan was submitted to and approved by the DP&I as part of the Construction Environment Management Plan.

Wallerawang Ash Dam Area

2018 - 2019

Heritage impacts

Minister's Condition of Approval 2.37

The Proponent shall ensure that all construction personnel are educated on their obligations in respect of the protection of Aboriginal and non-indigenous heritage sites and items.

**Compliance Assessment Observations and Comments** 

No aboriginal or other cultural heritage sites have been identified at Kerosene Vale. All of EnergyAustralia NSW's cultural sites are listed in the Section 170 The Lend Lease Work Procedures Manual includes Environmental Management Controls for Cultural Heritage and applies to all personnel.

Heritage and Conservation Register.

**Compliance Assessment Finding - Compliant** 

Minister's Condition of Approval 2.38

operational activities, all work likely to affect the heritage sites or item(s) is to cease immediately and the discovery of the objects shall be reported to DECC or the Denartment ac relevant If any previously unidentified heritage sites or items (Aboriginal and/or non-indigenous) are discovered during construction works reported to DECC or the Department as relevant.

**Compliance Assessment Observations and Comments** 

No previously unidentified heritage sites or items were discovered during the reporting period.

Compliance Assessment Finding - Not applicable

### Waste management

Minister's Condition of Approval 2.39

All waste materials shall be assessed, classified, managed and disposed of in accordance with Environmental Guidelines: Assessment, Classification and Management of Liquid and Non-Liquid Wastes (EPA, 1999).

**Compliance Assessment Observations and Comments** 

Lend Lease provides Monthly Ash Placement Work Instructions to address all issues of routine site maintenance as part of a monthly work program. Waste management is conducted in accordance with EPA guidelines.

2018 - 2019

Minister's Condition of Approval 2.40

All waste materials removed from the site shall only be directed to a waste management facility lawfully permitted to accept the materials.

**Compliance Assessment Observations and Comments** 

waste and materials for recycling. These are stored in intermediate storage facilities at Wallerawang Power Station and routinely removed by EnergyAustralia Lend Lease utilises EnergyAustralia NSW's waste management facilities for wastes generated in the operation of the repository, including waste oils, general NSW's waste contractors. No additional waste materials were removed from the site during the reporting period.

Compliance Assessment Finding - Compliant

Minister's Condition of Approval 2.41

processing, reprocessing, or disposal on the site, except as expressly permitted by a licence under the Protection of the Environment The Proponent shall not cause, permit or allow any waste generated outside the site to be received at the site for storage, treatment, Operations Act 1997, if such a licence is required in relation to that waste.

**Compliance Assessment Observations and Comments** 

No wastes generated outside the Kerosene Vale site are allowed to enter the area.

To prevent the unlawful access to the repository area, regular security patrols are conducted across the site. Both Lend Lease and EnergyAustralia NSW security personnel are required to report if they encounter any rubbish or wastes outside those that are allowed during routine operations.

Compliance Assessment Finding - Compliant

Report Title: Wallerawang Ash Dam Area 2018 -2019 Objective ID: A1493312

Wallerawang Ash Dam Area

2018 - 2019

### **Environmental Monitoring**

**Construction noise monitoring** 

### Minister's Condition of Approval 3.1

The Proponent shall prepare and implement a Construction Noise Monitoring Program to confirm the predictions of the noise assessment detailed in the document referred to under condition 1.1b) of this approval and assess compliance against the construction noise criterion stipulated in condition 2.7 of this approval. The noise monitoring program shall be prepared in consultation with, and to the satisfaction of, the DECC. The monitoring program shall form part of the Construction Noise Management Plan referred to in condition 6.3b) of this approval and must include monitoring of the construction noise generated during:

- a) The realignment of Sawyers Swamp Creek;
- b) Construction of the stabilisation berm;
- c) Excavation of the former pine plantation area;
- d) Relocation and construction of surface water management structures; and
- e) Concurrent construction activities.

The Proponent shall forward to the DECC and the Director-General a report containing the results of each noise assessment and describing any non-compliance within 14 days of conducting a noise assessment.

# **Compliance Assessment Observations and Comments**

A CEMP was prepared for the construction works associated with the development of KVAR Stage 2B in preparation for ash placement, including a Construction Noise Management Plan and Noise Monitoring Program. This was submitted to DP&I in August 2011 and approved on the 16<sup>th</sup> December 2011.

No construction activities took place during the reporting period.

2018 - 2019

**Operational noise review** 

Minister's Condition of Approval 3.2

Within 60 days of the commencement of operation of the project, unless otherwise agreed to by the Director-General, the Proponent shall submit for the approval of the Director-General an Operational Noise Review to confirm the operational noise impacts of the project. The Operational Noise Review must be prepared in consultation with, and to the satisfaction of, the DECC. The Review shall:

- a) Identify the appropriate operational noise objectives and level for sensitive receivers;
- b) Describe the methodologies for noise monitoring including the frequency of measurements and location of monitoring sites;
- c) Document the operational noise levels at sensitive receivers as ascertained by the noise monitoring program;
- Assess the noise performance of the project against the noise criterion specified in condition 2.15 of this approval and the predicted noise levels as detailed in the report referred to under condition 1.1b) of this approval; and (p
- e) Provide details of any entries in the Complaints Register (as required under condition 5.4 of this approval) relating to noise impacts.

Where monitoring indicates noise levels in excess of the operational noise criterion specified in condition 2.15 of this approval, the Proponent shall prepare a report as required by condition 2.18 of this approval.

**Compliance Assessment Observations and Comments** 

The Operational Noise Review (Parsons Brinckerhoff, 2009) was submitted to the DP&I on 16 September 2009, and the Department acknowledged its satisfaction that CoA 3.2 had been met on 18 September 2009.

Wallerawang Ash Dam Area

2018 - 2019

**Ongoing operational noise monitoring** 

Minister's Condition of Approval 3.3

The Proponent shall prepare and implement an Operational Noise Monitoring Program to assess compliance against the operational noise criterion stipulated in condition 2.15 of this approval, throughout the life of the project. The noise monitoring program shall be prepared in consultation with, and to the satisfaction of, the DECC.

The noise monitoring program shall be prepared in accordance with the requirements of the New South Wales Industrial Noise Policy (EPA, 2000) and must include, but not be limited to:

- a) Monitoring during ash placement in the far western area of the site adjacent to the haul road; and
- b) Monitoring of the effectiveness of any noise mitigation measures implemented under condition 2.18 of this approval, against the noise criterion specified in condition 2.15 of this approval.

within 30 metres of a dwelling where the dwelling is more than 30 metres from the boundary, to determine compliance with the noise criterion stipulated in condition 2.15 of this approval. Where it can be demonstrated that direct measurement of noise from the project is impractical, the DECC may accept alternative means of determining compliance (see Chapter 11 of the NSW Industrial Noise Policy). The Noise from the project is to be measured at the most affected point on or within the residential boundary, or at the most affected point modification factors in Section 4 of the NSW Industrial Noise Policy shall also be applied to the measured noise levels where applicable.

The Proponent shall forward to the DECC and the Director-General a report containing the results of any non-compliance within 14 days of conducting a noise assessment. Where monitoring indicates noise levels in excess of the operational noise criterion specified in condition 2.15 of this approval, the Proponent shall prepare a report as required by condition 2.18 of this approval.

The monitoring program shall form part of the Operational Noise Management Plan referred to in condition 6.5a) of this approval.

**Compliance Assessment Observations and Comments** 

and provided to Delta to determine the minimum monitoring requirements for groundwater following receipt of approval from the DP&I. EnergyAustralia An Operational Noise Monitoring Program in the form of the Operational Noise sub-plan was developed as part of the OEMP (Parsons Brinckerhoff, 2008b) NSW continue to implement the required noise monitoring assessments. No non-compliances were identified during the reporting period.

2018 - 2019

Groundwater monitoring

Minister's Condition of Approval 3.4

describe the location, frequency, rationale and procedures and protocols for collecting groundwater samples, as well as the parameters groundwater quality and hydrology. The program shall be developed in consultation with, and to the satisfaction of, the SCA, and shall The Proponent shall prepare and implement a Groundwater Monitoring Program to monitor the impacts of ash placement activities on local analysed and methods of analysis. The monitoring program shall be ongoing for the life of the project and include, but not be limited to:

- a) Monitoring at established bore sites (or replacement bore sites in the event that existing sites are damaged or lost) as described in the document referred to under condition 1.1b) of this approval; and
- b) A schedule for periodic monitoring of groundwater quality, depth and flow at all monitoring sites, at an initial frequency of no less than once every month for the first 12 months of operation.

The monitoring program shall form part of the Groundwater Management Plan referred to in condition 6.5b) of this approval

# **Compliance Assessment Observations and Comments**

A Groundwater Monitoring Program in the form of the Groundwater Quality sub-plan was developed as part of the OEMP (Parsons Brinckerhoff, 2008b) and provided to EnergyAustralia NSW, then Delta, to determine the minimum monitoring requirements for groundwater following receipt of approval from the DP&I.

2018 - 2019

### Surface water quality monitoring

### Minister's Condition of Approval 3.5

and SCA, and shall describe the location, frequency, rationale and the procedures and protocols for collecting water samples as well as the The Proponent is to implement a surface water quality monitoring program to monitor the impacts of the ash placement activities on, and the realignment of, Sawyers Swamp Creek. The Program shall be developed in consultation with and to the satisfaction of the DPI (Fisheries) parameters analysed and methods of analysis. The program shall include, but not necessarily be limited to:

- a) Monitoring at the four-existing water quality monitoring sites as described in the document referred to under 1.1b) of this approval;
  - b) Monitoring downstream of the realigned section of Sawyers Swamp Creek;
- c) Monitoring at groundwater discharge points into Sawyers Swamp Creek;
- Wet weather monitoring with a minimum of two events recorded within the first 12 months of both the operation of the project and post realignment of Sawyers Swamp Creek; and (p
- than once every month for the first 12 months and must include, but not be limited to, dissolved oxygen, turbidity, total phosphorus A schedule for periodic monitoring of surface quality at all sites throughout the life of the project, at an initial frequency of no less and total nitrogen. e

The monitoring program shall form part of the Surface Water Management Plan referred to in condition 6.5c) of this approval.

## **Compliance Assessment Observations and Comments**

A surface water Monitoring Program in the form of the surface water Quality sub-plan was developed as part of the OEMP (Parsons Brinckerhoff, 2008b) and provided to Delta to determine the minimum monitoring requirements for surface water following receipt of approval from the DP&I.

Compliance Assessment Finding - Compliant

## Sawyers Swamp Creek realignment monitoring

EnergyAustralia NSW decided upon commencement of the Project that the realignment of SSC was not necessary. Therefore, CoAs 3.6 and 3.7 relating to SSC realignment are not applicable.

2018 - 2019

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### Air quality monitoring

### Minister's Condition of Approval 3.8

1.1b) of this approval. The air quality monitoring program shall be ongoing for the life of the project, including final rehabilitation and The Proponent shall prepare an Air Quality Monitoring Program, in consultation with, and to the satisfaction of, the DECC. The Program shall include but not necessarily be limited to, monitoring for dust at the monitoring sites identified in the document referred to under condition stabilisation of the site.

The monitoring program shall form part of the Air Quality Management Plan referred to in condition 6.5d) of this approval.

## **Compliance Assessment Observations and Comments**

An air quality monitoring program in the form of the air quality sub-plan was developed as part of the OEMP (PB, 2009) and provided to Delta to determine the minimum monitoring requirements for air quality following receipt of approval from the DP&I. Dust monitoring results are recorded monthly with colour and textural observations. These results indicate that KVAR is managed effectively for ash dust and as such is in compliance with CoAs 2.33 and 3.8.

Compliance Assessment Finding - Compliant

# **Compliance Monitoring and Tracking**

Minister's Condition of Approval 4.1

Prior to each of the events listed below, the Proponent shall certify in writing to the satisfaction of the Director-General that it has complied with all conditions of this approval applicable prior to that event:

- a) Commencement of any construction works on the land subject of this approval; and
- b) Commencement of operation of the project.

## **Compliance Assessment Observations and Comments**

The DP&I indicated its satisfaction that EnergyAustralia NSW had met the relevant pre-operational requirements of this project before commencement in 2009. This included submission of a Pre-Operation Compliance Report, Compliance Tracking Program, and the Operation Environmental Management Plan.

Wallerawang Ash Dam Area

2018 - 2019

Minister's Condition of Approval 4.2
The Proponent shall develop and implement a Compliance Tracking Program for the project, prior to commencing operations, to track compliance with the requirements of this approval and shall include, but not necessarily be limited to:
a) Provisions for periodic review of the compliance status of the project against the requirements of this approval and the Statement of Commitments detailed in the document referred to in condition 1.1c) of this approval;
b) Provisions for periodic reporting of the compliance status to the Director-General;
c) A program for independent environmental auditing in accordance with AS/NZ ISO 19011:2003 – Guidelines for Quality and/or Environmental Management Systems Auditing;
d) Procedures for rectifying any non-compliance identified during environmental auditing or review of compliance;
e) Mechanisms for recording environmental incidents and actions taken in response to those incidents;
f) Provisions for reporting environmental incidents to the Director-General during construction and operation; and
g) Provisions for ensuring all employees, contractors and sub-contractors are aware of, and comply with, the conditions of this approval relevant to their respective activities.
The Compliance Tracking Program shall be implemented prior to operation of the project with a copy submitted to the Director-General for approval within four weeks of commencement of the project, unless otherwise agreed by the Director-General.
Compliance Assessment Observations and Comments
Environmental incidents that may occur in respect to KVAR Stage 2 operations are reported in accordance with the Operation Environmental Management Plan (Parsons Brinckerhoff, 2008b) and are captured within the Environmental Management System. Annual reporting requirements are covered by the preparation of the AEMR.
Sections of the Minister approved OEMP that relate to this Condition include:
Section 3.8 Environmental Audits (CoA 4.2c);
Section 3.8 Environmental Audits and Section 3.8.1 Non-Compliances (CoA 4.2d);
Section 3.9 Environmental Incidents Management (CoA 4.2e);
Section 3.9 Environmental Incidents Management (CoA4.2f); and
Section 3.5 Environmental Awareness Training and Site Inductions (4.2g).
Lend Lease have included the directive in the Repository Site Management Plan (Conneq, 2010) that formal site management processes be documented monthly and weekly in line with the OEMP and the Repository Management Plan. The Monthly Client Service Reports are used as a method for recording any incidences.
Compliance Assessment Finding - Compliant

2018 - 2019

Minister's Condition of Approval 4.3 and 4.4

Proponent to satisfy the requirements of condition 4.2. In doing so, the Proponent must demonstrate to the Director-General how these CoA 4.3 - Nothing in this approval restricts the Proponent from utilising any existing compliance tracking programs administered by the systems address the requirements and/or have been amended to comply with the requirements of the condition.

to ensure compliance with the conditions of this approval, and general consistency with the documents listed under condition 1.1 of this CoA 4.4 - The Proponent shall meet the requirements of the Director-General in respect of the implementation of any measure necessary approval.

## **Compliance Assessment Observations and Comments**

This project has a Minister approved OEMP (April, 2009), which is currently under review by EnergyAustralia NSW and will be submitted to the DPE for approval upon completion. The project also operates under EnergyAustralia NSW's ISO14001 accreditation and Environmental Management System.

The Secretary has not issued any requests to implement any additional measure to ensure compliance with the relevant CoAs for the KVAR Stage 2 project.

Compliance Assessment Finding - Not applicable

Wallerawang Ash Dam Area

2018 - 2019

# **Community Information and Complaints Management**

**Provision of Information** 

Minister's Conditions of Approval 5.1 and 5.2

associated with the project. The Proponent shall, subject to confidentiality, publish and maintain up-to-date information on this website or Prior to the commencement of the project, the Proponent shall establish and maintain a website for the provision of electronic information dedicated pages including, but not necessarily limited to:

- a) The documents referred to under condition 1.1 of this approval;
- This project approval, Environment Protection Licence and any other relevant environmental approval, licence or permit required and obtained in relation to the project; (q
- All strategies, plans and program required under this project approval, or details of where this information can be viewed; ົບ
- d) Information on construction and operational progress;
- e) The outcomes of compliance tracking in accordance with the requirements of this project approval.
- 5.2 The Proponent shall make all documents required to be provided under condition 5.1 of this approval publicly available.

## **Compliance Assessment Observations and Comments**

EA have developed a specific project website for Kerosene Vale Ash Repository that enables the provision of electronic information listed within CoA 5.1. A link to this web page is below.

https://www.energyaustralia.com.au/about-us/energy-generation/wallerawang-power-station-closure/kerosene-vale-ash-repository

The website includes:

- Major Project Application 07\_0005
- Kerosene Vale Stage 2 Ash Repository Area (two volumes) Environmental Assessment prepared by Parsons Brinckerhoff and dated 1 April 2008.
  - Kerosene Vale Stage 2 Ash Repository Area Submissions Report prepared by Parsons Brinckerhoff and dated 30 May 2008
    - Project Approval (Conditions of Approval) File S07/00001, dated 26 November 2008.
- Construction Environment Management Plan (Conneg, 2011)
- Operation Environment Management Plan (Parsons Brinckerhoff, 2008b)
- Copies of previous Annual Environment Management Reports

https://www.energyaustralia.com.au/about-us/energy-generation/wallerawang-power-station-closure/wallerawang-epa-reports. The Environment Protection Licence and Pollution Incident Response Management Plan are available at the web page below: Information on construction and operational progress is provided on the web page below:

https://www.energyaustralia.com.au/about-us/energy-generation/mt-piper-power-station/mt-piper-and-wallerawang-community.

The Water Access Licence and Water Supply Work and Water Use Approval are available at the web page below:

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https://www.energyaustralia.com.au/about-us/energy-generation/mt-piper-power-station/mt-piper-and-wallerawang-water-data

Compliance Assessment Finding - Compliant

**Complaints and enquiries procedure** 

Minister's Condition of Approval 5.3

Prior to the commencement of the project, the Proponent shall ensure that the following are available for community complaints and enquiries during construction and operation:

- a) A 24-hour contact number(s) on which complaints and enquiries about construction and operational activities may be registered;
  - b) A postal address to which written complaints and enquiries may be sent; and
- c) An email address to which electronic complaints and enquiries may be sent; and

d) An email address to which electronic complaints and enquiries may be transmitted.

The telephone number, postal address and email address shall be published in a newspaper circulating in the local area prior to the commencement of the project. The above details shall also be provided on the website required by condition 5.1 of this approval.

**Compliance Assessment Observations and Comments** 

The website:

https://www.energyaustralia.com.au/about-us/energy-generation/mt-piper-power-station lists the following contact details for the project:

24-hour contact number - via the Switchboard on 02 6354 8111

Postal address:

Environment Specialist

EnergyAustralia NSW Locked Bag 1000, Portland NSW 2847

Email: contactus@energyaustraliansw.com.au

Compliance Assessment Finding - Compliant

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Minister's Condition of Approval 5.4

The Proponent shall record the details of all complaints received through the means listed under condition 5.3 of this approval in an up-todate Complaints Register. The Register shall record, but not necessarily be limited to:

- a) The date and time of the complaint;
- The means by which the complaint was made (e.g. telephone, email, mail, in person); (q
- c) Any personal details of the complainant that were provided, or if no details were provided a note to that effect;
- d) The nature of the complaint;
- e) The time taken to respond to the complaint;
- f) Any investigations and actions taken by the Proponent in relation to the complainant; and
- g) If no action was taken by the Proponent in relation to the complaint, the reason(s) why no action was taken.

The Complaints Register shall be made available for inspection by the Director-General upon request.

# **Compliance Assessment Observations and Comments**

Any complaints called in to EnergyAustralia NSW go via the switchboard (02 6354 8111) and are then redirected to the appropriate area of EnergyAustralia NSW operations.

All complaints are recorded in the Ellipse system in the Incidents and Complaints Register with all details captured including actions to be taken if necessary. If actions were necessary, a review of those actions is undertaken before the work order is closed.

No complaints were received regarding KVAR for the reporting period.

Compliance Assessment Finding - Compliant

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### **Environmental Management**

**Environmental representative** 

### Minister's Condition of Approval 6.1

shall nominate for the approval of the Director-General a suitably qualified and experienced Environmental Representative(s) independent Prior to the commencement of any construction or operational activities, or as otherwise agreed by the Director-General, the Proponent of the design, construction and operation personnel. The Proponent shall engage the Environmental Representative(s) during any construction activities, and throughout the life of the project, or as otherwise agreed by the Director-General. The Environmental Representative(s) shall:

- a) Oversee the implementation of all environmental management plans and monitoring programs required under this approval, and advise the Proponent upon the achievements of these plans/programs;
- Have responsibility for considering and advising the Proponent on matters specified in the conditions of this approval and the Statement of Commitments as referred to under condition 1.1c) of this approval; (q
- Oversee the implementation of the environmental auditing of the project in accordance with the requirements of condition 4.2 of this approval and all relevant project Environmental Management System(s); and ົບ
- unintended or adverse environmental impacts, and, failing the effectiveness of such steps, to recommend to the Proponent that relevant activities are to be ceased as soon as reasonably practicable if there is a significant risk that an adverse impact on the Be given the authority and independence to recommend to the Proponent reasonable steps to be taken to avoid or minimise environment will be likely to occur. Ģ

## **Compliance Assessment Observations and Comments**

In March 2009 EnergyAustralia NSW nominated the Environment Manager- Western Nino di Falco as the Environmental Representative. The Environment Manager oversees the implementation of all operations at KVAR through attendance at Monthly Client Meetings with Lend Lease and regular liaison with the External Plant Manager. The Environment Manager guides the project through site visits, sampling and other regulatory activities to ensure compliance with the environmental requirements of the CoAs and all relevant licences.

Environmental Representative. Furthermore, in a letter dated 19 January 2017, EnergyAustralia NSW notified the DPE of Peter Griffiths appointment to Safety Leader within the Organisation and nominated the new NSW Environment Leader, Ben Eastwood, as the Environmental Representative, which was In February 2015, EnergyAustralia NSW notified the DPE of Mr di Falco's retirement and nominated the new Environment Manager, Peter Griffiths, as the agreed to by the Secretary in a letter dated 28 February 2017.

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**Construction environmental management** 

Minister's Conditions of Approval 6.2 and 6.3

Management Plan (CEMP). The CEMP shall outline the environmental management practices and procedures to be followed during construction. The CEMP shall be prepared in accordance with Guideline for the Preparation of Environmental Management Plans (DIPNR, 6.2 – Prior to the commencement of construction work, the Proponent shall prepare and implement a Construction Environmental 2004).

unless otherwise agreed by the Director-General. Construction shall not commence until written approval has been received from the The Construction Environmental Management Plan for the project (or any stage of the project) shall be submitted to the Director General for approval at least four weeks prior to the commencement of any construction work associated with the project (or stage as relevant), Director-General.

6.3 – As part of the Construction Environmental Management Plan for the project, the Proponent shall prepare and implement the following plans:

- a) A Construction Traffic Management Plan, prepared in consultation with the RTA, the relevant Council and emergency services to manage the construction traffic impacts of the project, including but not limited to:
  - Identifying construction vehicle volumes (construction staff vehicles, heavy vehicles and oversized loads) and haulage routes;
- Identifying any road closures and/or traffic detours during the haulage of oversized loads as agreed to by the relevant roads authority; ïi.
- Detailing a Construction Vehicle Code of Conduct to set driver behaviour controls to minimise impacts on the land uses along haulage routes (including noise minimisation measures); and Ш.
- *Complying with the document* Procedures for Use in the Preparation of a Traffic Management Plan (*RTA*, 2011). i,
- b) A Construction Noise Management Plan to detail how construction noise impacts would be minimised and managed. The Strategy shall be developed in consultation with, and to the satisfaction of, the DECC and shall include, but not necessarily be limited to:
- Details of construction activities and an indicative schedule for construction works; *.*.
- Identification of construction activities that have the potential to generate noise impacts on sensitive receivers; ïi.
- Procedures for assessing noise levels at sensitive receivers and compliance; Ш.
- Details of the reasonable and feasible actions and measures to be implemented to minimise noise impacts and, if any noise exceedence is detected, how any non-compliance would be rectified; and i.
  - Procedures for notifying sensitive receivers of construction activities that are likely to affect their noise amenity. >
- c) An Erosion and Sediment Control Plan to detail measures to minimise erosion and the discharge of sediment and other pollutants to land and/or water during construction works. The Plan must include, but not necessarily be limited to:
  - Identification of the construction activities that could cause soil erosion or discharge sediment or water pollutants from the site; .

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A description of the management methods to minimise soil erosion or discharge of sediment or water pollutants from the site, including a strategy to minimise the area of bare surfaces, stabilise disturbed areas, and minimise bank erosion; and Ϊ.

Demonstration that the proposed erosion and sediment control measures will conform with, or exceed, the relevant requirements of Managing Urban Stormwater: Soils and Construction (Landcom, 2004).

## **Compliance Assessment Observations and Comments**

A Construction Environmental Management Plan for KVAR Stage 2B was developed in consultation with EnergyAustralia NSW's Western Environment Section and approved by the DP&I in August 2011.

Compliance Assessment Finding - Compliant

### **Operational environmental management**

## Minister's Conditions of Approval 6.4 and 6.5

6.4 – The Proponent shall prepare and implement and Operation Environmental Management Plan to detail an environmental management framework, practices and procedures to be followed during operation of the project. The Plan shall be consistent with Guideline for the Preparation of Environmental Management Plans (DIPNR, 2004) and shall include, but not be limited to:

- a) Identification of all statutory and other obligations that the Proponent is required to fulfil in relation to operation of the project, including all approvals, licences and consultations;
- A description of the roles and responsibilities for all relevant employees (including contractors) involved in the operation of the project; **q**
- Overall environmental policies and principles to be applied to the operation of the project ົບ
- Standards and performance measures to be applied to the project, and a means by which environmental performance can be periodically reviewed and improved, where appropriate; Ģ
- Management policies to ensure that environmental performance goals are met and to comply with the conditions of this approval; G
  - f) The additional plans listed under condition 6.5 of this approval; and
- g) The environmental monitoring requirements outlined under conditions 3.3 to 3.5 inclusive and 3.8 of this approval.

The Plan shall be submitted for the approval of the Director-General no later than four weeks prior to the commencement of operation of the project, unless otherwise agreed by the Director-General. Operation shall not commence until written approval has been received from the Director-General.

Nothing in this approval precludes the Proponent from incorporating the requirements of the Operational Environmental Management Plan into existing environmental management systems and plan administered by the Proponent. 6.5 – As part of the Operation Environmental Management Plan for the project, required under condition 6.4 of this approval, the Proponent shall prepare and implement the following Management Plans:

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- An Operational Noise Management Plan to detail measures to mitigate and manage noise during operation of the project. The Plan Procedures to ensure that all reasonable and feasible noise mitigation measures are applied during operation of the project; shall be prepared in consultation with, and to the satisfaction of, the DECC and include, but not necessarily be limited to: . a)
- Identification of all relevant sensitive receivers and the applicable criteria at those receivers commensurate with the noise limit specified under condition 2.15 of this approval; ïi.
- Identification of activities that will be carried out in relation to the project and the associated noise sources; iii.
- Noise monitoring procedures (as referred to in condition 3.3 of this approval) for periodic assessment of noise impacts at the relevant receivers against the noise limits specified under this approval and the predicted noise levels as detailed in the report referred to under condition 1.1b) of this approval; iv.
- Details of all management methods and procedures that will be implemented to control individual and overall noise emissions from the site during operation; 2
- Procedures and corrective actions to be undertaken if non-compliance against the operational noise criteria is detected; and vi.
- vii. Provisions for periodic reporting of results to DECC.
- A Groundwater Management Plan to detail measures to mitigate and manage groundwater impacts. The Plan shall be prepared in consultation with, and to the satisfaction of, the SCA and include, but not necessarily be limited to: (q
- i. Baseline data on groundwater quality, depth and flow in the project area;
- ii. Groundwater objectives and impact assessment criteria;
- A program to monitor groundwater flows and groundwater quality in the project area as required by condition 3.4 of this approval; iii.
- A protocol for the investigation of identified exceedences of the groundwater impact assessment criteria; Ś.
- A response plan to address potential exceedences and groundwater impacts; and 2
- vi. Provisions for periodic reporting of results to the SCA.
- and the discharge of sediments and other pollutants to land and/or waters throughout the life of the project. The Plan shall be based A Surface Water Management Plan to outline measures that will be employed to manage water on the site, to minimise soil erosion on best environmental practice and shall be prepared in consultation with, and to the satisfaction of, the SCA and DPI (Fisheries). The Plan shall include, but not necessarily be limited to: ົບ
- Baseline data on the water quality and flow in Sawyers Swamp Creek up to the date of this approval; ...
- Water quality objectives and impact assessment criteria for Sawyers Swamp Creek; ïi.
- A program to monitor surface water quality in Sawyers Swamp Creek as referred to in condition 3.5 of this approval; iii.
- A protocol for the investigation of identified exceedences in the impact assessment criteria; Ś.
  - A response plan to address potential adverse surface water quality exceedences; 2

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	vi. A site water management strategy associated water management meas and the procedures for decommissic	A site water management strategy identifying clean and dirty water areas for Stage A, B and C of the project and the associated water management measures including erosion and sediment controls and provisions for recycling/reuse of water and the procedures for decommissioning water management structures on the site; and
	vii. Provisions for periodic reporting of	Provisions for periodic reporting of results to the DPI (Fisheries) and the SCA.
(p	<ul> <li>d) An Air Quality Management Plan to outline prepared in consultation with, and to the se</li> </ul>	An Air Quality Management Plan to outline measures to minimise impacts from the project on local air quality. The Plan shall be prepared in consultation with, and to the satisfaction of, the DECC and include, but not necessarily be limited to:
	i. Baseline data on dust deposition levels,	els;
	ii. Air quality objectives and impact assessment criteria;	sessment criteria;
	iii. An air quality monitoring program a	An air quality monitoring program as referred to in condition 3.8 of this approval;
	iv. An assessment of alternative meth winds;	An assessment of alternative methods of ash placement to minimise the exposure of active placement areas to prevailing winds;
	v. Mitigation measures to be incorpora	Mitigation measures to be incorporated during emplacement activities and haulage of ash;
	vi. An operating protocol for the reposi	An operating protocol for the repository irrigation system including activation rates, application rates and area of coverage;
	vii. A protocol for the investigation of v	A protocol for the investigation of visible emissions from the repository area;
	viii. A response plan to address visible e	A response plan to address visible emissions from the repository area; and
	ix. Provisions for periodic reporting of results to the DECC	esults to the DECC.
(ə	<ul> <li>A Landscape/Revegetation Plan to outline stabilisation of the site and compatibility v be limited to:</li> </ul>	A Landscape/Revegetation Plan to outline measures to minimise the visual impacts of the repository and ensure the long-term stabilisation of the site and compatibility with the surrounding land fabric and land use. The Plan shall include, but not necessarily be limited to:
	i. Identification of design objectives and	nd standards based on local environmental values, vistas, and land uses;
	ii. A description of short- and long-term revegetation measures;	n revegetation measures;
	iii. A schedule of species to be used in revegetation;	evegetation;
	iv. Timing and progressive implementatio and	ion of revegetation works as placement areas are completed, including landscape plans;
	v. Procedures and methods to monitor	Procedures and methods to monitor and maintain revegetated areas during the establishment phase and long-term.
	Revegetation works must incorporate the use of local native species.	ne use of local native species.
Comp	Compliance Assessment Observations and Comment:	nts
The Ol 2 com	Coperation Environmental Management Plan was printmenced in September 2009. The OEMP has been up	The Operation Environmental Management Plan was prepared by Parsons Brinckerhoff. Approval was granted in April 2009 and operations at KVAR Stage 2 commenced in September 2009. The OEMP has been reviewed by EnergyAustralia NSW during the 2018-19 reporting period to ensure that it reflects the
curren submit	current Care and Maintenance activities. The reviewed OEMP was prepared in consubmitted on the Department of Planning and Environment on the 4th August 2017.	current Care and Maintenance activities. The reviewed OEMP was prepared in consultation with the EPA, WaterNSW, DPI-Water, DPI-Fisheries and was submitted on the Department of Planning and Environment on the 4th August 2017.
omo)	Compliance Assessment Finding - Compliant	

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### **Environmental Reporting**

**Environmental incident reporting** 

Minister's Conditions of Approval 7.1 and 7.2

Proponent shall provide full written details of the incident to the Director-General within seven days of the date on which the incident 7.1 – The Proponent shall notify the Director-General of any environmental incident within 12 hours of becoming aware of the incident. The occurred. 7.2 – The Proponent shall meet the requirements of the Director-General to address the cause or impact of any environmental incident, as it related to this approval, reported in accordance with condition 7.1 of this approval, within such period as the Director-General may require.

**Compliance Assessment Observations and Comments** 

No environmental incidents requiring notification of the Secretary occurred within the April 2018- March 2019 reporting period

Compliance Assessment Finding - Not applicable

### Annual performance reporting

Minister's Condition of Approval 7.3

Management Report (AEMR). The AEMR shall review the performance of the project against the Operation Environmental Management Plan The Proponent shall, throughout the life of the project, prepare and submit for the approval of the Director-General, an Annual Environmental (refer to condition 6.4 of this approval) and the conditions of this approval. The AEMR shall include, but not necessarily by limited to:

- a) Details of compliance with the conditions of this approval;
- A copy of the Complaints Register (refer to 5.4 of this approval) for the preceding twelve-month period (exclusive of personal details), and details of how these complaints were addressed and resolved; (q
- Identification of any circumstances in which the environmental impacts and performance of the project during the year have not been generally consistent with the environmental impacts and performance predicted in the documents listed under condition 1.1 of this approval, with details of additional mitigation measures applied to the project to address recurrence of these circumstances; ົບ
- Results of all environmental monitoring required under conditions 3.3 to 3.8 of this approval, including interpretations and discussion by a suitably qualified person; and Ð
- the project have not been achieved, indicating the reason for failure to meet the criteria and the action taken to prevent recurrence A list of all occasions in the preceding twelve-month period when environmental goals/objectives/impact assessment criteria for of that type of failure. e

The Proponent shall submit a copy of the AEMR to the Director-General every year, with the first AEMR to be submitted no later than twelve months after the commencement of operation of the project. The Director-General may require the Proponent to address certain matters in

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relation to the environmental performance of the project in response to review of the Annual Environmental Report. Any action required to be undertaken shall be completed within such period as the Director-General may require. The Proponent shall make copies of each AEMR available for public inspection on request.

**Compliance Assessment Observations and Comments** 

This AEMR satisfies the requirements of CoA 7.3.

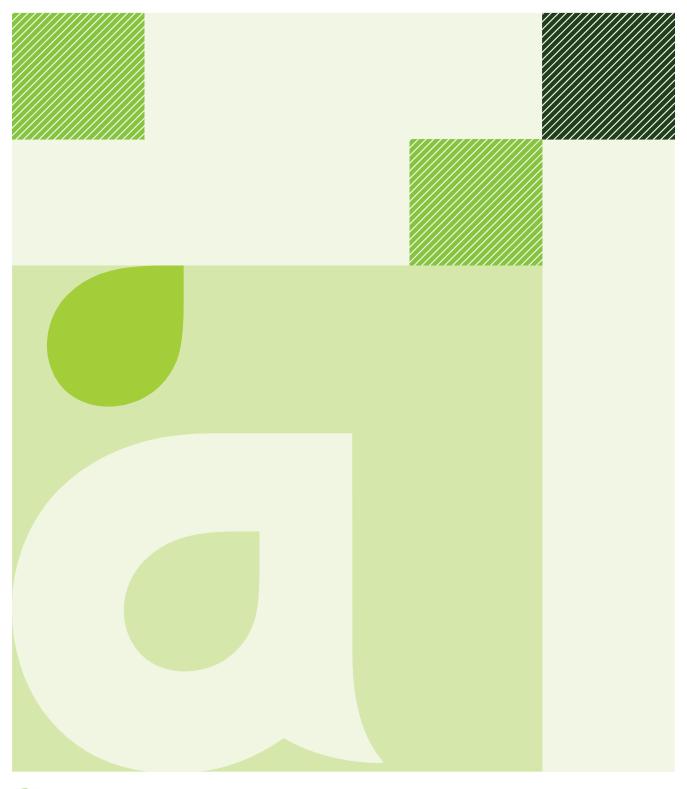
Compliance Assessment Finding - Compliant

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Annual Environmental Management Report Wallerawang Ash Dam Area 2018 - 2019

### Appendix B KVAR Stage 2 Noise Report – June 2018



### aurecon

**Project:** Kerosene Vale Ash repository Stage 2

Ongoing operational noise measurements (June 2018)

**Prepared for:** EnergyAustralia NSW

Project: 247023

13 July 2018

### **Document control record**

Document prepared by:

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Document control aurecon					aurecon	
Repo	rt Title	Ongoing operational noise	measurement	s (June 201	8)	
Document ID		247023-KV-REP-12-REV2	Project Number		247023	
File F	Path	\\Aurecon.info\Shares\AUSYD\Pro Delivery\12.Deliverables\Acoustic Noise June 2018 rev2.docx			eport\KVAR Co	mpliance
Client		EnergyAustralia NSW	Client Contact		Alicia de Vos	
Rev	Date	Revision Details/Status	Prepared by	Author	Verifier	Approver
1	5 July 2018	Initial Draft	AL	AL	BD	LT
2	13 July 2018	Final issue	AL	AL	BD	LT
Curre	Current Revision 2					

Approval				
Author Signature	this	Approver Signature		
Name	Akil Lau	Name	Les Thorpe	
Title	Acoustic Consultant	Title	Project Director	

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### 1 Introduction

Aurecon was engaged by EnergyAustralia NSW to carry out ongoing operational noise monitoring for the Kerosene Vale Stage 2 Ash Repository (KVAR) located in Wallerawang, NSW in accordance with Project Approval Application No. 07\_0005. The noise measurements were carried out on Sunday 17 June 2018 and Monday 18 June 2018, during the early morning and evening periods as per the requirements outlined in the KVAR Stage 2 Operational Noise and Vibration Management Plan (ONVMP).

### 1.1 Site details

The project site consists of an Ash Repository which services the nearby Wallerawang Power Station (WPS). During normal operation of the KVAR Stage 2, the following major noise emissions would be expected.

- Unloading of ash from trucks at the repository.
- Placement and handling of ash at the repository site.
- Operation of trucks on the private haulage road; this includes trucks leaving WPS loaded with ash (travelling north) and returning from the repository empty (travelling south).
- Water pumps operating at the repository.
- Water cart driving around.

WPS is currently being decommissioned, and as such KVAR is no longer fully operational. No noise emissions from the location of the KVAR was evident during the current site visit.

Figure 1 shows the site layout and location of sensitive receivers relative to the major noise sources which include the decommissioned WPS, as well as major roads in the area. Table 1 outlines the most affected sensitive receivers and their distance to the haulage road.

Representative sensitive receiver	Distance to haulage road (meters)*
60 Skelly Road	300
10 Skelly Road	270
21 Neubeck Street	145

### Table 1: Representative sensitive receivers

Note \* - distance relates to the property boundary or a point 30 m from the dwelling location

It should be noted that coal supply trucks also utilise the private haulage road. Their noise impacts are not considered to be part of the Stage 2 KVAR works and thus their noise impact is outside the scope of this report. While undertaking noise measurements it is extremely difficult to visually distinguish between coal supply trucks and ash trucks, therefore, for the purpose of prediction of noise emissions from ash trucks alone, EnergyAustralia NSW provides the number of truck movements for the periods of measurement.

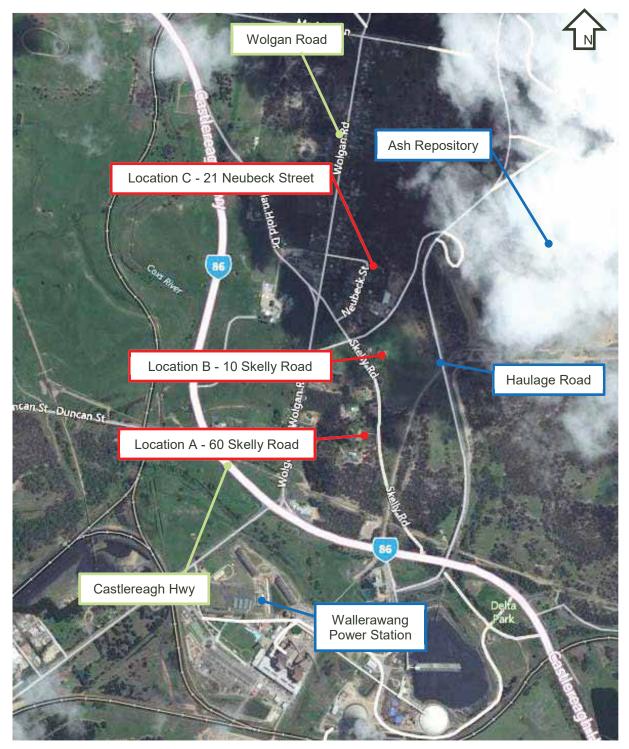


Figure 1 | Site details

### 2 Noise criteria

The applicable operational noise criteria are outlined in the Project Approval, Application No. 07\_0005. The criteria are summarised in Condition 2.15 as follows:

2.15 The cumulative operational noise from the ash placement area and ash haulage activity shall not exceed a  $L_{Aeq}$  (15 minute) of 40 dB(A) at the nearest most affected sensitive receiver during normal operating hours as defined in condition 2.8.

This criterion applies under the following meteorological conditions:

- a) Wind speeds up to 3 m/s at 10 meters above ground<sup>1</sup>; and/or
- b) Temperature inversion conditions of up to 3°C/100 m and source to receiver gradient winds of up to 2 m/s at 10 m above ground level

Normal operating hours in accordance with Conditions 2.8 are 7:00 am to 10:00 pm Monday to Sunday.

### 3 Noise measurements

### 3.1 Measurement methodology

Two types of measurements were carried out during the current monitoring period:

- Ambient noise measurements and
- Sound exposure level measurements.

The measurements were carried out on Sunday 17 June 2018 and Monday 18 June 2018, during the early morning and evening periods, when the noise impacts are likely to be the most significant.

### Ambient noise measurements

The ambient compliance noise measurements were conducted using a Larson Davis 831 Type 1 sound level meter which was set to 'A' frequency weighting, 'F' time weighting, and was fitted with an approved windshield. Measurements were typically taken at a height of 1.2 metres and at least 3.5 metres from any reflecting structure other than the ground.

Measurements were undertaken for a period of 15 minutes at each of the selected measurement locations (See Table 2). A Larson Davis CAL200 was utilised to calibrate the sound level meters before and after each series of measurements. No significant calibration drift was noted.

### Weather conditions

The weather during the ambient noise logging ranged from overcast to sunny conditions, and wind speeds were less than 3 m/s at ground level. Measurements were generally taken in accordance with the Australian Standard *AS 1055.1 1997: Acoustics – Description and measurement of environmental noise*. Refer to Appendix D for weather summary. There was intermittent rain and high winds (> 5m/s) during two days of monitoring. Attended noise measurements were only undertaken when the weather was suitable in accordance with AS 1055.1.

<sup>&</sup>lt;sup>1</sup> As per AS 1055.1 – 1997, noise measurements should be avoided when maximum windspeed exceed 5 m/s at the microphone position.

### Sound exposure level (SEL) measurements

The Sound Exposure Level (SEL) measurements were also carried out using the Larson Davis 831 Type 1 sound level meter. SEL is the equivalent one second A-weighted sound level which produces the same sound energy as an actual identified event. The SEL measurement was commenced when a truck/ light vehicle was observed to pass a nominated reference location and stopped when the end of the truck passed a second nominated reference location. The nominated reference locations were identified where the truck could be visually observed.

### 3.2 Measurement locations

The measurement locations were chosen to represent the three most affected sensitive receivers as outlined in the ONVMP and shown in Table 1. These three receivers were identified based on the information in the Stage 2 Kerosene Vale Ash Repository operational noise review.

Due to the high background noise levels at each of the three monitoring locations it was difficult to assess individual truck noise events. A fourth noise monitoring location identified as Location D and shown in Appendix C, was selected closer to the haulage route to measure individual truck pass-by events. Table 2 and Figure 2 outline the noise measurement locations.

Measurement location	Measurement distance to haulage road (meters)	Representative sensitive receiver
Α	300	60 Skelly Road
В	270	10 Skelly Road
С	145	21 Neubeck Street
D	80	-

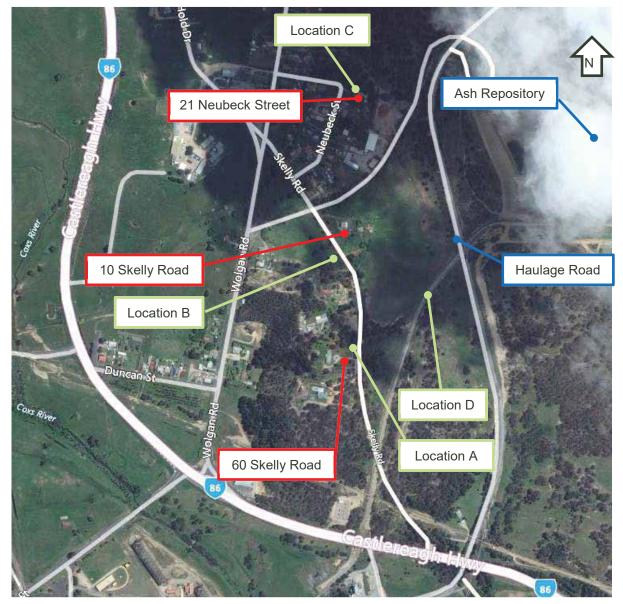


Figure 2 | Noise measurement locations

### 3.3 Conditions during measurements

### 3.3.1 Operating conditions

EnergyAustralia NSW stated that no trucks were operating during any of the measurement periods.

### 3.3.2 Meteorological conditions

The meteorological conditions applicable to the noise survey period are based on meteorological data provided at 15 minute intervals from the Mt Piper weather station. This data is shown in Appendix D.

Periods of rain and adverse winds during the noise survey were excluded.

### 3.4 Results

### 3.4.1 Ambient noise measurements

The results from the 15-minute ambient noise measurements at each of the measurement locations are shown in Table 3.

Table 3: N	loise	measurement	results	(15 minute)

ion	Date of measurement	Time	Measured sound pressure level dB(A)				ure	Predicted noise contributi	Number of truck Pass-bys and direction of travel <sup>1</sup>		
Location			L <sub>Ae</sub> q <sup>#</sup>	L <sub>Am</sub> ax <sup>*</sup>	Lami n**		<b>L</b> д9 0^	on by KVAR (dBA)	North	South	Total
(문) Sunday (문) 17/06/2018 (전) 문	8:10	45	67	35	46	38	0	0	0	0	
	17/06/2018	17:25	44	57	39	46	41	0	0	0	0
ି କ ତ ନ୍ଦି Monday 18/06/2018	9:12	48	61	42	50	44	0	0	0	0	
	18/06/2018	17:31	44	55	40	46	41	0	0	0	0
ਤਿੰਦੀ ਤਿੰਦੀ ਨੇ ਇੰ 17/06/2018	Sunday	8:29	45	61	37	48	41	0	0	0	0
	17/06/2018	18:50	43	55	40	45	41	0	0	0	0
은 윤 Monda	Monday	9:31	45	65	36	47	40	0	0	0	0
	18/06/2018	17:45	45	58	40	48	41	0	0	0	0
ଁ ଞ୍ଧ 17/	Sunday	8:41	42	67	35	43	38	0	0	0	0
	17/06/2018	19:07	42	55	38	44	40	0	0	0	0
- <del>7</del>	Monday	9:47	48	65	39	50	43	0	0	0	0
	18/06/2018	17:57	41	52	38	43	39	0	0	0	0

Note : <sup>1</sup> - Truck counts include ash trucks and light commercial vehicles.

Exceedances of the  $L_{Aeq (15 min)}$  of 40 dB(A) are shown in Bold.

- <sup>#</sup> L<sub>Aeq</sub> refers to A-weighted equivalent continuous sound pressure level over measurement period. It is used to quantify the average noise level over a time period.
- \* L<sub>Amax</sub> refers to the maximum A-weighted noise level detected during the measuring period. It refers to the maximum background noise detected.
- \*\* *L<sub>Amin</sub>* refers to the minimum A-weighted noise level detected during the measuring period. It refers to the minimum background noise detected.
- \* L<sub>A10</sub> refers to the A-weighted noise level which is exceeded for only 10% of the measuring period. It is usually used as the descriptor for intrusive noise level and represents ambient road traffic noise in general.
- <sup>^</sup> L<sub>A90</sub> refers to the A-weighted noise level which is exceeded for 90% of the measuring period. It is usually used as the descriptor for background noise level during the measurement period.

The measured  $L_{Aeq (15 min)}$  exceeded the assessment criteria of  $L_{Aeq (15 min)}$  of 40 dB(A) during all of the attended noise monitoring events. As there were no truck movements associated with the operation of the KVAR during the attended noise monitoring event, it can be assumed that the KVAR operations did not contribute to the background noise levels at any of the measurement locations and that the high noise levels are associated with local noise events such as traffic from surrounding roads and birds/insects. Noise contribution from the KVAR is therefore considered to be 0 dBA.

### 3.4.2 SEL measurements

The individual truck pass-by noise event (SEL) measurements at Location D (approximately 80 meters from the haulage road) were conducted on 7 November 2011, 21 April 2013 and 31 March 2014. The results are summarised in Table 4. The number of actual truck pass-bys counted during the daytime survey are also summarised in Table 4. These data were used to predict the noise impact from the truck movement on the sensitive receivers.

Based on the visual site inspection, the grade (slope) of the haulage road rises from south to north. The trucks moving in the northerly direction on the haulage road appear to rev the engine more compared to the trucks moving in the opposite direction and thereby producing a marginally higher SEL as evident in the results summarised in Table 4.

Date	Truck travelling direction	Average event duration (sec)	Average SEL dB(A)	No. of valid truck event measurements
7/11/2011	South	28.9	68	8
	North	18.1	70	9
21/04/2013	South	24.0	67	5
	North	19.5	70	7
31/04/2014	South	27.7	69	2
	North	28.3	70	2

Table 4: SEL noise measurement results at Location D

### 4 Noise assessment

General observation regarding the ambient noise environment, as well as the truck movements and ash repository operations, during the attended noise measurements are described as follows.

- Operational noise from the KVAR site and the truck engine noise was inaudible at the sensitive receiver locations during the attended noise measurements and no ash trucks or light commercial vehicles were visible on the haul road.
- The noise levels at all locations were affected by background noise sources such as bird/insects, domestic animals and domestic noise. Background noise at all sites was dominated by the intermittent traffic noise from nearby Castlereagh Highway and Wolgan Road.

General observations for the three monitoring locations are described below.

### 4.1 Location A (60 Skelly Road)

The background noise contributions at Location A were predominantly from the traffic noise from Castlereagh Highway and distant traffic. Faint and intermittent traffic noise from Wolgan Road was also audible.

The haulage road was clearly visible from this location, however no coal or ash trucks were visible on the haulage road during the attended noise monitoring period (except for one light commercial vehicle

during the Monday morning period). Noise from birds and insects also contributed to the ambient noise at this location.

As shown in Table 3, the background noise varied over the two days with  $L_{A90}$  ranging from 38 dB(A) to 43 dB(A). The background noise ( $L_{A90}$ ) during the attended noise measurements was predominantly due to road traffic on the Castlereagh Highway, Wolgan Road and other nearby roads.

### 4.2 Location B (10 Skelly Road)

Contributions to the background noise at Location B were predominantly from birds/insects/animals and traffic on Wolgan Road and Skelly Road.

Traffic noise from Wolgan Road and Skelly Road was clearly audible at this location and also contributed to the ambient noise levels.

The haulage road was clearly visible from this measuring location, however no coal or ash trucks were visible on haulage road during the attended noise monitoring period movement.

Background noise levels was fairly consistent over the two days with  $L_{A90}$  ranging from 40 dB(A) to 41dB(A).

### 4.3 Location C (21 Neubeck Street)

Contributions to the background noise at Location C were predominantly from birds/insects/animals and distant traffic on Wolgan Road and other roads. Traffic noise from Wolgan Road was clearly audible and also contributed to the ambient noise levels.

The haulage road was not clearly visible from this location because of an earth mound and heavy vegetation blocking the line of sight; however no truck engine noise was audible during the attended noise monitoring period.

Background noise varied over the two days with LA90 ranging from 38 dB(A) to 44 dB(A).

### 4.4 Location D

The noise data collected at Location D (Figure 2 and Appendix C) measured the SEL of individual truck pass-by events on 7 November 2011, 22 April 2013 and 31 April 2014 (See Table 4).

This location is closest to the haulage road and as such, each truck pass-by was the dominant noise source (clearly audible above other ambient noise sources) during these monitoring events.

### 5 Analysis and recommendations

### 5.1 Data analysis

As can be observed from the summary of noise measurements presented above, the existing ambient noise levels  $L_{Aeq (15 min)}$  exceed the assessment criteria of  $L_{Aeq (15 min)}$  of 40 dB(A) on all but three of the monitoring events. This section deals with noise prediction based on the number of truck movements (worst case scenario) for any worst case 15 minute period.

To assess the impact of the ash truck noise emissions, the influence of individual truck pass-by noise events have to be taken into account.  $L_{Aeq (15 min)}$  noise level was predicted based on the SEL measurement results (shown in Table 4) and the number of truck movements provided by EnergyAustralia NSW.

The predicted noise levels take into account the total number of truck pass-bys (including ash trucks and small commercial vehicles) and the distance of the noise source from the receiver. The assessment included the calculated barrier effect (- 2dB(A)) at Location C. This is due to the earth mound located on the northern side of the site which blocks the line of sight between 21 Neubeck Street and the haulage road, therefore attenuating the noise from the haulage road. Generally, trucks operate at a constant rate, with approximately 15-20 minute circuits for each truck. Table 5 provides a summary of truck pass-bys based on information collected during a previous site visit.

	Information collected during site visit on 30-31 March 2014					
Periods	Total number of trucks pass bys per 45 minutes	Average number of trucks pass bys per 15 minutes				
Morning 30/03/2014	7	2.3				
Evening 30/03/2014	2	0.7				
Morning 31/03/2014	7	2.3#				
Evening 31/03/2014	3	1.0				

Table 5: Truck movement data

Note: the figure in **bold** is the worst-case truck movement (most frequent) used to predict the noise contribution from the truck movements (shown in Table 6)

# Maximum number of truck pass-bys as per information collected during the site visit.

As shown in Table 5, the maximum number of truck pass-bys was during the morning period on both 30/03/2014 and 31/03/2014. The lowest truck pass-bys was during the evening period on 30/03/2014. The noise emissions from the KVAR are considered to be below the assessment criteria as they were predominantly inaudible during the noise survey and could not be distinguished.

Table 6 provides the noise predictions from haulage trucks alone at the nearest sensitive receivers based on SEL measurements. The prediction is calculated from the movement of ash trucks based on the worst case scenario (i.e. 2.3 truck pass-bys during any 15 minute period).

Table 6: Noise predictions from truck movements based on SEL measurements

Sensitive receiver	Distance to haulage road (m)	No. of average truck movements per 15min	Predicted contribution L <sub>Aeq (15 min)</sub> (dBA)	Criteria L <sub>Aeq (15 min)</sub> (dBA
60 Skelly Road	300	2.3	32	40
10 Skelly Road	270	2.3	33	40
21 Neubeck Street *	145	2.3	37*	40

Note \* - Includes the barrier attenuation (-2dBA) provided by the earth mound blocking direct line of sight between the residence and haulage road.

Based on the worst case scenario the noise impact from truck movements complies with noise criteria of  $L_{Aeq (15 min)}$  of 40 dB(A) at all the sensitive receiver locations.



There were no truck movements during this current noise monitoring event, therefore the operational noise emissions from the Stage 2 KVAR is considered to be compliant with Condition 2.15 of the Project Approval.

# 6 Conclusion

Aurecon conducted operational noise monitoring for the Stage 2 KVAR located in Wallerawang, NSW. The noise measurements were carried out at the three most affected sensitive receiver locations on Sunday 17 June 2018 and Monday 18 June 2018, in the early morning and evening in accordance with the KVAR Stage 2 ONVMP.

The applicable noise assessment criteria of  $L_{Aeq (15 minute)}$  of 40 dB(A) from all ash haulage and ash placement associated operational noise emissions at the nearest sensitive receivers is outlined in the Project Approval, Application No. 07\_0005.

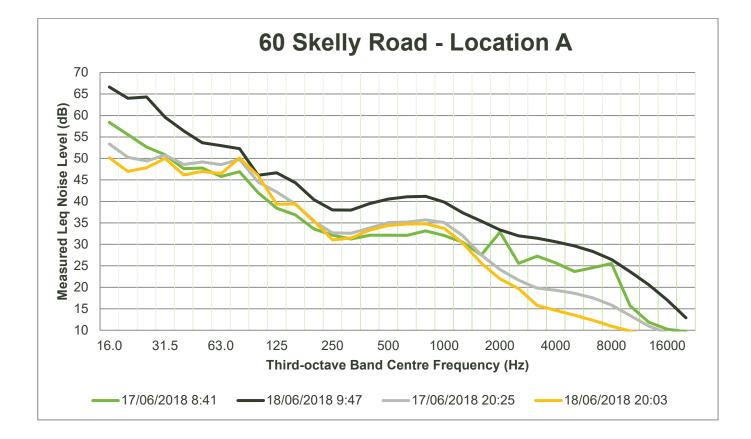
The primary contributor to the background and ambient noise levels at all measurement locations was the traffic noise on the nearby roads.

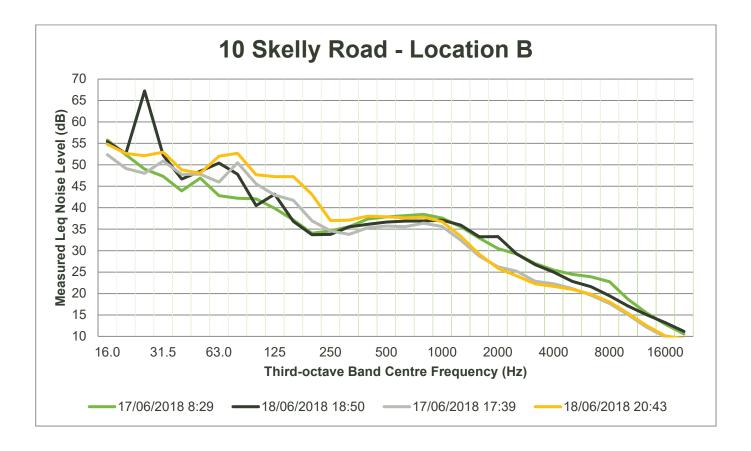
Based on the noise predictions resulting noise from the operation of trucks/ light commercial vehicles from the Stage 2 KVAR are considered compliant with the Conditions of Approval.

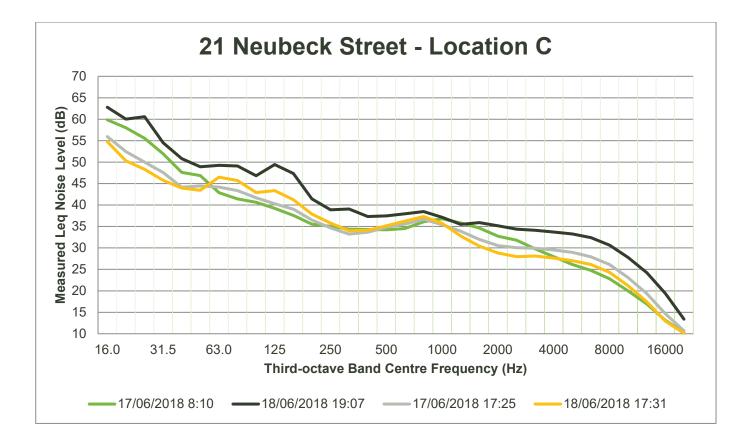
## 7 References

- Kerosene Vale Stage 2 Ash Repository, Operational Environmental Management Plan (OEMP), Parsons Brinckerhoff, April 2009, which includes:
  - Appendix A: KVAR Stage 2 Operations, Operational Noise and Vibration Management Plan (ONVMP), Parsons Brinckerhoff, April 2009
- Project Approval (PA), Application: No 07\_0005, Delta Electricity, 26 November 2008, Department of Planning
- Stage 2 Kerosene Vale Ash Repository operational noise review, Parsons Brinckerhoff, September 2009.
- Office of Environment & Heritage (OEH) Interim Construction Noise Guideline (ICNG).
- Office of Environment & Heritage (OEH) Industrial Noise Policy (INP).
- Australian Standard AS 1055 1997: Acoustics Description and measurement of environmental noise.

# Appendix A Measured noise spectra







# Appendix B Glossary of terms

Term	Definition
Sound Pressure Level	Sound or noise is the sensation produced at the ear by very small fluctuations in atmospheric pressure. The human ear responds to changes in sound pressure over a very wide range (from 20 microPascals to 60 Pascals). A scale that compresses this range to a more manageable size and that is best matched to subjective response is the logarithmic scale, rather than a linear scale.
Sound Pressure Level (Lp)	Is defined as: $L_{P} = 10 \log_{10} \left( \frac{p^{2}}{p_{ref}^{2}} \right) dB$ In the above equation, <i>p</i> is the sound pressure fluctuation (above or below atmospheric pressure), and <i>p</i> <sub>ref</sub> is 20 microPascals (2 x 10 <sup>-5</sup> Pa), the approximate threshold of hearing. To avoid a scale which is too compressed, a factor of 10 is included, giving rise to the decibel, or dB for short.
A-Weighted Decibel (dB(A)) & Loudness	In some circumstances, the sound pressure level is expressed as C- Weighted decibels, instead of the more common A-Weighted. The C- Weighting filter is designed to replicate the response of the human ear above 85 dB, and places a greater weighting on low frequency noise.
LAeq	The time averaged C-weighted sound pressure level for a time interval, as defined in AS1055.1. It is generally described as the equivalent continuous C-weighted sound pressure level that has the same mean square pressure level as a sound that varies over time. It can be considered as the average sound pressure level over the measurement period.
L <sub>Ceq</sub>	The time averaged C-weighted sound pressure level for a time interval, as defined in AS1055.1. It is generally described as the equivalent continuous C-weighted sound pressure level that has the same mean square pressure level as a sound that varies over time. It can be considered as the average sound pressure level over the measurement period.
L <sub>An</sub>	The sound level, which, for a specified time interval, in relation to an investigation of a noise, means the A-weighted sound pressure level that is equalled or exceeded for n% of the interval. Commonly used percentages are 1, 10, 90 & 99%.

Term	Definition		
L <sub>Cpk</sub>	The peak C-weighted sound pressure level for a time interval.		
L <sub>Cmax,T</sub>	The average maximum C-weighted sound pressure level, which, for the specified time interval, means the C-weighted sound pressure level during the interval obtained by using the fast time weighting and arithmetically averaging the maximum sound levels of the noise during the interval. Under certain conditions the 10th percentile noise level, L <sub>C10,T</sub> , can represent the average maximum C-weighted sound pressure level.		
L <sub>A10</sub>	A-weighted noise level which is exceeded for only 10% of the measuring period. It is usually used as the descriptor for intrusive noise level and represents ambient road traffic noise in general.		
L <sub>A90</sub>	A-weighted noise level which is exceeded for 90% of the measuring period. It is usually used as the descriptor for background noise level during the measurement period.		
Lamin	Minimum A-weighted noise level detected during the measuring period. It refers to the minimum background noise detected.		
Octave	Frequency bands allow a representation of the spectrum associated with a particular noise. They are an octave wide, meaning that the highest frequency in the band is just twice the lowest frequency, with all intermediate frequencies included and all other frequencies excluded. Each octave band is described by its centre frequency.		
Maximum Exposure Time (Hours)	The maximum possible time a person can be safely exposed to a specific noise level ( $\ensuremath{L_{Aeq}}\xspace$ ).		
Sound Exposure Level (SEL)	Sound exposure level abbreviated as SEL and L <sub>AE</sub> , is the total noise energy produced from a single noise event. The Sound Exposure Level is a metric used to describe the amount of noise from an event such as an individual aircraft flyover. It is computed from measured dB(A) sound levels. The Sound Exposure Level is the integration of all the acoustic energy contained within the event.		

# Appendix C Site photograph



Figure 3 | Location D

# Appendix D Weather data

#### Table 7: Meteorological conditions during noise survey

Date	Time	Rainfall (mm)	Wind Speed 10m above ground (m/s)	Wind Direction (deg.)	Temp (°C)	Relative humidity (%)
17/06/2018	0:00	0.0	2.2	244	1.9	94
17/06/2018	0:15	0.0	1.2	186	1.6	94
17/06/2018	0:30	0.0	3.1	239	1.0	92
17/06/2018	0:45	0.0	3.9	261	2.2	90
17/06/2018	1:00	0.0	3.9	254	2.2	89
17/06/2018	1:15	0.0	4.7	255	2.3	88
17/06/2018	1:30	0.0	4.4	251	2.0	89
17/06/2018	1:45	0.0	4.5	254	2.2	90
17/06/2018	2:00	0.0	3.7	251	2.0	91
17/06/2018	2:15	0.0	3.9	253	1.8	92
17/06/2018	2:30	0.0	3.7	249	1.9	91
17/06/2018	2:45	0.0	3.5	247	1.9	90
17/06/2018	3:00	0.0	3.4	249	1.9	89
17/06/2018	3:15	0.0	2.9	258	1.7	88
17/06/2018	3:30	0.0	1.1	226	1.4	89
17/06/2018	3:45	0.0	1.1	235	1.1	90
17/06/2018	4:00	0.0	1.8	249	1.4	91
17/06/2018	4:15	0.0	2.0	271	1.6	91
17/06/2018	4:30	0.1	2.2	265	1.4	95
17/06/2018	4:45	0.0	1.3	216	1.4	96
17/06/2018	5:00	0.1	1.2	221	1.1	97
17/06/2018	5:15	0.0	0.8	144	0.8	98
17/06/2018	5:30	0.0	0.9	199	0.4	99
17/06/2018	5:45	0.0	2.1	281	0.5	99

						Deleti
Date	Time	Rainfall (mm)	Wind Speed 10m above ground (m/s)	Wind Direction (deg.)	Temp (°C)	Relative humidity (%)
17/06/2018	6:00	0.0	3.9	261	1.1	98
17/06/2018	6:15	0.0	4.3	260	1.1	96
17/06/2018	6:30	0.0	4.0	260	0.9	98
17/06/2018	6:45	0.0	3.3	254	0.9	98
17/06/2018	7:00	0.0	4.0	259	1.0	98
17/06/2018	7:15	0.1	2.7	266	0.9	98
17/06/2018	7:30	0.1	4.1	270	0.9	98
17/06/2018	7:45	0.1	5.9	266	1.0	97
17/06/2018	8:00	0.1	4.2	270	0.8	98
17/06/2018	8:15	0.1	3.1	273	0.9	98
17/06/2018	8:30	0.1	3.7	270	1.1	96
17/06/2018	8:45	0.1	3.3	263	1.2	94
17/06/2018	9:00	0.0	1.3	198	1.2	95
17/06/2018	9:15	0.0	1.7	219	1.4	95
17/06/2018	9:30	0.0	3.9	262	1.5	94
17/06/2018	9:45	0.0	3.5	275	1.6	94
17/06/2018	10:00	0.0	3.8	266	1.9	93
17/06/2018	10:15	0.0	3.1	252	2.0	92
17/06/2018	10:30	0.0	4.3	264	2.3	90
17/06/2018	10:45	0.0	3.5	271	2.5	90
17/06/2018	11:00	0.0	4.6	270	2.6	89
17/06/2018	11:15	0.0	4.0	256	2.7	87
17/06/2018	11:30	0.0	4.1	268	2.6	88
17/06/2018	11:45	0.0	3.6	267	2.7	87
17/06/2018	12:00	0.0	4.3	263	2.8	88
17/06/2018	12:15	0.1	4.5	262	2.9	87
17/06/2018	12:30	0.0	5.7	263	3.0	87
17/06/2018	12:45	0.0	5.3	271	2.9	89
17/06/2018	13:00	0.0	4.8	265	3.1	90
17/06/2018	13:15	0.0	5.5	268	3.0	90
17/06/2018	13:30	0.0	4.6	265	2.9	91
17/06/2018	13:45	0.0	5.2	265	2.9	92
17/06/2018	14:00	0.0	4.9	276	2.8	92
17/06/2018	14:15	0.0	4.1	278	2.8	93
17/06/2018	14:30	0.0	5.0	269	2.9	93

Date	Time	Rainfall (mm)	Wind Speed 10m above ground (m/s)	Wind Direction (deg.)	Temp (°C)	Relative humidity (%)
17/06/2018	14:45	0.0	4.3	273	3.2	91
17/06/2018	15:00	0.0	4.4	274	3.3	90
17/06/2018	15:15	0.0	4.2	270	3.5	89
17/06/2018	15:30	0.0	4.3	283	3.5	89
17/06/2018	15:45	0.0	4.0	278	3.5	89
17/06/2018	16:00	0.0	4.7	278	3.5	89
17/06/2018	16:15	0.0	4.0	278	3.5	88
17/06/2018	16:30	0.0	3.8	278	3.5	88
17/06/2018	16:45	0.0	4.5	271	3.3	91
17/06/2018	17:00	0.0	3.9	272	3.4	91
17/06/2018	17:15	0.0	5.2	276	3.4	90
17/06/2018	17:30	0.0	4.9	278	3.2	91
17/06/2018	17:45	0.0	4.9	280	3.0	93
17/06/2018	18:00	0.0	4.1	267	3.0	93
17/06/2018	18:15	0.0	3.1	276	2.8	95
17/06/2018	18:30	0.0	3.6	261	2.7	95
17/06/2018	18:45	0.1	4.6	267	2.6	95
17/06/2018	19:00	0.0	2.9	287	2.4	96
17/06/2018	19:15	0.0	2.7	286	2.3	97
17/06/2018	19:30	0.1	2.0	284	2.4	98
17/06/2018	19:45	0.0	3.0	271	2.5	97
17/06/2018	20:00	0.0	3.1	279	2.6	97
17/06/2018	20:15	0.0	3.2	276	2.5	97
17/06/2018	20:30	0.0	2.2	260	2.5	97
17/06/2018	20:45	0.0	2.8	266	2.5	98
17/06/2018	21:00	0.0	2.7	281	2.6	98
17/06/2018	21:15	0.0	2.4	297	2.6	98
17/06/2018	21:30	0.0	2.4	275	2.8	99
17/06/2018	21:45	0.0	2.2	288	2.9	99
17/06/2018	22:00	0.1	2.1	279	3.0	99
17/06/2018	22:15	0.0	1.8	260	3.1	99
17/06/2018	22:30	0.0	3.0	275	3.3	99
17/06/2018	22:45	0.0	2.0	276	3.3	98
17/06/2018	23:00	0.0	3.0	266	3.3	98
17/06/2018	23:15	0.1	2.8	266	3.4	98

Date	Time	Rainfall (mm)	Wind Speed 10m above ground (m/s)	Wind Direction (deg.)	Temp (°C)	Relative humidity (%)
17/06/2018	23:30	0.0	1.9	255	3.4	98
17/06/2018	23:45	0.0	2.4	270	3.4	98
18/06/2018	0:00	0.0	2.2	254	3.4	98
18/06/2018	0:15	0.0	2.7	250	3.8	96
18/06/2018	0:30	0.0	3.0	264	3.9	96
18/06/2018	0:45	0.0	2.0	268	3.8	96
18/06/2018	1:00	0.0	3.1	253	3.9	96
18/06/2018	1:15	0.0	4.4	252	3.8	96
18/06/2018	1:30	0.0	4.6	250	3.8	97
18/06/2018	1:45	0.0	4.7	248	3.9	96
18/06/2018	2:00	0.0	3.3	242	3.9	96
18/06/2018	2:15	0.0	2.0	220	4.0	96
18/06/2018	2:30	0.0	2.2	211	4.0	96
18/06/2018	2:45	0.0	3.3	233	3.9	95
18/06/2018	3:00	0.0	3.7	232	3.8	95
18/06/2018	3:15	0.0	3.5	229	3.8	95
18/06/2018	3:30	0.0	3.9	224	3.7	95
18/06/2018	3:45	0.0	4.5	228	3.9	94
18/06/2018	4:00	0.0	3.9	230	3.9	93
18/06/2018	4:15	0.0	3.6	219	3.8	93
18/06/2018	4:30	0.0	3.8	220	3.8	93
18/06/2018	4:45	0.0	3.2	220	3.7	93
18/06/2018	5:00	0.0	2.9	212	3.6	92
18/06/2018	5:15	0.0	2.0	190	3.7	90
18/06/2018	5:30	0.0	2.6	230	3.8	90
18/06/2018	5:45	0.0	3.2	231	3.9	90
18/06/2018	6:00	0.0	3.1	227	4.0	90
18/06/2018	6:15	0.0	3.6	206	3.9	89
18/06/2018	6:30	0.0	2.8	200	4.0	89
18/06/2018	6:45	0.0	3.7	214	4.0	89
18/06/2018	7:00	0.0	4.0	215	3.9	90
18/06/2018	7:15	0.0	2.8	206	3.8	90
18/06/2018	7:30	0.0	2.7	204	3.8	91
18/06/2018	7:45	0.0	3.2	211	3.8	90
18/06/2018	8:00	0.0	3.9	220	4.0	90

Date	Time	Rainfall (mm)	Wind Speed 10m above ground	Wind Direction	Temp	Relative humidity
		(mm)	(m/s)	(deg.)	(°C)	(%)
18/06/2018	8:15	0.0	3.4	220	4.3	89
18/06/2018	8:30	0.0	4.9	223	4.6	88
18/06/2018	8:45	0.0	5.7	227	4.8	87
18/06/2018	9:00	0.0	5.5	220	4.9	87
18/06/2018	9:15	0.0	4.9	211	5.7	83
18/06/2018	9:30	0.0	4.4	212	5.8	83
18/06/2018	9:45	0.0	4.1	209	6.4	81
18/06/2018	10:00	0.0	4.3	215	6.0	84
18/06/2018	10:15	0.0	4.3	221	6.0	84
18/06/2018	10:30	0.0	4.4	222	6.8	82
18/06/2018	10:45	0.0	4.1	216	7.7	79
18/06/2018	11:00	0.0	5.6	220	7.6	78
18/06/2018	11:15	0.0	4.8	221	7.9	76
18/06/2018	11:30	0.0	4.4	217	8.3	75
18/06/2018	11:45	0.0	4.4	227	8.6	74
18/06/2018	12:00	0.0	4.9	219	8.7	71
18/06/2018	12:15	0.0	5.1	218	8.5	71
18/06/2018	12:30	0.0	4.9	213	8.6	72
18/06/2018	12:45	0.0	5.4	215	9.0	68
18/06/2018	13:00	0.0	5.5	219	8.4	71
18/06/2018	13:15	0.0	4.8	214	9.0	70
18/06/2018	13:30	0.0	5.3	216	9.2	68
18/06/2018	13:45	0.0	5.2	218	8.8	69
18/06/2018	14:00	0.0	5.5	220	9.1	69
18/06/2018	14:15	0.0	4.8	223	9.3	68
18/06/2018	14:30	0.0	4.8	223	8.8	71
18/06/2018	14:45	0.0	4.5	224	8.9	72
18/06/2018	15:00	0.0	4.1	223	8.6	74
18/06/2018	15:15	0.0	3.7	223	8.1	76
18/06/2018	15:30	0.0	4.5	228	7.6	79
18/06/2018	15:45	0.0	4.7	229	7.3	81
18/06/2018	16:00	0.0	3.5	222	7.7	80
18/06/2018	16:15	0.0	4.2	221	7.0	81
18/06/2018	16:30	0.0	3.5	218	6.3	85
18/06/2018	16:45	0.0	3.9	223	6.1	87

Date	Time	Rainfall (mm)	Wind Speed 10m above ground (m/s)	Wind Direction (deg.)	Temp (°C)	Relative humidity (%)
18/06/2018	17:00	0.0	4.0	218	6.0	87
18/06/2018	17:15	0.0	3.5	222	5.5	90
18/06/2018	17:30	0.0	3.9	221	5.4	91
18/06/2018	17:45	0.0	3.6	224	5.3	91
18/06/2018	18:00	0.0	2.3	226	5.1	91
18/06/2018	18:15	0.0	1.9	198	4.8	92
18/06/2018	18:30	0.0	2.8	223	5.1	92
18/06/2018	18:45	0.0	2.9	220	5.4	90
18/06/2018	19:00	0.0	2.9	221	5.2	90
18/06/2018	19:15	0.0	2.4	212	5.1	91
18/06/2018	19:30	0.0	3.5	205	5.1	92
18/06/2018	19:45	0.0	3.6	222	5.3	92
18/06/2018	20:00	0.0	2.8	228	5.2	94
18/06/2018	20:15	0.0	2.2	220	5.2	95
18/06/2018	20:30	0.0	2.0	222	5.3	94
18/06/2018	20:45	0.0	1.8	220	5.4	93
18/06/2018	21:00	0.0	1.9	220	5.2	95
18/06/2018	21:15	0.0	2.3	214	5.1	94
18/06/2018	21:30	0.0	2.1	204	5.1	92
18/06/2018	21:45	0.0	2.1	206	5.3	91
18/06/2018	22:00	0.0	3.2	214	5.2	91
18/06/2018	22:15	0.0	3.9	213	5.1	87
18/06/2018	22:30	0.0	2.9	196	4.9	83
18/06/2018	22:45	0.0	1.9	188	4.6	84
18/06/2018	23:00	0.0	2.1	173	4.3	86
18/06/2018	23:15	0.0	1.7	191	3.7	87
18/06/2018	23:30	0.0	2.1	220	3.2	89
18/06/2018	23:45	0.0	2.0	226	3.0	88

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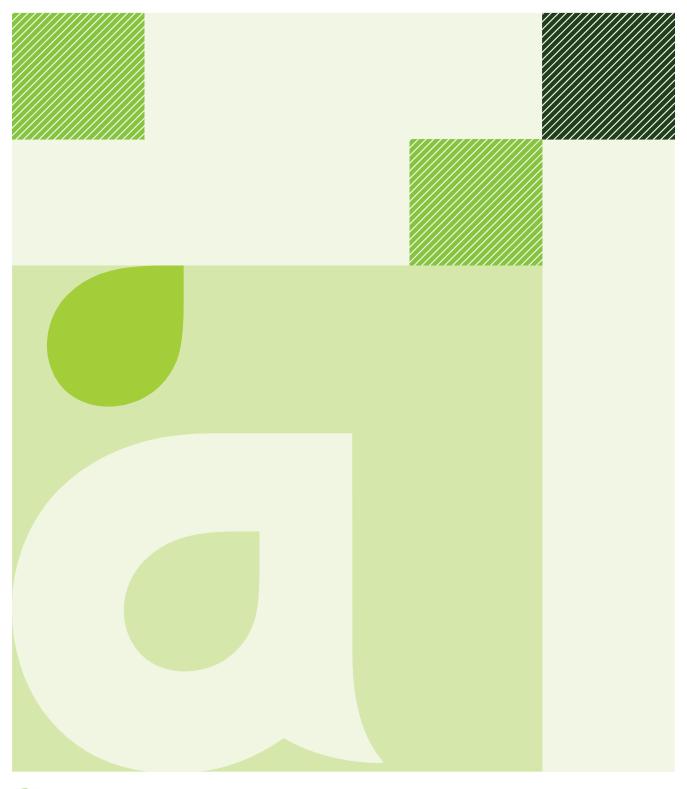
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Annual Environmental Management Report Wallerawang Ash Dam Area 2018 - 2019

# Appendix C KVAR Stage 2 Noise Report – October 2018



# aurecon

**Project:** Kerosene Vale Ash repository Stage 2

Ongoing operational noise measurements (Oct 2018)

**Prepared for:** EnergyAustralia NSW

Project: 247023

1 November 2018

# **Document control record**

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Report Title Ongoing operational noise measurements (Oct 2018)					3)		
Docu	ment ID	247023-KV-REP-13-REV1	Project Numb	ber	247023		
File P	Path	\\Aurecon.info\Shares\AUSYD\Projects\BG\247023\3.Project Delivery\12.Deliverables\Acoustics\181101_October 2018 Survey\Report\KVAR Compliance Noise Oct 2018 rev1.docx					
Clien	t	EnergyAustralia NSW	Client Contact An		Anthony N	nthony Nolan	
Rev	Date	Revision Details/Status	Prepared by	Author	Verifier	Approver	
1	1 November 2018	Final Issue	AL	AL	НМ	LT	
Current Revision 2							

Approval						
Author Signature	this	Approver Signature				
Name	Akil Lau	Name	Les Thorpe			
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Glossary of terms

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# 1 Introduction

Aurecon was engaged by EnergyAustralia NSW to carry out ongoing operational noise monitoring for the Kerosene Vale Stage 2 Ash Repository (KVAR) located in Wallerawang, NSW in accordance with Project Approval Application No. 07\_0005. The noise measurements were carried out on Sunday 28 October 2018 and Monday 29 October 2018, during the early morning and evening periods as per the requirements outlined in the KVAR Stage 2 Operational Noise and Vibration Management Plan (ONVMP).

## 1.1 Site details

The project site consists of an Ash Repository which services the nearby Wallerawang Power Station (WPS). During normal operation of the KVAR Stage 2, the following major noise emissions would be expected.

- Unloading of ash from trucks at the repository.
- Placement and handling of ash at the repository site.
- Operation of trucks on the private haulage road; this includes trucks leaving WPS loaded with ash (travelling north) and returning from the repository empty (travelling south).
- Water pumps operating at the repository.
- Water cart driving around.

WPS is currently being decommissioned, and as such KVAR is no longer fully operational. No noise emissions from the location of the KVAR was evident during the current site visit.

Figure 1 shows the site layout and location of sensitive receivers relative to the major noise sources which include the decommissioned WPS, as well as major roads in the area. Table 1 outlines the most affected sensitive receivers and their distance to the haulage road.

Representative sensitive receiver	Distance to haulage road (meters)*
60 Skelly Road	300
10 Skelly Road	270
21 Neubeck Street	145

#### Table 1: Representative sensitive receivers

Note \* - distance relates to the property boundary or a point 30 m from the dwelling location

It should be noted that coal supply trucks also utilise the private haulage road. Their noise impacts are not considered to be part of the Stage 2 KVAR works and thus their noise impact is outside the scope of this report. While undertaking noise measurements it is extremely difficult to visually distinguish between coal supply trucks and ash trucks, therefore, for the purpose of prediction of noise emissions from ash trucks alone, EnergyAustralia NSW provides the number of truck movements for the periods of measurement.

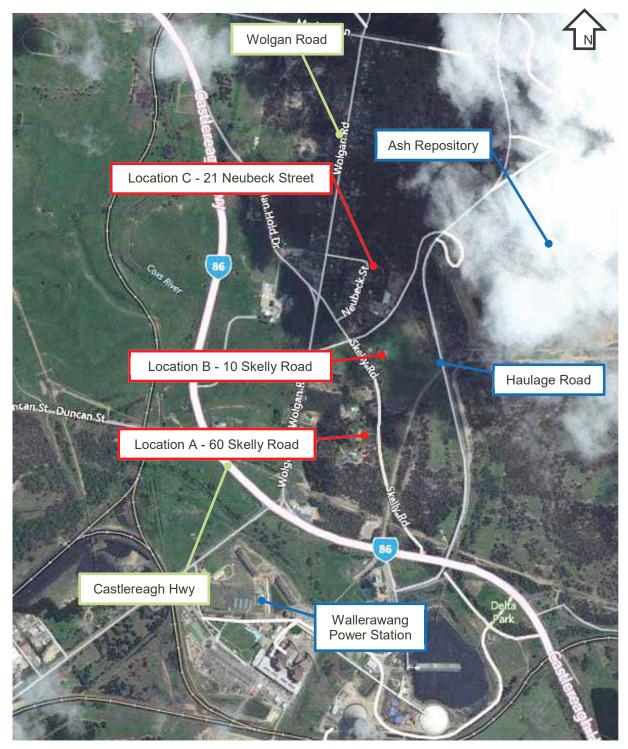


Figure 1 | Site details

## 2 Noise criteria

The applicable operational noise criteria are outlined in the Project Approval, Application No. 07\_0005. The criteria are summarised in Condition 2.15 as follows:

2.15 The cumulative operational noise from the ash placement area and ash haulage activity shall not exceed a  $L_{Aeq}$  (15 minute) of 40 dB(A) at the nearest most affected sensitive receiver during normal operating hours as defined in condition 2.8.

This criterion applies under the following meteorological conditions:

- a) Wind speeds up to 3 m/s at 10 meters above ground<sup>1</sup>; and/or
- b) Temperature inversion conditions of up to 3°C/100 m and source to receiver gradient winds of up to 2 m/s at 10 m above ground level

Normal operating hours in accordance with Conditions 2.8 are 7:00 am to 10:00 pm Monday to Sunday.

## 3 Noise measurements

### 3.1 Measurement methodology

Two types of measurements were carried out during the current monitoring period:

- Ambient noise measurements and
- Sound exposure level measurements.

The measurements were carried out on Sunday 28 October 2018 and Monday 29 October 2018, during the early morning and evening periods, when the noise impacts are likely to be the most significant.

#### Ambient noise measurements

The ambient compliance noise measurements were conducted using a Larson Davis 831 Type 1 sound level meter which was set to 'A' frequency weighting, 'F' time weighting, and was fitted with an approved windshield. Measurements were typically taken at a height of 1.2 metres and at least 3.5 metres from any reflecting structure other than the ground.

Measurements were undertaken for a period of 15 minutes at each of the selected measurement locations (See Table 2). A Larson Davis CAL200 was utilised to calibrate the sound level meters before and after each series of measurements. No significant calibration drift was noted.

#### Weather conditions

The weather during the ambient noise logging can be summarised as sunny conditions, and wind speeds were less than 3 m/s at ground level. Measurements were generally taken in accordance with the Australian Standard *AS 1055.1 1997: Acoustics – Description and measurement of environmental noise*. Refer to Appendix D for weather summary.

<sup>&</sup>lt;sup>1</sup> As per AS 1055.1 – 1997, noise measurements should be avoided when maximum windspeed exceed 5 m/s at the microphone position.

#### Sound exposure level (SEL) measurements

The Sound Exposure Level (SEL) measurements were also carried out using the Larson Davis 831 Type 1 sound level meter. SEL is the equivalent one second A-weighted sound level which produces the same sound energy as an actual identified event. The SEL measurement was commenced when a truck/ light vehicle was observed to pass a nominated reference location and stopped when the end of the truck passed a second nominated reference location. The nominated reference locations were identified where the truck could be visually observed.

### 3.2 Measurement locations

The measurement locations were chosen to represent the three most affected sensitive receivers as outlined in the ONVMP and shown in Table 1. These three receivers were identified based on the information in the Stage 2 Kerosene Vale Ash Repository operational noise review.

Due to the high background noise levels at each of the three monitoring locations it was difficult to assess individual truck noise events. A fourth noise monitoring location identified as Location D and shown in Appendix C, was selected closer to the haulage route to measure individual truck pass-by events. Table 2 and Figure 2 outline the noise measurement locations.

Measurement location	Measurement distance to haulage road (meters)	Representative sensitive receiver
Α	300	60 Skelly Road
В	270	10 Skelly Road
С	145	21 Neubeck Street
D	80	-

Table 2: Representative noise measurement location	s
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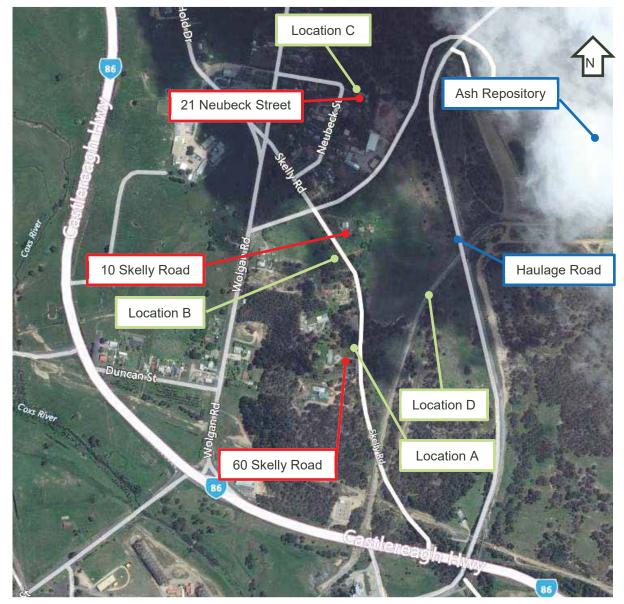


Figure 2 | Noise measurement locations

## 3.3 Conditions during measurements

### 3.3.1 Operating conditions

EnergyAustralia NSW stated that no trucks were operating during any of the measurement periods.

### 3.3.2 Meteorological conditions

The meteorological conditions applicable to the noise survey period are based on meteorological data provided at 15 minute intervals from the Mt Piper weather station.

### 3.4 Results

#### 3.4.1 Ambient noise measurements

The results from the 15-minute ambient noise measurements at each of the measurement locations are shown in Table 3.

u		Time	Measured sound pressure level dB(A)				ure	Predicted noise	Number of truck Pass-bys and direction of travel <sup>1</sup>		
Location	Date of measurement		L <sub>Aeq</sub> #	LAmax*	LAmin**	LA10^^	L <sub>A90</sub> ^	contributi on by KVAR (dBA)	North	South	Total
	Sunday	8:56	39	68	32	39	34	0	0	0	0
60 Skelly Road (A)	28/10/2018	21:12	48	75	32	43	35	0	0	0	0
60 S Roa	Monday 29/10/2018	9:26	37	63	29	38	31	0	0	0	0
		20:58	42	56	34	44	36	0	0	0	0
	Sunday 28/10/2018	8:23	43	69	30	42	33	0	0	0	0
10 Skelly Road (B)		18:50	39	62	32	40	34	0	0	0	0
10 S Roa	Monday 29/10/2018	9:11	40	65	29	40	31	0	0	0	0
		20:42	42	63	36	43	38	0	0	0	0
× ~	Sunday 28/10/2018	7:50	44	65	29	47	34	0	0	0	0
Neubeck reet (C )		19:07	40	57	27	44	32	0	0	0	0
	Monday	8:53	42	61	26	45	30	0	0	0	0
21 St	29/10/2018	20:24	42	57	34	44	37	0	0	0	0

Note : <sup>1</sup> - Truck counts include ash trucks and light commercial vehicles.

Exceedances of the  $L_{Aeq (15 min)}$  of 40 dB(A) are shown in Bold.

<sup>#</sup> L<sub>Aeq</sub> refers to A-weighted equivalent continuous sound pressure level over measurement period. It is used to quantify the average noise level over a time period.

- \* *L<sub>Amax</sub>* refers to the maximum A-weighted noise level detected during the measuring period. It refers to the maximum background noise detected.
- \*\* L<sub>Amin</sub> refers to the minimum A-weighted noise level detected during the measuring period. It refers to the minimum background noise detected.
- \* L<sub>A10</sub> refers to the A-weighted noise level which is exceeded for only 10% of the measuring period. It is usually used as the descriptor for intrusive noise level and represents ambient road traffic noise in general.
- L<sub>A90</sub> refers to the A-weighted noise level which is exceeded for 90% of the measuring period. It is usually used as the descriptor for background noise level during the measurement period.

The measured  $L_{Aeq (15 min)}$  exceeded the assessment criteria of  $L_{Aeq (15 min)}$  of 40 dB(A) during all of the attended noise monitoring events. As there were no truck movements associated with the operation of the KVAR during the attended noise monitoring event, it can be assumed that the KVAR operations did not contribute to the background noise levels at any of the measurement locations and that the high noise levels are associated with local noise events such as traffic from surrounding roads and birds/insects. Noise contribution from the KVAR is therefore considered to be 0 dBA.

### 3.4.2 SEL measurements

The individual truck pass-by noise event (SEL) measurements at Location D (approximately 80 meters from the haulage road) were conducted on 7 November 2011, 21 April 2013 and 31 March 2014. The results are summarised in Table 4. The number of actual truck pass-bys counted during the daytime survey are also summarised in Table 4. These data were used to predict the noise impact from the truck movement on the sensitive receivers.

Based on the visual site inspection, the grade (slope) of the haulage road rises from south to north. The trucks moving in the northerly direction on the haulage road appear to rev the engine more compared to the trucks moving in the opposite direction and thereby producing a marginally higher SEL as evident in the results summarised in Table 4.

Date	Truck travelling direction	Average event duration (sec)	Average SEL dB(A)	No. of valid truck event measurements
7/11/2011	South	28.9	68	8
//11/2011	North	18.1	70	9
21/04/2013	South	24.0	67	5
21/04/2013	North	19.5	70	7
31/04/2014	South	27.7	69	2
31/04/2014	North	28.3	70	2

#### Table 4: SEL noise measurement results at Location D

## 4 Noise assessment

General observation regarding the ambient noise environment, as well as the truck movements and ash repository operations, during the attended noise measurements are described as follows.

- Operational noise from the KVAR site and the truck engine noise was inaudible at the sensitive receiver locations during the attended noise measurements and no ash trucks or light commercial vehicles were visible on the haul road.
- The noise levels at all locations were affected by background noise sources such as bird/insects, domestic animals and domestic noise. Background noise at all sites was dominated by the intermittent traffic noise from nearby Castlereagh Highway and Wolgan Road.

General observations for the three monitoring locations are described below.

### 4.1 Location A (60 Skelly Road)

The background noise contributions at Location A were predominantly from the traffic noise from Castlereagh Highway and distant traffic. Faint and intermittent traffic noise from Wolgan Road was also audible.



The haulage road was clearly visible from this location, however no coal or ash trucks were visible on the haulage road during the attended noise monitoring period Noise from birds and insects also contributed to the ambient noise at this location.

As shown in Table 3, the background noise varied over the two days with  $L_{A90}$  ranging from 31 dB(A) to 36 dB(A). The background noise ( $L_{A90}$ ) during the attended noise measurements was predominantly due to road traffic on the Castlereagh Highway, Wolgan Road and other nearby roads.

## 4.2 Location B (10 Skelly Road)

Contributions to the background noise at Location B were predominantly from birds/insects/animals and traffic on Wolgan Road and Skelly Road.

Traffic noise from Wolgan Road and Skelly Road was clearly audible at this location and also contributed to the ambient noise levels.

The haulage road was clearly visible from this measuring location, however no coal or ash trucks were visible on haulage road during the attended noise monitoring period movement.

Background noise levels was fairly consistent over the two days with  $L_{A90}$  ranging from 31 dB(A) to 38dB(A).

## 4.3 Location C (21 Neubeck Street)

Contributions to the background noise at Location C were predominantly from birds/insects/animals and distant traffic on Wolgan Road and other roads. Traffic noise from Wolgan Road was clearly audible and also contributed to the ambient noise levels.

The haulage road was not clearly visible from this location because of an earth mound and heavy vegetation blocking the line of sight; however no truck engine noise was audible during the attended noise monitoring period.

Background noise varied over the two days with LA90 ranging from 32 dB(A) to 37 dB(A).

## 4.4 Location D

The noise data collected at Location D (Figure 2 and Appendix C) measured the SEL of individual truck pass-by events on 7 November 2011, 22 April 2013 and 31 April 2014 (See Table 4).

This location is closest to the haulage road and as such, each truck pass-by was the dominant noise source (clearly audible above other ambient noise sources) during these monitoring events.

# 5 Analysis and recommendations

## 5.1 Data analysis

As can be observed from the summary of noise measurements presented above, the existing ambient noise levels  $L_{Aeq (15 min)}$  exceed the assessment criteria of  $L_{Aeq (15 min)}$  of 40 dB(A) on all but three of the monitoring events. This section deals with noise prediction based on the number of truck movements (worst case scenario) for any worst case 15 minute period.

To assess the impact of the ash truck noise emissions, the influence of individual truck pass-by noise events have to be taken into account.  $L_{Aeq (15 min)}$  noise level was predicted based on the SEL measurement results (shown in Table 4) and the number of truck movements provided by EnergyAustralia NSW.

The predicted noise levels take into account the total number of truck pass-bys (including ash trucks and small commercial vehicles) and the distance of the noise source from the receiver. The assessment included the calculated barrier effect (- 2dB(A)) at Location C. This is due to the earth mound located on the northern side of the site which blocks the line of sight between 21 Neubeck Street and the haulage road, therefore attenuating the noise from the haulage road. Generally, trucks operate at a constant rate, with approximately 15-20 minute circuits for each truck. Table 5 provides a summary of truck pass-bys based on information collected during a previous site visit.

	Information collected during site visit on 30-31 March 2014					
Periods	Total number of trucks pass bys per 45 minutes	Average number of trucks pass bys per 15 minutes				
Morning 30/03/2014	7	2.3				
Evening 30/03/2014	2	0.7				
Morning 31/03/2014	7	2.3#				
Evening 31/03/2014	3	1.0				

Table 5: Truck movement data

Note: the figure in **bold** is the worst-case truck movement (most frequent) used to predict the noise contribution from the truck movements (shown in Table 6)

# Maximum number of truck pass-bys as per information collected during the site visit.

As shown in Table 5, the maximum number of truck pass-bys was during the morning period on both 30/03/2014 and 31/03/2014. The lowest truck pass-bys was during the evening period on 30/03/2014. The noise emissions from the KVAR are considered to be below the assessment criteria as they were predominantly inaudible during the noise survey and could not be distinguished.

Table 6 provides the noise predictions from haulage trucks alone at the nearest sensitive receivers based on SEL measurements. The prediction is calculated from the movement of ash trucks based on the worst case scenario (i.e. 2.3 truck pass-bys during any 15 minute period).

Table 6: Noise predictions from truck movements based on SEL measurements

Sensitive receiver	Distance to haulage road (m)	No. of average truck movements per 15min	Predicted contribution L <sub>Aeq (15 min)</sub> (dBA)	Criteria L <sub>Aeq (15 min)</sub> (dBA
60 Skelly Road	300	2.3	32	40
10 Skelly Road	270	2.3	33	40
21 Neubeck Street *	145	2.3	37*	40

Note \* - Includes the barrier attenuation (-2dBA) provided by the earth mound blocking direct line of sight between the residence and haulage road.

Based on the worst case scenario the noise impact from truck movements complies with noise criteria of  $L_{Aeq (15 min)}$  of 40 dB(A) at all the sensitive receiver locations.



There were no truck movements during this current noise monitoring event, therefore the operational noise emissions from the Stage 2 KVAR is considered to be compliant with Condition 2.15 of the Project Approval.

# 6 Conclusion

Aurecon conducted operational noise monitoring for the Stage 2 KVAR located in Wallerawang, NSW. The noise measurements were carried out at the three most affected sensitive receiver locations on Sunday 28 October 2018 and Monday 29 October 2018, in the early morning and evening in accordance with the KVAR Stage 2 ONVMP.

The applicable noise assessment criteria of  $L_{Aeq (15 minute)}$  of 40 dB(A) from all ash haulage and ash placement associated operational noise emissions at the nearest sensitive receivers is outlined in the Project Approval, Application No. 07\_0005.

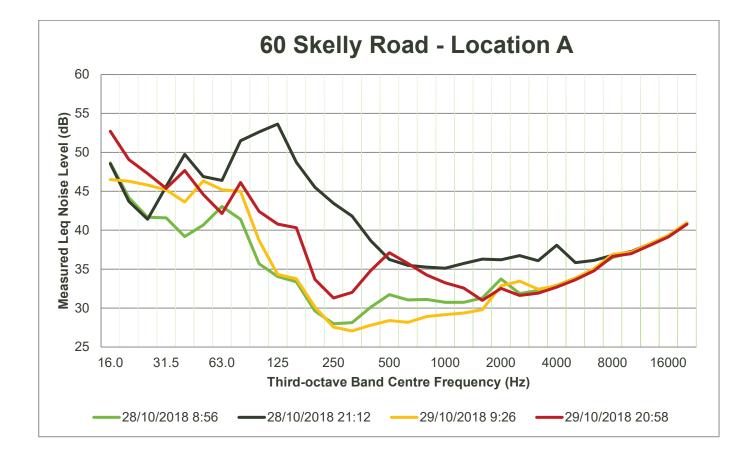
The primary contributor to the background and ambient noise levels at all measurement locations was the traffic noise on the nearby roads.

Based on the noise predictions resulting noise from the operation of trucks/ light commercial vehicles from the Stage 2 KVAR are considered compliant with the Conditions of Approval.

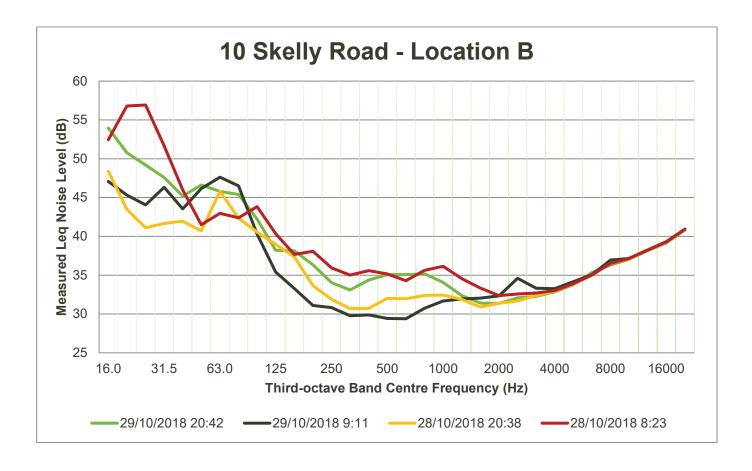
## 7 References

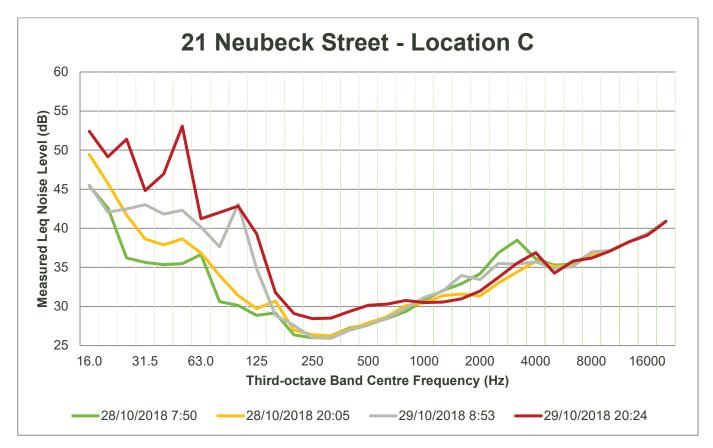
- Kerosene Vale Stage 2 Ash Repository, Operational Environmental Management Plan (OEMP), Parsons Brinckerhoff, April 2009, which includes:
  - Appendix A: KVAR Stage 2 Operations, Operational Noise and Vibration Management Plan (ONVMP), Parsons Brinckerhoff, April 2009
- Project Approval (PA), Application: No 07\_0005, Delta Electricity, 26 November 2008, Department of Planning
- Stage 2 Kerosene Vale Ash Repository operational noise review, Parsons Brinckerhoff, September 2009.
- Office of Environment & Heritage (OEH) Interim Construction Noise Guideline (ICNG).
- Office of Environment & Heritage (OEH) Industrial Noise Policy (INP).
- Australian Standard AS 1055 1997: Acoustics Description and measurement of environmental noise.

# Appendix A Measured noise spectra



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# Appendix B Glossary of terms

Term	Definition			
Sound Pressure Level	Sound or noise is the sensation produced at the ear by very small fluctuations in atmospheric pressure. The human ear responds to changes in sound pressure over a very wide range (from 20 microPascals to 60 Pascals). A scale that compresses this range to a more manageable size and that is best matched to subjective response is the logarithmic scale, rather than a linear scale.			
Sound Pressure Level (Lp)	Is defined as: $L_{p} = 10 \log_{10} \left( \frac{p^{2}}{p_{ref}^{2}} \right) dB$ In the above equation, <i>p</i> is the sound pressure fluctuation (above or below atmospheric pressure), and <i>p<sub>ref</sub></i> is 20 microPascals (2 x 10 <sup>-5</sup> Pa), the approximate threshold of hearing. To avoid a scale which is too compressed, a factor of 10 is included, giving rise to the decibel, or dB for short.			
A-Weighted Decibel (dB(A)) & Loudness	In some circumstances, the sound pressure level is expressed as C- Weighted decibels, instead of the more common A-Weighted. The C- Weighting filter is designed to replicate the response of the human ear above 85 dB, and places a greater weighting on low frequency noise.			
LAeq	The time averaged C-weighted sound pressure level for a time interval, as defined in AS1055.1. It is generally described as the equivalent continuous C-weighted sound pressure level that has the same mean square pressure level as a sound that varies over time. It can be considered as the average sound pressure level over the measurement period.			
L <sub>Ceq</sub>	The time averaged C-weighted sound pressure level for a time interval, as defined in AS1055.1. It is generally described as the equivalent continuous C-weighted sound pressure level that has the same mean square pressure level as a sound that varies over time. It can be considered as the average sound pressure level over the measurement period.			
L <sub>An</sub>	The sound level, which, for a specified time interval, in relation to an investigation of a noise, means the A-weighted sound pressure level that is equalled or exceeded for n% of the interval. Commonly used percentages are 1, 10, 90 & 99%.			

Term	Definition
L <sub>Cpk</sub>	The peak C-weighted sound pressure level for a time interval.
L <sub>Cmax,T</sub>	The average maximum C-weighted sound pressure level, which, for the specified time interval, means the C-weighted sound pressure level during the interval obtained by using the fast time weighting and arithmetically averaging the maximum sound levels of the noise during the interval. Under certain conditions the 10th percentile noise level, $L_{C10,T}$ , can represent the average maximum C-weighted sound pressure level.
L <sub>A10</sub>	A-weighted noise level which is exceeded for only 10% of the measuring period. It is usually used as the descriptor for intrusive noise level and represents ambient road traffic noise in general.
L <sub>A90</sub>	A-weighted noise level which is exceeded for 90% of the measuring period. It is usually used as the descriptor for background noise level during the measurement period.
Lamin	Minimum A-weighted noise level detected during the measuring period. It refers to the minimum background noise detected.
Octave	Frequency bands allow a representation of the spectrum associated with a particular noise. They are an octave wide, meaning that the highest frequency in the band is just twice the lowest frequency, with all intermediate frequencies included and all other frequencies excluded. Each octave band is described by its centre frequency.
Maximum Exposure Time (Hours)	The maximum possible time a person can be safely exposed to a specific noise level ( $\ensuremath{L_{Aeq}}\xspace$ ).
Sound Exposure Level (SEL)	Sound exposure level abbreviated as SEL and L <sub>AE</sub> , is the total noise energy produced from a single noise event. The Sound Exposure Level is a metric used to describe the amount of noise from an event such as an individual aircraft flyover. It is computed from measured dB(A) sound levels. The Sound Exposure Level is the integration of all the acoustic energy contained within the event.

# Appendix C Site photograph



Figure 3 | Location D

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Annual Environmental Management Report Wallerawang Ash Dam Area 2018 - 2019

# Appendix D Water Quality Assessment – June 2019

# Kerosene Vale Ash Dam and Dry Ash Repository

Water Quality Assessment from April 2018 to March 2019 in Relation to the Decommissioned Wallerawang Power Station

# **Energy Australia NSW**

Reference: 502838 Revision: 1 2019-06-24





# **Document control record**

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Repo	rt title	Water Quality Assessment fro Decommissioned Wallerawan			Relation to the	e
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File p	ath	\\Aurecon.info\Shares\AUSYD\Pr Wallerawang Groundwater Annua Reporting\2019\Report\20190624	al Reports\9			rojects\502838 -
Client	:	Energy Australia NSW				
Client	contact		Client refere	nce		
Rev	Date	Revision details/status	Author	Reviewer	Verifier (if required)	Approver
0	2019-05-22	Draft	A. Basson	D. Harris		
1	2019-06-12	Draft (rev 1)	A. Basson	D. Harris		P. Sangarananda
1	2019-06-24	Final	A.Basson	D. Harris		
Curre	nt revision	1				

Approval			
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# **Executive summary**

This annual assessment report contributes to the Annual Environment Management Report (AEMR) for the 2018 / 2019 reporting period for the decommissioned and partly capped Kerosene Vale Ash Repository (KVAR) to address the requirements of the NSW Department of Planning and Environment's Consent Conditions (Condition 7.3 (c), (d) and (e) of Project Approval 07\_0005) for monitoring to be undertaken to ascertain whether there have been any effects of the dry ash placement on the local surface or groundwater quality, pursuant to Conditions 3.4 and 3.5 of Project Approval 07\_0005.

Groundwater and surface water quality signals within / downgradient of the KVAR and surface water (WX7) / groundwater (D5) receiving sites are highly complex spatially and temporally.

Influences on water quality are associated with a number of existing and past land uses including the KVAD, SSCAD, Lidsdale Cut, open cut mining, chitter deposits, underground mining; along with on-site management measures including subsurface drains, pump back systems and discharge from Springvale Mine at LDP009.

Review of both recent (2018-2019) and historical (1991-2019) data for surface water monitoring associated with the KVAR has identified that the KVAR is currently not having a measurable impact on surface water quality in Sawyers Swamp Creek (SSC) at the designated surface water receiving site (WX7/site 41). There appears to be no direct correlation between elevated levels of arsenic and molybdenum in surface waters at WX7 and activities associated with the construction or operation of KVAR or SSCAD. The water quality profile in SSC indicates that the water in the creek is dominated by the discharge water from the adjacent mining activities (LDP009), currently discharging approximately 18MI/d to SSC.

The 95<sup>th</sup> percentile concentrations of water quality parameters within groundwater bore D5 (site 36) currently exceeds the selected WQGVs for Al, B, Cd, Cr, Cu, Fe, Hg, Mn, Ni, Pb and Zn. A number of these exceedances could potentially be attributed to background levels including pH, Al, Cr, Cu, and Pb, as historically they exceeded the WQGV above the ash repository area at site WGM1/D1 (site 32). Results are reflective of water quality contributions from current and historic land use practices. It is possible that the KVAR is contributing to some elevated parameters in groundwater for Bore D5.

Due to the complexity of current and historic land use activities, including local chitter deposits, pumping and discharge regimes for the KVAR and SSCAD, it is not conclusive (based on the data set available) to directly attribute water quality impacts observed in groundwater in Bore D5 solely to a single source such as the KVAR.

Further hydrogeological investigation and modelling would be required to assess the KVAR's and SSCAD's contribution to water quality changes in Bore D5.

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# 1 Introduction

# 1.1 Background

In 2002, Delta Electricity (now EnergyAustralia NSW) obtained approval for conversion of the wet slurry ash placement process at Wallerawang Power Station to dry ash. The dry ash placement is called the Kerosene Vale Ash Repository (KVAR). Stage 1 of the KVAR placement began in 2003 and was completed and capped in February 2009. Approval was obtained for further ash placement in the Stage 2 Area at the KVAR in November 2008. The Stage 2 Area placement began in April 2009 and was ongoing until Wallerawang Power Station, including the Kerosene Vale Ash Repository (KVAR), ceased operation and subsequent ash production in March 2014.

One of the primary objectives of the design and operation of the KVAR is to have no adverse impact on the local ground or surface water quality. More specifically, this means that leachates from the dry ash placement should not increase concentrations of the various water quality characteristics in the receiving waters by more than the locally derived guidelines (which is based on the 90th percentile of the background, pre-placement sites) or the ANZECC (2000) guidelines for protection of aquatic life (whichever is higher).

This report provides an assessment of surface water and groundwater quality for the April 2018 – March 2019 reporting period and considers previous years monitoring results for interpretation of trends.

# **1.2** Site Regulation

The annual assessments of surface water and groundwater quality are undertaken in accordance with the NSW Department of Planning and Environment's Development Consent conditions for the Kerosene Vale Ash Repository outlined in the KVAR Operations Environmental Management Plan, and because the Wallerawang Power Station Environment Protection Licence (EPL) has been retained by EnergyAustralia NSW.

# 1.3 Intended Outcomes

This assessment of groundwater and surface water quality for the decommissioned KVAR includes the following scope of works:

- Discuss the changes (if any) in surface water and groundwater quality as a result of the seepage collection and diversion systems for:
  - Sub-surface drains in the Kerosene Vale Ash Dam (KVAD) under the dry ash Kerosene Vale Ash Repository (KVAR)
  - The Sawyers Swamp Creek Ash Dam (SSCAD) v-notch pump-back system
  - Diversion of the KVAD groundwater to Lidsdale Cut via the unblocked KVAD toe drains
  - Diversion of the Lidsdale Cut discharge from Sawyers Swamp Creek (SSC) to the Sawyers Swamp Creek Ash Dam (SSCAD).
- The effects of the Stage 1 and Stage 2A dry ash placements on surface and groundwater receiving waters with the effects of the local coal mining and the Springvale Mine water discharge considered.

# 1.4 Scope of Works

In accordance with previous reports, the contract and fee proposal, and to meet requirements in response to the NSW Department of Planning and Environment's Development Consent conditions for the Kerosene Vale Ash Repository, the assessment of groundwater and surface water quality for the decommissioned KVAR includes the following scope of works, which are addressed in this report:

- Definition of Water Quality Criteria, Including:
  - ANZECC 2000 Water Quality Guideline Values (WQGVs)
  - Local Water Quality Guidelines Values (WQGVs)
- Assessment of recent (2018-2019) and historic trends in surface water quality data from upstream, downstream and background reference locations summarized in Table 4-1, Section 4.1.1
- Assessment of recent (2018-2019) and historic trends in groundwater quality and level data from upstream, downstream and background reference locations summarized in Table 4-3, Section 4.2.1
- Assessment and summary of groundwater surface water interactions for SSC, and likely effects of groundwater seepage from the KVAR and discharge from Springvale Mine
- Comparison of groundwater and surface water quality monitoring results against ANZECC 2000 95% Species Protection Levels, ANZECC 2000 99% Species Protection Levels (mercury and selenium), and derived local WQGVs

## 1.5 **Previous Reports**

To satisfy project objectives Aurecon has reviewed relevant information from the following existing reports:

- Aurecon (2017): Kerosene Vale Ash Dam and Dry Ash Repository Water Quality Assessment from April 2016 to March 2017 in Relation to the Decommissioned Wallerawang Power Station. Prepared for EnergyAustralia NSW. Rev 1, 16 June 2017. Reference: 256109.
- Aurecon (2016): Kerosene Vale Ash Dam and Dry Ash Repository Water Quality Assessment from April 2015 to March 2016 in Relation to the Decommissioned Wallerawang Power Station. Prepared for EnergyAustralia NSW. Rev 4, 14 November 2016. Reference: 208562.
- Aurecon (2015): Kerosene Vale Ash Dam and Dry Ash Repository Water Quality Assessment from April 2013 to March 2015 in Relation to the Decommissioned Wallerawang Power Station. Prepared for EnergyAustralia NSW. Rev 4, 8 October 2015. Reference: 208562.
- Aurecon (2014): Kerosene Vale Ash Dam and Dry Ash Repository KVAR Stage 2 Water Quality Assessment February 2012 to March 2013. Prepared for EnergyAustralia NSW. 16th January 2014.
- Aurecon (2012): Kerosene Vale Ash Dam and Dry Ash Repository KVAR Stage 2A Water Quality Assessment April 2010 to January 2012. Prepared for Delta Electricity Western 9th October 2012.
- Aurecon (2010): KVAD Stage 2 Water Quality Assessment October 2007 to March 2010. Draft Report Prepared for Delta Electricity Western 18 June 2010.
- EnergyAustralia NSW (2014): Kerosene Vale Ash Repository Stage 2 Annual Environmental Management Report, April 2013 – March 2014. EnergyAustralia NSW, NSW Australia.
- EnergyAustralia NSW (2014): Kerosene Vale Ash Dam and Dry Ash Repository Stage 2 Water Quality Assessment, April 2013 to March 2014. EnergyAustralia NSW, NSW Australia.
- EnergyAustralia NSW (2013): Kerosene Vale Ash Repository Stage 2 Annual Environmental Management Report, April 2012 – March 2013. EnergyAustralia NSW, NSW Australia.
- Delta Electricity (2012): Kerosene Vale Ash Repository Stage 2 Annual Environmental Management Report, May 2011 – April 2012. Delta Electricity NSW, NSW Australia.
- Delta Electricity (2011): Kerosene Vale Ash Repository Stage 2 Annual Environmental Management Report, 2010 – 2011. Delta Electricity NSW, NSW Australia.
- Parsons Brinkerhoff (2010): 1<sup>st</sup> Annual Environmental Management Report for Kerosene Vale Stage 2 Ash Repository Area. Prepared for Delta Electricity. October 2010.

# **1.6** Information Provided by EnergyAustralia NSW

EnergyAustralia NSW has provided copies of the following documents to Aurecon to satisfy the project objectives:

- Surface water quality data from April 2018 to March 2019 from upstream, downstream and background reference locations summarized in Table 4-1, Section 4.1.1
- Groundwater quality and level data from April 2018 to March 2019 from upstream, downstream and background reference locations summarised in Table 4-3, Section 4.2.1

# 1.7 Data Quality

The data contained within this report has been provided to Aurecon by EnergyAustralia NSW. The data was checked for outliers using the ANZECC (2000) (Chapter 6) protocols for data analysis and interpretation.

Care should be exercised in labelling extreme observations as 'outliers', however "on the balance of probabilities, an observation beyond three standard deviations from the mean is likely to be aberrant" (ANZECC, 2000). As such observations beyond three standard deviations that present no rational explanation, such as a shift in environmental conditions, were excluded from the statistical interpretation of recorded data with all exclusions and reasoning for exclusion logged for critical review.

The Operational Environmental Management Plan (OEMP) requires the existing monitoring program to continue, with the addition of low detection limit analysis for trace metals (to ensure that the detection limit is lower than ANZECC 2000, or locally derived WQGVs). With the exception of Silver (Ag) all metals were tested at levels below the WQGVs.

In accordance with ANZECC (2000) guidance (Chapter 6) protocols for data analysis and interpretation, where parameter concentrations have been recorded as less than the laboratory limits of reporting (LOR), the equivalent LOR value has been used as proxy for the parameter concentration for the purpose of statistical assessment.

In house assessment methods<sup>1</sup> based upon the Standard Methods (APHA, 1998) are used for the general water quality characteristics, which include:

 Alkalinity, sulphate, chloride, calcium, magnesium, sodium, potassium, total dissolved solids (TDS) and Turbidity<sup>2</sup> (NTU)

And for trace metals and elements, which include:

Copper, cadmium, chromium, lead, zinc, iron, manganese, mercury, selenium, silver, arsenic, barium, boron and fluoride, molybdenum, nickel and beryllium.

The trace metals and elements monitored are the same for surface and groundwater. Molybdenum, nickel and beryllium have been monitored since July 2007, but beryllium was stopped in April 2010 and aluminium has been monitored since July 2010.

Since April 2006, the laboratory limits of reporting (LOR) for routine monitoring of most trace metals in surface water and groundwater samples were lower than the ANZECC (2000) guidelines. Particular attention has been directed at the trace metals arsenic, cadmium, chromium, copper, mercury, nickel and lead, as well as the trace element selenium, which have been analysed with a low detection limit. However, due to sample matrix interference, silver has continued to be analysed above the ANZECC guideline trigger value of 0.05  $\mu$ g/L since November 2001.

<sup>&</sup>lt;sup>1</sup> Nalco has NATA accreditation Number 1099 and is accredited for ISO/IEC 17025

<sup>&</sup>lt;sup>2</sup> Representative of total suspended solids (TSS, also known as non-filterable residue, NFR) – ANZECC (2000)

# 2 Site Characterisation

# 2.1 Site Location

The Kerosene Vale Ash Repository (KVAR) is owned and operated by EnergyAustralia NSW. The KVAR is located approximately 2.5 kilometres north-east of Wallerawang Power Station and approximately 10 kilometres north-west of the city of Lithgow, which is 150 kilometres north-west of Sydney (Figure 2-1). The KVAR is situated in the centre of the Sawyers Swamp Creek (SSC) catchment, and receives rainfall runoff from the Newnes Plateau and surrounding hillslopes.

# 2.2 Landscape and Geology

The project area is located within the Kerosene Vale valley, which is defined by a drainage basin with a catchment area of approximately 9km<sup>2</sup>. The drainage basin is characterised by an elongate, gently sloping, steep sided valley, through which the Narrabeen group sandstones have been cut, exposing the Permian Illawarra Coal Measures and depositing discrete alluvial sequences.

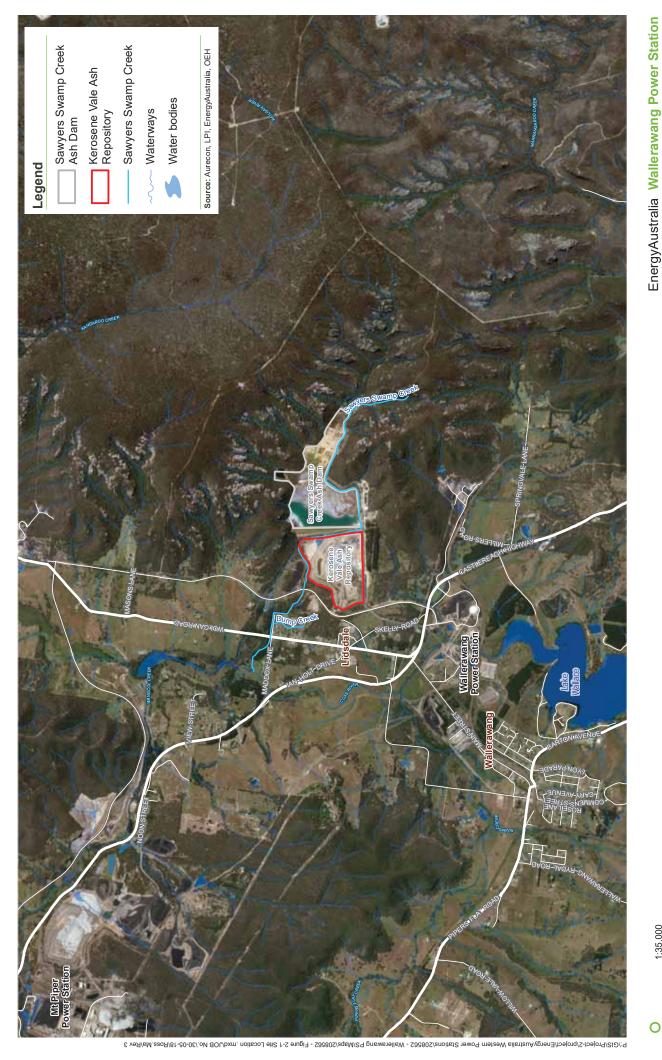
Geological units of the project area are presented in Table 2-1 below, and presented in Figure 2-2 :

Period	Group	Subgroup	Formation	Seam	Approx. Thickness
Regolith / Quaternary	Quaternary	Quaternary	Quaternary Alluvium / Regolith	-	
Triassic	Narrabeen Group	Grose	Banks Wall Sandstone	-	
			Mt York Claystone	-	
			Burra Moko Head Sandstone	-	
			Caley	-	
Permian	Illawarra	Wallerawang	Farmers Creek	Katoomba	
	Coal Measures			Middle River	
		Charbon	Denman	-	
			Irondale Coal	Irondale	1.4 – 1.6
		Cullen Bullen	Lidsdale	Lidsdale	1.4 – 4
			Lithgow	Lithgow	1.1 – 3.7
			Marrangaroo Conglomerate	-	
		Nile Subgroup	Gundangaroo,	-	
			Coorongooba Creek Sandstone,	-	
			Mt Marsden Claystone	-	
	Shoalhaven	Berry Siltstone	-	-	

Table 2-1 Stratigraphic Units – Project Area

Geological units within the immediate project area dip in accordance with the regional profile (moderately towards the east, and to the north). Borehole logs indicate the presence of 3 distinct coal seams, including an upper (shallow) coal seam at approximately 920mAHD below the KVAR, a middle (intermediate) seam at approximately 910mAHD below the KVAR, and a lower coal seam (the Lidsdale Coal Measure) at approximately 900mAHD below the KVAR.



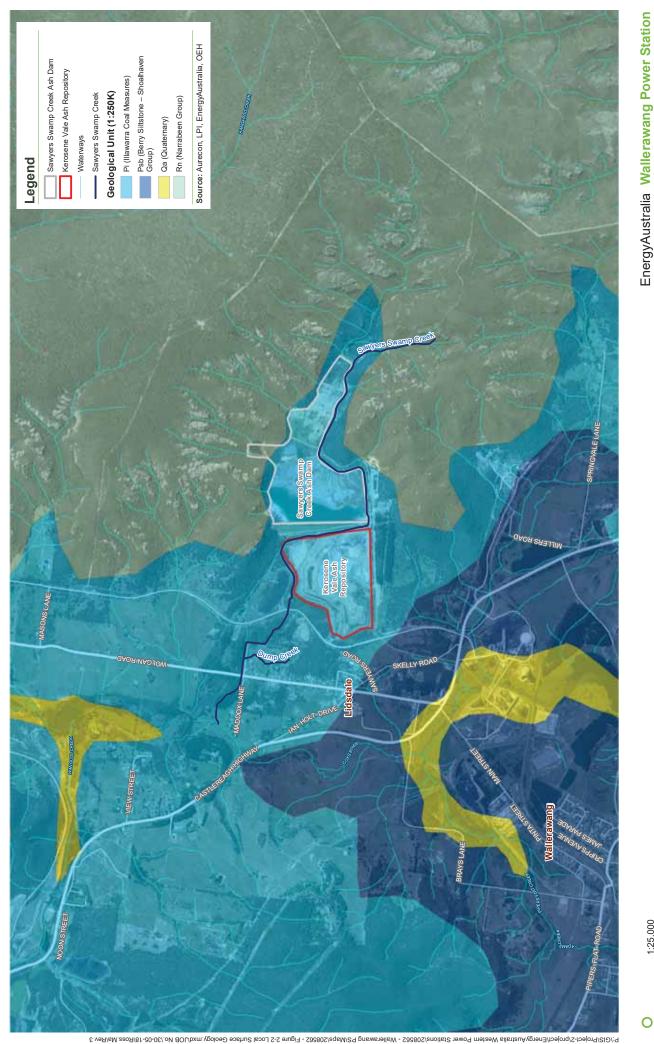


Projection: GDA 1994 MGA Zone 56

1,000m

1:35,000





500

1,000 m

Projection: GDA 1994 MGA Zone 56

Figure 2-2: Local Surface Geology

0

1:25,000

Creation of the Sawyers Swamp Creek Ash Dam (SSCAD) and Kerosene Vale Ash Repository has modified the catchment morphology. Upgradient and to the east of SSCAD, in the upper portions of the catchment valley, the topography has been modified from its original profile through emplacement of ash, to form a gently sloping (0.2% gradient) surface up to the SSCAD dam wall, which bisects the valley along a north-south axis.

Ash emplacement in the eastern portion of the catchment forms a wedge shape above the original (palaeo) surface of the basin valley. The ash wedge ranges in depth from 0m in the vicinity of the Freshwater Diversion Dam, to approximately 22m at the eastern most portion of the SSCAD pond (adjacent to pond C), and likely extending to 25m+ near the SSCAD cut-off wall. Locally the ash wedge is overlain by a thin cap of silty clay (c. 0.5m thick) and underlain by a layer of alluvial / residual type material (silty sand / clayey sand) (c.2.0m thick), underlain in turn by bedrock material (siltstones, shales and coals) of the Illawarra Coal Measures (ICM).

The profile of the valley falls sharply (approximately 16% gradient) on the western side of the ash dam wall, from approximately 940m AHD to approximately 915m AHD at its base. At the base of the SSCAD ash dam wall, Sawyers Swamp Creek (SSC) cuts up to the north from its diversion at the southern portion of the SSCAD dam, before meandering to the west and out to the Cox's River. To the west of the SSCAD and SSC, the original topography has been further modified through emplacement of the Kerosene Vale Ash Repository (KVAR) and underlying Kerosene Vale Ash Dam (KVAD), which together form a mound, rising up to approx. 20m above the original ground surface to a height of approximately 940mAHD. The SSC has been modified to flow to the east of the KVAR, before cutting around the north of the mound on its path out to the Cox's River.

# 2.3 Hydrogeology

The hydrogeology of the project area is complex owing to the extensive modifications to the drainage basin landform as a result of construction of the SSCAD, KVAR and historical modification to channel routing of the Sawyers Swamp Creek.

A groundwater contour plot (Figure 2-3) has been developed using recent (2017) groundwater monitoring data. The contour plots show that groundwater flows through the Narrabeen Group Sandstones and Upper Illawarra Coal Measures are generally to the west through the catchment, from the upper portions of the catchment, through / below the SSCAD and KVAR / KVAD and out towards Sawyers Swamp Creek, where groundwater flow paths turn to the south / south-east with the regional flow regime.





P:/Gl3/Project-Z/project/EnergyAustralia Western Power Stations/208562 - Walkerawang PS/Maps/208562 - Figure 2-3 5m Catchment Croundwater SSC mxd/DB No./30-05-16/Ross.Mas/Res 3

Projection: GDA 1994 MGA Zone 56

400m

200

1:9,000

0

EnergyAustralia Wallerawang Power Station

# 2.4 Site History

#### 2.4.1 Construction and Development

The Kerosene Vale Ash Repository (KVAR) area was originally constructed between 1960 and 1990, during which time it was filled with a combination of by-product (wet) ash from the Wallerawang Power Station and mining spoil from Springvale Colliery. Kerosene Vale was used as an ash dam during its operation and subsequent capping in 1990, hence it is distinguished as the Kerosene Vale Ash Dam (KVAD).

Between 1980 and 2003 wet ash from Wallerawang Power Station was emplaced within the Sawyers Swamp Creek Ash Dam (SSCAD) located east of and immediately upgradient of the KVAD. However, in 2001, Delta Electricity identified the need for additional storage capacity due to storage constraints within the SSCAD.

The KVAD area was identified as a suitable site, as it had been historically used for the purpose of ash placement for Wallerawang Power Station. However, placement of ash over the KVAD required a change from wet ash to a dry ash operation.

In 2002, approval was granted to Delta Electricity to change from wet ash to dry ash placement activities and to use the current KVAR area for dry ash storage. In 2003, placement of wet ash in the SSCAD ceased and placement of dry ash in the Stage 1 area of the KVAR commenced.

In November 2008, Delta Electricity received further project approval for extension of the KVAR. Subsequently the Stage 1 KVAR area was capped in February 2009 and placement in the Stage 2 KVAR area commenced in April 2009, with placement in the planned Stage 2A area outlined in the original ash placement strategy (Parsons Brinkerhoff, 2008).

With ash placement commencing in Stage 2A, Delta Electricity's contract structural engineers reviewed the ash placement strategy. Following this review, it was determined that previously planned construction activities were not required to facilitate the placement of ash in the Stage 2A. Subsequently a revised ash emplacement strategy was developed, which has been used in the design, construction and management of the recently decommissioned KVAR. Figure 2-4 presents a schematic of the placement strategy for Stage 1, 2A and 2B, with a Stage 2C placement area located between Stages 2A and 2B.

In January 2012, the Stage 2C area was excavated in preparation for ash placement, however ash placement did not proceed as a result of the subsequent decommissioning of Wallerawang in 2014.

In January 2014, Wallerawang Power Station's Unit 7 was removed from service and deregistered from the market; whilst in March 2014, Unit 8 was placed in long term storage. As a consequence, Wallerawang Power Station has not generated ash requiring disposal at KVAR since April 2014. Further, EnergyAustralia is currently negotiating with NSW Treasury to produce a plan for the decommission, deconstruction and rehabilitation of the entire operational facility at Wallerawang including the ash placement areas.

#### 2.4.2 Key Events

Through the lifecycle of dry ash placement in the KVAR, a number of key events can be identified associated with environmental management of the site, which have subsequently affected the dynamics of surface watergroundwater interactions and water quality signals. These events are summarised alongside the construction and development activities associated with the site in Table 2-2, and are approximate only.

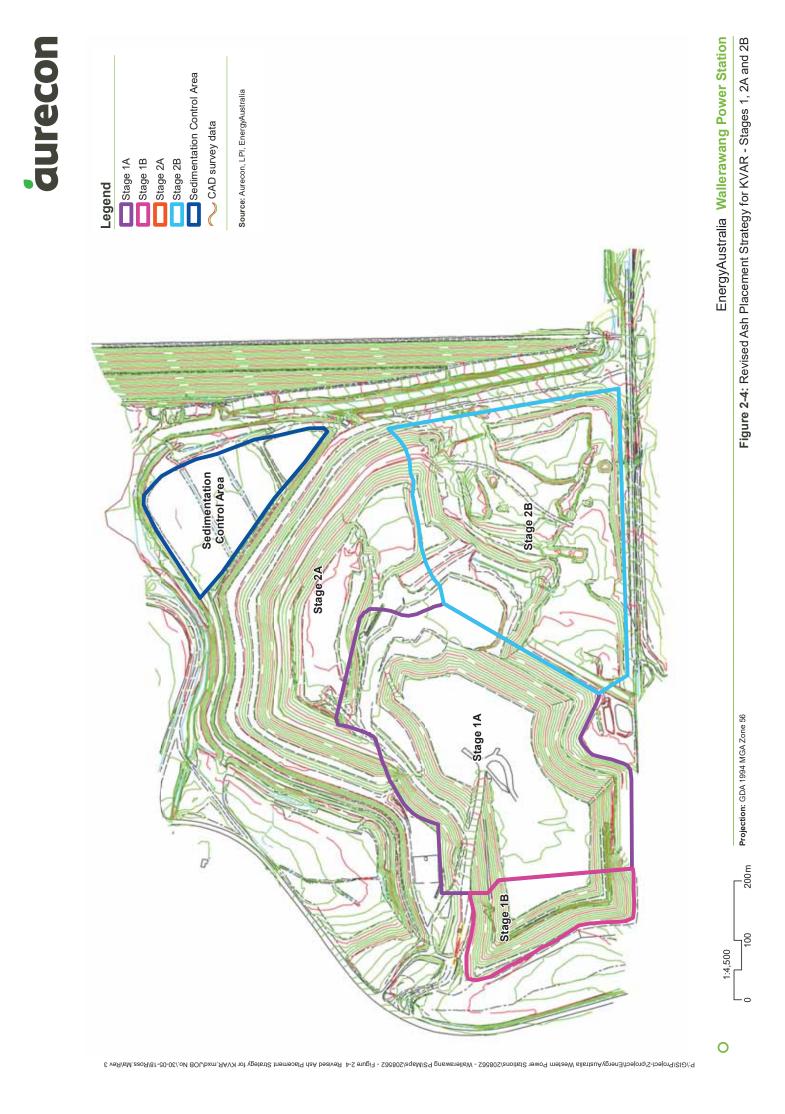
#### Table 2-2 Kerosene Vale Ash Repository – Record of Key Activities and Events

Approximate Date	Event Description
1960-1980	KVAD Wet Ash Emplacement
1980-2003	SSCAD Wet Ash Emplacement
1990	KVAD Capped
May 2003	Stage 1 Dry Ash Emplacement in Stage 1 KVAR
2006	KVAD Toe Drains Blocked
February 2009	Stage 1 Dry Ash Emplacement Complete and Capped
April 2009	Stage 2A Dry Ash Emplacement
February 2010	Stage 1 KVAD Toe Drains Unblocked to LC
May 2010	SSCAD Seepage Collection Installed
October 2010	Unblocked KVAD Toe Drains and Reinstated Seepage Collection and Diversion System to Lidsdale Cut.
October 2010	Sub-Surface Drains Installed for KVAD within KVAR Stage 2 Area and connected to KVAD Toe Drains
February 2011	Stage 2 Subsurface Unblocked to LC
July 2011	Springvale Mine Water Discharge Pipe Leak
January 2012	Stage 2C - Commenced, Never Emplaced
June 2012	Pumping from LC to SSC Stops
July 2012	Pumping from LC to SSCAD Via Canal Starts
July 2013	Springvale Mine Discharge 18ML/d to SSC Starts
March 2014	KVAR ceased operation and ash production
July 2015	Stage 2C Excavation and Clean Water Detention Pond

The key events affecting environmental conditions within the KVAR during its operational lifecycle, that are not related to general construction and development of the site include:

- 2006 Blockage of the KVAD toe drains
- October 2010 Unblocking of the KVAD toe drains
- October 2010 Installation of subsurface drains for the Stage 2 KVAR area
- October 2010 Reinstatement of seepage collection and diversion system to Lidsdale Cut
- February 2011 Unblocking of the Stage 2 subsurface drains
- June 2011 Springvale Mine Water Discharge Leak
- June 2012 Discharge from Lidsdale Cut to Sawyers Swamp Creek via v-notch ceases
- July 2012 Pumping from Lidsdale Cut to Sawyers Swamp Creek Ash Dam via the Return Canal commences
- July 2013 Springvale Mine Discharge (18ML/d) to Sawyers Swamp Creek Commences

In addition to the above list of events EnergyAustralia NSW has advised Aurecon that extensive erosion of the dry ash surface on the eastern side of the Stage 2 area had occurred and the batter was repaired in 2017. Rainfall runoff flowed to the southern side of the KVAR and the various surface water collection ponds and overflows collected the ash before the runoff entered the return canal.



# 2.5 Site Layout and Design

The current layout, design and operations at the KVAR are a result of the long history of events and activities related to ash emplacement and environmental management, including construction of the original KVAR (KVAD) between 1960 and 1990. Construction of the SSCAD and emplacement of wet ash between 1980 and 2003, and subsequent construction and development of the recently decommissioned KVAR between 2003 and 2014. Figure 2-5 presents the current layout and design of the KVAR relative to the SSC catchment features, including the SSCAD and SSC. Key elements of the KVAR, SSC and SSCAD are discussed in the following sections.

#### 2.5.1 Sawyers Swamp Creek

Sawyers Swamp Creek is an ephemeral creek which drains the Sawyers Swamp Creek Catchment of the Newnes Plateau. SSC flows from east to west and forms a tributary to the Coxs River, which drains south towards Lake Wallace. Any overflow from Lake Wallace is transmitted to Lake Lyell, which is the water supply reservoir for Mt Piper Power Station and part of the Sydney Drinking Water Supply. The natural course of SSC has been diverted through artificial channel modifications so that flows bypass the SSCAD and KVAR.

The flow path of SSC is currently to the south of the SSCAD, before turning north, passing between SSCAD and the KVAR. At northernmost portion of the KVAR, (north of the sedimentation area), SSC bends to the west passing between the KVAR and Centennial's Coal Stockpile beyond the northern boundary of the site. Sawyers Swamp Creek subsequently flows out to Coxs River, past Lidsdale Cut and Dump Creek, which forms a tributary to SSC.

Discharge through SSC is currently modified to a sustained flow in the lower portion of SSC catchment as a result of discharge from Springvale Colliery through LDP009, which is located adjacent to the SSCAD Spillway. The discharge through LDP009 is currently around 18ML/d.

#### 2.5.2 SSCAD

The SSCAD is a major artificial surface water body located between Springvale Colliery and the KVAD. The dam was historically used for wet ash disposal from Wallerawang Power Station. The SSCAD is separated from SSC by a toe drain to the south and by a dam wall to the west, through which seepage is collected via a concrete drain and returned to the SSCAD via a pump-back system.

Water levels in SSCAD are controlled by a gravity overflow outlet weir located at the front of the spillway. From the weir SSCAD, water discharges through a HDPE pipe to the Return Water Canal where it is pumped back to the SSCAD.

Catchment runoff from upstream of the ash dam enters the creek, via a pipe, that discharges over the spillway and joins SSC. Mine water discharge from Springvale Colliery enters SSC upstream of the spillway and mixes with catchment runoff.

#### 2.5.3 KVAR / KVAD

The KVAR / KVAD form an area characterised by an artificial mound of dry processed ash (KVAR) overlying a capped unit of wet processed ash (KVAD) which has been sequentially deposited in the KVAR area since the 1960s. Seepage and leachate within the KVAR / KVAD is controlled by a complex network of subsurface drains, connected to toe drains, leachate collection ponds and a return water canal (which is pumped to SSCAD).

Rainfall runoff from the northern part of KVAR is collected by a perimeter drain which directs the runoff to a Collection Pond in the north-east of the Stage 2 area. Groundwater seepage collected in the subsurface drains is also collected in this pond and the water is sent to the Lidsdale Cut pond via the pipeline. It is also understood that some of the water in the Collection Pond is reused for dust suppression by spraying on the dry ash deposit.

The KVAR / KVAD is hydraulically isolated from SSC by the KVAD toe drains which collect and transmit seepage / leachate to Lidsdale Cut Pond, local sumps, and / or the Return Water Canal.

#### 2.5.4 Lidsdale Cut Pond

Lidsdale Cut Pond is an artificial waterbody formed as a result of historical mining activities. Seepage from the KVAD / KVAR is collected and sent to the Lidsdale Cut Pond via the existing KVAD toe drains. Historically, seepage from the KVAD was discharged directly to SSC from the Lidsdale Cut pond via a v-notch. However, in June 2012, the v-notch was sealed in order to halt discharge to SSC, and in July 2012 water from Lidsdale Cut Pond was re-circulated to SSCAD via the return canal located to the south of the Stage 1 KVAR emplacement area. In 2017 this process was modified so that water from Lidsdale Cut Pond is currently discharged to the Dirty Water Pond (identified in Figure 2-5), located near the KVAR / KVAD dump valves, prior to being discharged to the SSCAD.

EnergyAustralia NSW has advised Aurecon that the water in the Lidsdale Cut pond is regularly pumped to maintain a water level about 0.4 to 0.6m above the current void bottom.

#### 2.5.5 Return Water Canal

The Return Water Canal is located to the south of the Stage 1 KVAR emplacement area and KVAD footprint. The Return Water Canal historically received pumped water from Lidsdale Cut Pond, until operations were modified in 2017. The Return Water Canal currently receives surface water runoff and seepage directly from the KVAR. Overflow water from the SSCAD is also discharged to the Return Water Canal via a HDPE pipe. Water within the Return Canal is discharged to the SSCAD via a pump-back system.





Figure 2-5: Site Layout and Design

EnergyAustralia Wallerawang Power Station

Projection: GDA 1994 MGA Zone 56

200m

1:5,500

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# 3 Water Quality Guidelines

# 3.1 ANZECC Guidelines

As used in previous reports since 2008, the principle of the ANZECC (1995) guidelines for protection of groundwater, where the potential future use of the water resource is considered, has been taken into account. In this regard, the Irrigation, Ecosystem and additional guidelines for protection of livestock or drinking water has been used, where appropriate, to provide a wider context of the ANZECC (2000) guidelines, and to define acceptable ambient water quality at the KVAR Stage 2 receiving water sites.

Due to the mineralised conditions and long history of mining related activities within the SSC catchment and wider Wallerawang region, locally derived water quality guidelines have been applied to several water quality parameters that are likely to have been affected by the historical activities and local conditions.

The groundwater background concentrations were adopted from the pre-placement data from the background bore, WGM1/D2, and elevated concentrations at the seepage detection bore WGM1/D5 and Lidsdale Cut (WX5) were also taken into account. The surface water background concentrations use the pre- placement data at Dump Creek, WX11, which is the local background for the mineralised area. The pre-KVAR data at WX7 was also taken into account.

The water quality monitoring is undertaken to ascertain whether the local/ANZECC (2000) guidelines (as applicable) and groundwater investigation levels (GILs – NEPM 2013) are met in the groundwater receiving water bores D5 and D6 and in Sawyers Swamp Creek at the final surface water receiving water site, WX7.

In accordance with ANZECC guidelines, the 95<sup>th</sup> percentile of concentrations in water quality monitoring results are compared against the adopted Water Quality Guideline Values (WQGVs), which include both ANZECC (1995) trigger values and locally derived guideline values.

# 3.2 NEPM Guidelines

Groundwater investigation levels (GILs) are the concentrations of a contaminant in groundwater above which further investigation (point of extraction) or a response (point of use) is required. GILs are based on Australian water quality guidelines and drinking water guidelines and are applicable for assessing human health risk and ecological risk from direct contact (including consumption) with groundwater. Further information is provided in Section 2.8 and Schedule B6.

The Groundwater investigation levels (GILs) are based on the Australian Water Quality Guidelines 2000 (AWQG), Australian Drinking Water Guidelines 2011 (ADWG) and Guidelines for Managing Risk in Recreational Waters 2008 (GMRRW). The GILs are adopted in the NEPM as investigation levels in the context of the framework for risk-based assessment of groundwater contamination (refer Schedule B6), i.e. levels above which further assessment is required.

The AWQG provide tabulated values based on percentage species protection for various aquatic environments and water uses. The appropriate settings for current and potential uses of groundwater need to be identified for the aquifer undergoing assessment. The guideline documents should be consulted for appropriate interpretation of guideline values, in consultation with relevant regulatory authorities if necessary.

# 3.3 Applicability of Water Quality Guidelines

- The surface water guideline goals apply to the receiving waters of Sawyers Swamp Creek at WX7, only for the effects of the ash placement input concentrations (including the associated effects of coal waste/chitter leachates), but not for the effects of the Springvale Coal Mine input
- The groundwater goals apply to the seepage detection bore WGM1/D5, but not to Lidsdale Cut (WX5) since July 2012. These monitoring points are also used for early warning of potential effects on the Sawyers Swamp Creek receiving waters. These goals are used for assessment of the decommissioned KVAR effects in this report.

# 4 Surface Water and Groundwater Monitoring Results: 2018 - 2019

# 4.1 Surface Water

#### 4.1.1 Monitoring Locations

To satisfy sampling requirements for the project, EnergyAustralia NSW undertook surface water sampling at the monitoring locations summarised in Table 4-1, below and presented in Figure 4-1.

	e Mine Water Swamp Creek	Springvale Discharge Springvale Mine Water Discharge Surface Water Receiving S	2011-2018 (no 2018/19 data)	Inside	
A1 Sawyers S	Swamp Creek	Discharge	(no 2018/19 data)	Inside	
		Surface Water Receiving S			Building
			Site		
	<i>X</i> ()	Receiving Water Site	1991-2019	228961	6302719
	S	awyers Swamp Creek Additior	nal Sites		
92 Upstream	SSCAD (WX1)	Upgradient of SSCAD Surface Water	1992-2018 (dry 2019)	231969	6301582
93 SSC Dow	nstream V-notch	SSC Downstream of SSCAD Seepage Collection	2010-2019	230166	6302340
83 SSC Dow	nstream KVAR	SSC Downstream of KVAR Stage 2A	2010-2019	229650	6302246
225 SSCAD S	pillway	SSCAD Water Outflow	2012-2019	230369	6302775
		SSCAD			
38 Sawyers S Dam (SSC	Swamp Creek Ash CAD 38)	SSCAD Water Input from Return Canal	1996-2019	229766	6301457
79 SSCAD V	'-notch	SSCAD Seepage Collection	2010-2019	230259	6302287
		KVAR / KVAD			
81 West KVA Left	D Wall subsurface	North-West Wall of KVAR / KVAD	2010-2017 (dry 2018/19)	229684	6302194
80 West KVA Right	AD Wall Subsurface	North-West Wall of KVAR / KVAD	2010-2019	229660	6302179
86 North Wa	Il Collection	North Wall of KVAR / KVAD	2010-2019	229909	6302201
87	Vater Runoff / West all Subsurface	North Wall Surface Water Runoff	2010-2019	229947	6302227
		Lidsdale Cut Pond			
40 Lidsdale 0	Cut (WX5)	Lidsdale Cut Monitoring	1992-2019	229402	6302329
		Dump Creek			
39 Dump Cre	eek (WX11)	Dump Creek Monitoring	1991-2019	229102	6302666

The monitoring locations were selected to represent surface water quality upstream, downstream and at several reference locations.

Routine long-term water quality data has been collected for SSC at receiving water (WX7), and upgradient location (WX1) since 1991 / 1992. Water quality data for additional sites upgradient and downgradient of the KVAR (Sites 83, 93, 225) are available from 2010. Long term water quality data has also been collected for Lidsdale Cut Pond at WX5 and Dump Creek at WX11. Water quality data is available for SSCAD from 1996, whilst data for KVAR / KVAD monitoring points is available from 2010.





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# EnergyAustralia Wallerawang Power Station



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#### 4.1.2 Monitoring Methodology

Routine surface water monitoring is undertaken on a monthly basis on behalf of EnergyAustralia NSW by Nalco Analytical Resources who measure conductivity, pH and temperature in the field using calibrated instrumentation.

Aurecon understand that all surface water samples were collected in accordance with ANZECC (2000) monitoring guidelines (Chapter 4) for shallow waters, with samples collected from just below the surface (0.25m-0.5m) either directly to sample collection bottles by hand (using disposable nitrile gloves) or using a plastic bucket fixed to a rope – cleaned prior to use and between sampling sites and dispensed into sample collection bottles.

#### 4.1.3 Monitoring Results

Surface water monitoring results for the 2018-2019 reporting period are presented in Appendix C along with a statistical summary of the data.

In accordance with ANZECC (2000) and ADWG (2011) guidelines, the 95<sup>th</sup> Percentile of the test results from surface water monitoring for toxicants and stressors have been compared against selected surface water guideline values that are based on ANZECC (2000) Trigger Values (ANZECC, 2000 Section 7.4.4.1, Step 2) or ADWG Values (ADWG, 2011 – Chapter 10), and against local WQGVs where locally derived WQGVs supplant ANZECC / ADWG Trigger Values. The results from this assessment are presented in Table 4-2 below.

Table 4-2 Summary Statistics 2018-2019 Surface Water Monitoring Results (mg/L) – 95 <sup>th</sup> Percentiles	Statistic	s 2018-20	19 Surfac	e Water N	Aonitorin	g Results	3 – (T/Bu)	15 <sup>th</sup> Percent	iles														
Sample Location	Hd	Cond (µs/cm)	TDS	SO4	Ū	AI*	As	Ag	Ba	Be	<u>*</u>	cd	స	Cu	L	Fe-F	Hg	Mn	Mo	ż	Pb	Se	Zn*
											Sprir	Springvale Discharge	irge										
Springvale (158)	QN	QN	QN	QN	QN	QN	QN	QN	QN	QN	QN	QN	QN	QN	QN	QN	QN	QN	QN	QN	QN	QN	QN
										Sawyers Sv	vamp Cree	Swamp Creek – Surface Water Receiving Site	Vater Receiv	ing Site									
WX7 (41)	8.7	1284	813	130	9.1	2.2	0.026	0.001	0.026	QN	0.19	0.0001	0.001	0.0025	1.31	0.062	0.00004	0.01	0.049	0.004	0.002	0.001	0.025
										Sawj	rers Swam	Sawyers Swamp Creek – Additional Sites	ditional Site	s								-	
Upstream SSCAD WX1 (92)	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRΥ	DRY	DRY	DRY	DRY	DRY	ркү	DRY	DRY	DRY
Downstream V- Notch (93)	8.6	1284	792	25	9.4	4.1	0:030	0.001	0.026	Q	0.46	0.0001	0.001	0.0045	1.34	0.074	0.00004	0.03	0.049	0.005	0.001	0.001	0.025
Downstream KVAR (83)	8.7	1274	780	35	9.8	1.7	0.027	0.001	0.027	QN	0.14	0.0001	0.001	0.0015	1.36	0.053	0.00004	0.01	0.051	0.004	0.001	0.001	0.022
Spillway (225)	8.3	1279	741	27	9.7	4.4	0.028	0.001	0.025	QN	0.19	0.0001	0.001	0.0083	1.95	0.054	0.00004	0.02	0.050	0.004	0.002	0.001	0.035
												SSCAD											
SSCAD (38)	6.4	710	455	307	8.6	0.8	0.001	0.001	0.128	Q	1.20	0.0015	0.001	0.002	0.49	0.047	0.00004	1.04	0.041	0.052	0.001	0.001	0.207
SSCAD V-Notch (79)	6.9	2482	1936	1326	84	0.5	0.001	0.001	0.074	QN	1.85	0.0003	0.001	0.003	2.6	0.095	0.00004	3.69	0.002	0.034	0.001	0.0004	0.035
											×	KVAR / KVAD	-	1								1	
West KVAD seepage left (81)	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY
West KVAD seepage right (80)	2.9	4749	4093	2822	44	51	0.001	0.001	0.004	QN	15	0.0025	0.001	0.008	25	71	0.00005	24	0.001	2.66	0.001	0.002	3.85
North Wall Collection (86)	2.9	5033	4264	2921	27	45	0.005	0.001	0.001	QN	12	0.0004	0.003	0.003	69	56	0.00004	18	0.001	1.39	0.001	0.005	3.69
Subsurface Throughflow (87)	3.1	5133	5061	3511	28	86	0.047	0.001	0.002	QN	13	0.0013	0.003	0.005	86	139	0.00004	17	0.001	1.64	0.001	0.070	4.84
												Lidsdale Cut											
Lidsdale Cut WX5 (40)	3.3	4015	3713	3023	28	139	0.019	0.001	0.023	QN	11	0.0350	0.014	0.025	26	9.8	0.00004	15	0.001	1.32	0.011	0.115	2.88
												Dump Creek											
Dump Ck WX11 (39)	3.3	1734	1168	882	36	7.0	0.001	0.001	0.038	QN	2.66	0.0017	0.001	0.024	2.37	11.1	0.00004	6.58	0.001	0.73	0.008	0.001	2.24
												WQGVs											
Surface Water WQGV	6.5- 8.0	2200	1500^	1000++	350+	5.25^^	0.024	0.00005	0.7+++	0.1	<u>1.25</u>	0.0015	0.005	0.005	1.5+++	0.3+++	0.00006	1.9	0.01+	0.05	0.005	0.005	0.153
Notes:																							
Red: Blue: Purple: Bold Underline: ++	U C C C C C C C C C C C C C C C C C C C	Exceeds WQGV (receiving environment monitoring location) Exceeds WQGV (on-site monitoring location) Laboratory Limits of Reporting Exceed WQGV Local Reference WQGV (using 90th percentile of pre-dry pla Irrigation water moderately tolerant crops; irrigation. Note: ML Livestock ADWGV	3V (receivir 3V (on-site nits of Rept ce WQGV - r moderatel VGV	ng environn monitoring orting Exce. (using 90th ly tolerant c	nent monit location) ed WQGV percentile ;rops; irrig;	oring locatic of pre-dry I ation. Note:	Exceeds WQGV (receiving environment monitoring location) Exceeds WQGV (on-site monitoring location) Laboratory Limits of Reporting Exceed WQGV Local Reference WQGV (using 90th percentile of pre-dry placement data) Irrigation water moderately tolerant crops; irrigation. Note: Molybdenum dr Liveskock ADWGV	Exceeds WQSV (receiving environment monitoring location) Exceeds WQSV (on-site monitoring location) Laboratory Limits of Reporting Exceed WQGV Local Reference WQGV (using 90th percentile of pre-dry placement data) Irrigation water moderately tolerant crops; irrigation. Note: Molybdenum drinking is 0.05 mg/L Livestock ADWGV	.05 mg/L														
< v v v	AL AL	roundwater uminium sui	conductivity face water	/ derived fr local goal f nner lead	om TDS 91 rom Dump nickel and	0th percentil √Creek 90th I zinc adiust	le of 2000 m I Percentile a	Groundwater conductivity derived from TDS 90th percentile of 2000 mg/L TDS/0.77; Creek TDS derived Aluminium surface water local goal from Dump Creek 90th Percentile and groundwater local goal from b Cadminim Chronoium Conner lead nicket and zince adjusted for effets of hardness: Ca Moni, WCMMD	Creek TDS ter local goo Ca Mrin V	derived fro I from bore VGM1/D5 3	m 0.68 x 2 D6 90th pr	Groundwater conductivity derived from TDS 90th percentile of 2000 mg/L TDS/0.77; Creek TDS derived from 0.68 x 2200 µS/cm, which is the Aluminium surface water local goal from Dump Creek 90th Percentile and groundwater local goal from bore D6 90th percentile (data for both) Cadminim Chroneium Conner lead airkel and zinc adiusted for effects of bardness. Ca Min in WGM1015 52 3.200 mod	for both)	Groundwater conductivity derived from TDS 90th percentile of 2000 mg/L TDS/0.77; Creek TDS derived from 0.68 x 2200 µS/cm, which is the ANZECC (2000) low land river cond. Aluminium surface water local goal from Dump Creek 90th Percentile and groundwater local goal from bore D6 90th percentile (data for both) Commium Chromeium Concer lead nicked and zinc adjusted for effects of barchees: Ca. Mor in WC4M105.27.3. 39.0 mol 1. in Sawware Swamn Creek 51.6.38.0 mol 1. respectively	low land river	from 0.68 x 2200 µS/cm, which is the ANZECC (2000) low land river conductivity for protection of aquatic life are D6 90th percentile (data for both) 6. 20.3 . 29.0 m/nl · in Sawvers Swamm Creek 51.6. 38.0 m/nl · respectively.	r protection of	f aquatic life					
	5		, , ,			2			5 5 5		6			6	1	financia							

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#### WX7 – Receiving Site

As outlined in Section 3.3, the surface WQGVs apply only to the receiving waters of Sawyers Swamp Creek at WX7. The results presented in Table 4-2 indicate that the 95<sup>th</sup> percentile concentrations of key parameters of surface water samples at WX7 in SSC from the 2018-2019 monitoring period are generally below the adopted WQGVs with the exception of the following:

- pH Exceeds upper limit
- Arsenic Marginally exceeds ANZECC (2000) WQGV
- Molybdenum Marginally exceeds Irrigation WQGV

Exceedances of these parameters at WX7 are attributed to discharge from Springvale Mine at LDP009 into SSC. Aurecon understands that Springvale Mine Discharges approximately 18ML/d into SSC at LDP009, and that the discharge is sampled at Site 158. Due to the ephemeral nature of SSC, discharge from Springvale Mine dominates surface water in SSC and as a result water quality at WX7 (Site 41) is reflective of the Springvale Discharge sampled at Site 158.

As the observed concentrations of water quality parameters in SSC at WX7 are reflective of discharge from Springvale Mine, it can be inferred that the KVAR is not currently affecting water quality in SSC at the receiving site.

#### Sawyers Swamp Creek Additional Sites

The results presented in Table 4-2 indicate that 95<sup>th</sup> percentile concentrations of key parameters in the SSC additional sites, including sites 93, 83 and 225, from the 2018-2019 monitoring period are generally below the adopted WQGVs with the exception of the following:

- pH Exceeds upper limit
- Arsenic Marginally exceeds ANZECC (2000) WQGVs
- Molybdenum Marginally exceeds Irrigation WQGVs
- Copper (Site 225 only) Exceeds ANZECC (2000) WQGV
- Fluoride (Site 225 only) Exceeds Drinking Water ADWGV

Site 92 (WX1) was dry throughout the 2018-2019 monitoring period and as such no water quality data is available for assessment. Concentrations of water quality parameters at Sites 93, 83 and 225 are similar to water quality at WX7 (Site 41). As these sites are located downgradient of the Springvale Mine Licence Discharge Point (LDP009), and show close similarity with the historic chemistry of Springvale Mine water discharge, it is clear that water quality at these sites is dominated by the Springvale Mine water discharge and is generally unaffected by the KVAR.

Water quality results from these monitoring sites are consistent with water quality results from previous years.

#### SSCAD

The results presented in Table 4-2 indicate that 95<sup>th</sup> percentile concentrations of several key parameters from the 2018-2019 monitoring period SSCAD monitoring points (Sites 38 & 79) exceeded the adopted WQGVs, including:

- pH (Site 38 only) Below lower limit
- Conductivity (Site 79 only) Exceeds ANZECC (2000) WQGV
- TDS (Site 79 only) Exceeds the pre-defined limit (derived from 0.68 x 2200 µS/cm, which is the ANZECC (2000) low land river conductivity for protection of aquatic life)
- Sulfate (Site 79 only) Exceeds Livestock ADWGV
- Boron (Site 79 only) Exceeds locally derived WQGV

- Fluoride (Site 79 only) Exceeds Drinking Water ADWGV
- Manganese (Site 79 only) Exceeds ANZECC (2000) WQGV
- Molybdenum (Site 38 only) Exceeds Irrigation WQGV
- Nickel (Site 38 only) Marginally exceeds ANZECC (2000) WQGV
- Zinc (Site 38 only) Exceeds locally derived WQGV

The elevated concentrations of water quality parameters at these sites is attributed to the storage and recirculation of SSCAD overflow water and KVAR / KVAD leachate from to the Return Water Canal for Site 38 and reflective of SSCAD pond water which has passed through the SSCAD wall for Site 79. The concentrations of trace metals and sulfate are indicative of a fly ash leachate with neutral (SSCAD) to acidic (KVAR) pH characteristics. The relatively neutral pH observed at Site 79 may also be as result of pH buffering by clays within the SSCAD wall.

Both sites 79 and 38 are hydraulically isolated from SSC and receiving water site WX7, and water quality at these locations does not directly affect the water quality in SSC. Monitoring results from these sites are consistent with the monitoring results from previous years.

#### KVAR / KVAD

The results presented in Table 4-2 indicate that the 95<sup>th</sup> percentile concentrations of key parameters in surface water monitoring locations for the KVAR / KVAD over the 2018-2019 monitoring period generally exceeded the adopted WQGVs with the exceptions of Cl, As (excluding Site 87), Ba, Cd (excluding Site 80), Cr, Cu (excluding Sites 80 & 87), Hg, Mo, Pb, and Se (excluding Site 87). pH was highly acidic (c. pH 3.0, indicative of an acidic fly ash).

It is noted that these locations sample both seepage and surface water runoff from the KVAR / KVAD and as such are indicative of seepage waters emanating from the KVAR / KVAD into the KVAD toe drains, which hydraulically isolate the KVAR / KVAD from SSC. Water collected in the KVAD toe drains is transmitted to Lidsdale Cut, from where it is currently pumped to the dirty water pond (adjacent to the Return Water Canal) and back to the SSCAD.

The KVAR / KVAD surface water monitoring sites (80, 81, 86, 87) are hydraulically isolated from SSC by the KVAD / KVAR toe drains which divert water from the KVAD / KVAR to Lidsdale Cut Pond.

Water quality results from these monitoring sites are consistent with water quality results from previous years

#### Lidsdale Cut Pond (WX5)

The results presented in Table 4-2 indicate that the 95<sup>th</sup> percentile concentrations of key parameters in surface water monitoring locations for Lidsdale Cut over the 2018-2019 monitoring period generally exceeded the adopted WQGVs, with the exceptions of Cl, As, Ba, Hg and Mo. With the exception of Cd, Fe and F, concentrations of water quality parameters are comparable with those sampled from the KVAR / KVAD sample points, indicative of the current drainage system from the KVAD toe drains to Lidsdale Cut. pH was highly acidic (pH 3.1), symptomatic of a dry, acidic fly ash (Ward et al., 2009).

The results for WX5 suggest the KVAR may potentially be affecting water quality in Lidsdale Cut Pond. It should be noted however that Lidsdale Cut Pond is pumped back to the Dirty Water Pond adjacent to the Return Water Canal, before being pumped back to SSCAD. Therefore, the water in Lidsdale Cut Pond does not directly affect water quality in SSC or at receiving Site WX7.

Water quality results from these monitoring sites are consistent with water quality results from previous years

#### Dump Creek (WX11)

The results presented in Table 4-2 indicate that the 95<sup>th</sup> percentile concentrations of several key parameters in surface water monitoring locations for Dump Creek over the 2018-2019 monitoring period exceeded the adopted WQGVs, including:

pH – Below lower limit

- Aluminium Exceeds locally derived WQGV
- Boron Exceeds locally derived WQGV
- Cadmium Exceeds ANZECC (2000) WQGV
- Copper Exceeds ANZECC (2000) WQGV
- Fluoride Exceeds Drinking Water ADWGV
- Iron Exceeds Drinking Water ADWGV
- Manganese Exceeds ANZECC (2000) WQGV
- Nickel Exceeds ANZECC (2000) WQGV
- Lead Exceeds ANZECC (2000) WQGV
- Zinc Exceeds locally derived WQGV

Concentrations of sulfate were elevated but marginally below the adopted WQGV. The origin of elevated concentrations of water quality parameters at Dump Creek requires further investigation, however may reflect leachate seepage from ash within the KVAR / KVAD (as indicated by the low pH of sampled waters) to groundwater and subsequent discharge to surface water at Dump Creek, which forms a tributary to Sawyers Swamp Creek upgradient of (east of) WX7 surface water receiving site. Indications of impacts to Dump Creek from the KVAR are also evident from historical records (discussed in Section 5.1.6) which indicates that impacts to water quality in Dump Creek occurred concurrent with (and not preceding) KVAR dry ash emplacement and subsequently modified by leakage and then discharge from Springvale Mine.

Due to the complexity of current and historic land use activities, including local chitter deposits, pumping and discharge regimes for the KVAD and SSCAD, it is not conclusive (based on the data set available) to directly attribute water quality impacts observed in Dump Creek solely to a single source such as the KVAR.

# 4.2 Groundwater

#### 4.2.1 Monitoring Locations

To satisfy sampling requirements for the project, EnergyAustralia NSW undertook groundwater sampling at the monitoring locations summarized in Table 4-3, below and presented in Figure 4-1.

Site #	Nalco Site ID	Purpose	Monitoring Period	Easting	Northing
		Groundwater Receiving Site			
36	Groundwater Bore WGM1/D5	Regional Surficial – Downgradient KVAR / KVAD	1988-2019	229636	6302189
		KVAR / KVAD			
37	Groundwater Bore WGM1/D6	Regional Coal Seam – Downgradient KVAR / KVAD	1988-2019	229415	6302029
77	Groundwater Bore AP09	KVAD North Wall	2010-2019	229837	6302182
78	Groundwater Bore AP17	KVAD North Wall	2010-2019	229916	6302192
94	KVAD Seepage	KVAD Seepage	2010-2019	229462	6302267
85	Groundwater Bore GW6	Seepage – Downgradient KVAR / KVAD	2010-2019 Dry from 2017	229753	6302222
75	Groundwater Bore GW10	KVAD West Wall	2010-2019 Dry from 2013	229612	6302000

Table 4-3 Project Groundwater Monitoring Locations

Site #	Nalco Site ID	Purpose	Monitoring Period	Easting	Northing
76	Groundwater Bore GW11	KVAD West Wall	2010-2019 Dry from 2016	229648	6302092
	Downgradient of	SSCAD / Upgradient – Cross Grad	lient of KVAR /	KVAD	
33	Groundwater Bore WGM1/D2	Regional - South East	1988-2019	229681	6301387
34	Groundwater Bore WGM1/D3	Regional - East below SSCAD, Upgradient KVAR / KVAD	1988-2019	230278	6301752
35	Groundwater Bore WGM1/D4	Regional – NE of SSC	1988-2019	230159	6302353
		Upgradient of SSCAD			
32	Groundwater Bore WGM1/D1	Regional - Upstream – Upper Catchment	1988-2019	231992	6301405

The monitoring locations were selected to represent groundwater quality upstream, downstream and reference locations for KVAR / KVAD. Borehole logs for the selected monitoring wells are presented in Appendix D.

Groundwater levels are also recorded during collection of water quality samples. Groundwater levels often play an important role in the understanding of groundwater quality and the effects of groundwater levels on water quality are discussed later in this report. Figures E1-E6 Appendix E, present long-term graphs of groundwater levels for monitoring Bores D1-D6, which were installed and have subsequently been monitored since 1988. The logs for these bores are presented in Appendix D.

The bores GW6 (Site 85), AP09 (Site 77) and AP17 (Site 78), shown in Figure 4-1, sample the groundwater in the KVAD beneath the KVAR along the north wall of the KVAD / KVAR Stage 2A area. Records for AP09 and AP17 are available from 2010 to the current monitoring period (2019). No records are available for GW6 for the 2018-2019 monitoring period.

The bores GW10 (Site 75) and GW11 (Site 76), shown in Figure 4-1, sample the groundwater in the KVAD beneath the KVAR along the western wall of the KVAD / KVAR Stage 2A area. Water quality records for GW10 are available from 2010 to 2012 with frequent gaps in available data. Water quality records for GW11 are available from 2010 to 2016, with frequent gaps in available data. Data for GW10 and GW11 are not available for the 2018-2019 monitoring period.

The bore D6 (Site 37) samples groundwater within the Illawarra Coal Measures downgradient of the KVAR / KVAD, and SSCAD, but upgradient of Lidsdale Cut. Water quality records for D6 are available from 1988 to 2019 and are generally complete, but with missing data between February 1998 - November 2001 and October 2004 – July 2007. Data is available for the 2018-2019 monitoring period.

The bores D2 (Site 33), D3 (Site 34) and D4 (Site 35) sample groundwater within the Narrabeen Group and Illawarra Coal Measures upgradient / cross gradient of the KVAR / KVAD and downgradient of the SSCAD. Water quality records for D2, D3 and D4 are available from 1988 to 2019, including the 2018-2019 monitoring period. Water quality records for D2, D3 and D4 are generally complete, with the exception of missing data between September 1997 and November 2001.

The data from these bores was used to assess the potential effects of the KVAR and KVAD on groundwater quality at the receiving water bore MPGM4/D5.

#### 4.2.2 Monitoring Methodology

Routine groundwater monitoring is undertaken on a monthly basis on behalf of EnergyAustralia NSW by Nalco Analytical Resources who measure conductivity, pH and temperature in the field using calibrated instrumentation.

Groundwater bores are bailed and sampled after allowing time for the water level in the bore to re-establish. The depth to the water level from the top of the bore pipe is measured using a dip meter and the water surface elevation is calculated to AHD(m) after allowing for the pipe height.

#### 4.2.3 Monitoring Results

Groundwater monitoring results for the 2018-2019 reporting period are presented in Appendix C along with a statistical summary of the data.

In accordance with the National Water Quality Management Strategy (NWQMS) Guidelines for Groundwater Protection in Australia (2013) and National Environment Protection Council (NEPC, 1999 as amended in May, 2013), the 95<sup>th</sup> Percentile of the test results from groundwater monitoring for toxicants and stressors have been compared against selected groundwater investigation levels, that are based on NEPM (2013) Groundwater Investigation Levels (NEPM, 2013 – Schedule B1, Section 3.2.1), .Where GILs are absent, the 95<sup>th</sup> percentile of results have been compared against ANZECC (2000) WQGVs, (ANZECC, 2000 Section 7.4.4.1, Step 2), or ADWG Values (ADWG, 2011 – Chapter 10), and against local WQGVs, where locally derived WQGVs supplant NEPM GIL / ANZECC / ADWG Trigger Values. The results from this assessment are presented in Table 4-4 below.

					1																i		1
Site Name / ID	Н	Cond (µs/cm)	TDS	SO4	Ū	A*	As	Ag	Ba	Be	* *	B	ວັ	Ē	u.	<b>Ее-</b> Е	Рġ	ЧW	Мо	z	Pb	Se	zn*
										Ground	Groundwater Receiving Site	ving Site											
WGM1/D5 (36)	4.0	1158	890	597	28.8	28.1	0.004	0.0010	0.07	QN	2.26	0.008	0.005	0.019	0.99	5.57	0.00006	6.40	0.003	0.444	0.024	0.002	1.73
											KVAR / KVAD	6											
WGM1/D6 (37)	3.9	2210	1986	1311	56.2	9.2	0.003	0.0010	0.03	QN	1.39	0.001	0.008	0.034	0.31	236	0.00005	11.19	0.001	0.609	0.020	0.001	1.66
AP09 (77)	5.9	2840	2425	1553	34.1	66.0	0.062	0.0010	0.02	QN	3.46 0	0.0002	0.001	0.001	8.9	103	0.00004	9.18	0.209	1.42	0.001	0.001	1.39
AP17 (78)	3.5	5545	5900	4124	29.2	50.7	0.105	0.0010	0.02	QN	15.2 0	0.002	0.009	0.01	82.1	195	0.00004	15.8	0.007	1.84	0.002	0.168	5.85
KVAD Seepage (94)	3.1	5624	6830	4705	38.9	334	0.049	0.0010	0.02	QN	19.3	0.092	0.044	0.07	59.5	45.5	0.00004	22.6	0.002	2.45	0.004	0.063	4.72
GW6 (85)	QN	QN	Q	QN	QN	QN	QN	Q	Q	QN	QN	QN	QN	Q	Q	Q	QN	QN	QN	Q	QN	QN	QN
GW10 (75)	QN	QN	QN	QN	QN	QN	QN	Q	Q	QN	QN	QN	QN	QN	Q	Q	QN	QN	Q	QN	QN	QN	Q
GW11 (76)	QN	QN	Q	QN	QN	QN	QN	Q	Q	QN	QN	QN	QN	Q	Q	Q	QN	QN	QN	Q	QN	QN	QN
								Downgradient of	ent of SSC.	Jan / Upg	SSCAD / Upgradient – Cross Gradient of KVAR / KVAD	ross Gradie	nt of KVAR	/ KVAD									
WGM1/D3 (34)	4.1	4167	4450	3088	31.5	112	0.013	0.0010	0.06	QN	9.68	0.032	0.003	0.027	13.9	48.4	0.00004	13.6	0.001	3.93	0.013	0.020	4.17
WGM1/D4 (35)	6.1	1769	1255	924	41.1	0.02	0.002	0.0010	0.02	QN	1.81 0	0.0001	0.001	0.001	0.27	52.0	0.00004	13.7	0.001	0.030	0.001	0.0002	0.037
WGM1/D2 (33)	3.5	680	386	195	38.9	2.6	0.002	0.0010	0.06	QN	0.26 0	0.0002	0.004	0.004	0.05	0.76	0.00005	0.66	0.002	0.075	0.009	0.0008	0.128
										Upgr	Upgradient of SSCAD	SCAD											
WGM1/D1 (32) [single sample]	5.2	116	108	6.4	19.5	1.4	0.001	0.0010	0.04	Q	0.05 0	0.0001	0.001	0.005	0.01	1.56	0.00004	0.08	0.001	0.003	0.002	0.0002	0.106
										Grou	Groundwater WQGVs	3GVs											
Groundwater WQGV	6.5-8.0	2600	2000++	1000++	350+	5.1 ^ ^	0.024	0.00005	0.7+++	0.1	<u>1.7</u>	0.001	0.004	0.005	1.5 +++	<u>1.7</u>	0.00006	1.9	0.01+	0.137	0.01	0.005	0.505
Red: Blue: Purple: Bold Underline: + + + + + + A Mote: Note:	Exceed Exceed Laborat Local R Irrigatioi Livestoc Drinking Groundv Aluminit	Exceeds WQGV (receiving environment monitoring location) Exceeds WQGV (on-site monitoring location) Laboratory Limits of Reporting Exceed WQGV Local Reference WQGV (using 90th percentile of pre-dry placement data) Livistoton water moderately tolerant crops; irrigation. Note: Molybdenum drinking is 0.05 mg/L Livistoto MAGV Livistoto ADMGV Groundwater conductivity derived from TDS 90th percentile of 2000 mg/L TDS/0.77; Creek TDS derived from 0.68 x 2200 µS/cm, which is the ANZECC (2000) low land river condu Groundwater conductivity derived from TDS 90th percentile of 2000 mg/L TDS/0.77; Creek TDS derived from 0.68 x 2200 µS/cm, which is the ANZECC (2000) low land river condu Groundwater conductivity derived from TDS 90th percentile and groundwater local goal from bore D6 90th percentile (data for both) Groundwater conductivity derived from Dump Creek 30th Percentile and groundwater local goal from bore D6 90th percentile and groundwater local goal from bore D6 90th percentile and groundwater conductive Aluminium surface water local goal from Dump Creek 30th Percentile and groundwater local goal from bore D6 90th percentile and groundwater local goal from bore D6 90th percentile (data for both) Cadmium, Chromium, Copper, lead, nickel and zinc adjusted for effects of hardness: Ca, Mg in WGM/ID5 22.3, 290 mg/L: in Sawyers Swamp Creek 51.6, 38.0 mg/L, respectively	environme environme ting Exceet sing 90th p tolerant crr telerived frorr cal goal fro per, lead, ni	nt monitorin cation) erentile of t pps; irrigatior n Dump Cre ickel and zin	g location) ore-dry plav n. Note: Mc nercentile o oek 90th Pe c adjusted	coment data coment data contraction for effects of for effects of	1) drinking is 0.1 - TDS/0.77; t	35 mg/L Creek TDS d Tr local goal · Ca, Mg in W	lerived from from bore E GM1/D5 22	10.68 × 2 36 90th p 1.3, 29.0 r	200 µS/cm, v ercentile (dat	which is the , ta for both) yers Swamp	ANZECC (20 . Creek 51.6,	00) low land 38.0 mg/L, r	river conduc espectively	tivity for pr	from 0.68 x 2200 µS/cm, which is the ANZECC (2000) low land river conductivity for protection of aquatic life ore D6 90th percentile (data for both) 15 22.3, 29.0 mg/L: in Sawyers Swamp Creek 51.6, 38.0 mg/L, respectively	atic life	-	-			

Table 4-4 Summary Statistics 2018-2019 Groundwater Monitoring Results (mg/L) – 95<sup>th</sup> Percentiles

#### Groundwater Bore D5 – Receiving Site

As outlined in Section 3.3, the groundwater WQGVs apply to bore D5 only, which is designated as the groundwater receiving site. The results presented in Table 4-4 indicate that concentrations of key parameters in groundwater water samples collected from Groundwater Bore D5 (from the 2018-2019 monitoring period) show a number of variable exceedances of the adopted WQGVs, including:

- pH (below ANZECC lower limit)
- Aluminium (exceeds Local WQGV)
- Boron (exceeds Local WQGV)
- Cadmium (exceeds ANZECC WQGV)
- Chromium (exceeds ANZECC WQGV)
- Copper (exceeds ANZECC WQGV)

- Iron (exceeds Local WQGV)
- Mercury (exceeds ANZECC WQGV)
- Manganese (exceeds ANZECC WQGV)
- Nickel (exceeds Local WQGV)
- Lead (exceeds Local WQGV)
- Zinc (exceeds local WQGV)

The chemical signature (pattern and concentration of elevated key parameters) of D5 are comparable with the chemical signatures of Bore D6 and AP09 and similar to AP17 and the KVAD Seepage, due to elevated concentrations and exceedances of AI, B, Cd, Fe, Mn, Ni, and Zn and low pH at all locations. Concentrations in D5 are notably lower for F, Fe, SO<sub>4</sub>, conductivity and TDS than for D6, AP09, AP17 and the KVAD Seepage monitoring point.

The mechanisms affecting water quality in D5 are discussed in detail in Sections 5.2.1, and 6 of this report. The results from historic review and assessment of recent (2018-2019 results) indicate that placement of dry ash within the KVAR may potentially be affecting water quality in bore D5. However, it is noted that discharge from Springvale mine has influenced water quality in D5 through local recharge of groundwater upgradient of the KVAR and adjacent to Bore D5 and through local seepage to D5 via SSC.

Due to the complexity of current and historic land use activities, including local chitter deposits, pumping and discharge regimes for the KVAD and SSCAD, it is not conclusive (based on the data set available) to directly attribute water quality impacts observed in groundwater in Bore D5 solely to a single source such as the KVAR.

#### **KVAR / KVAD**

The concentrations of key parameters within Bores D6, AP09, AP17 and the KVAD seepage (Site 94) monitoring point also variably exceed the WQGVs outlined above for D5, along with exceeding ANZECC (2000) WQGVs for:

Conductivity

Fluoride

Total dissolved solids

Selenium (AP17 and KVAD Seep)

Sulfate

A review of the historic water quality monitoring results for Site 94 (Section 5.2.2) indicates a reduction in concentrations of all water quality parameters at the start of the 2017-2018 monitoring period, and subsequent results that are both reduced and notably inconsistent with previous years. It was originally suggested that this change could likely reflect a change in the sampling location for Site 94, however the 2018-2019 monitoring data indicated a return to the long-term values and trends. The irregular 2017/2018 data has thus been omitted from the long-term dataset.

Similar to D5, identification of the factors currently affecting water quality in bore D6 is not conclusive without consideration of baseline (pre-dry ash placement) conditions of long term water quality trends for D6, due to the long history of water quality impacting activities locally affecting the KVAR area, including wet ash / coal reject placement in the KVAD (1960-1980), and wet ash placement in the SSCAD (1980-2003).

The mechanisms affecting water quality in D6 are discussed in detail in Sections 5.2.2, and 6 of this report. The results from historic review and assessment of recent (2018-2019 results) indicate that placement of dry ash within the KVAR may currently be affecting water quality in bore D6.

Due to the complexity of current and historic land use activities, including local chitter deposits, pumping and discharge regimes for the KVAD and SSCAD, it is not conclusive (based on the data set available) to directly attribute water quality impacts observed in groundwater in Bore D6 solely to a single source such as the KVAR.

#### SSC / SSCAD and Boreholes Upgradient of KVAR

Groundwater chemistry of two of the sample sites upgradient of the KVAR and downgradient of the SSCAD (Bores D2 & D4) show statistically comparable chemical signatures between sampling points. For these two monitoring bores the concentrations of key parameters are generally below the adopted WQGVs with the exception of:

pH (below ANZECC lower limit)

- Iron at D4 (exceeds Local WQGV)
- Boron at D4 (exceeds Local WQGV)
- Manganese at D4 (exceeds ANZECC WQGV)

A review of the historic water quality monitoring results for bore D2 (Site 33) (Section 5.2.3) indicates that low pH levels currently observed at bore D2 reflect current conditions from a long-term trend of declining pH. Long trends for other water quality parameters including the indicator parameters Mn, B, Ni, SO<sub>4</sub> and conductivity show that the current water quality at bore D2 does not show impacts from KVAR ash placement or associated activities.

Concentrations of the key parameters Cd, Fe, Ni and Zn are elevated to levels exceeding WQGVs within bore D3 (Site 34). The mechanisms affecting water quality in bore D3 are discussed in greater detail in Sections 5.2.3, & 6 of this report as the current concentrations of water quality parameter must be described in context with recent historical activities and mechanisms that currently affect water quality.

Notably from Sections 5.2.3, & 6, it is determined that a commencement of discharge from Springvale Mine at LDP009 has resulted in a rise in groundwater levels in the south-east corner of the KVAR, proximal to bore D3. The rise in groundwater levels is theorised to have resulted in migration of groundwater into the dry ash KVAR, resulting in recent (post June 2013) changes to water quality which currently affect the water quality in bore D3, along with compound effects on water quality in the KVAR / KVAD sampling bores and downgradient sites D6 and D5.

Current groundwater quality at bore D4 (Site 34) is complexly influenced by both discharge from Springvale Mine, cross gradient groundwater flow from KVAR / KVAD and seepage from SSCAD. Historical influences of these factors are discussed in Sections 5.2.3, & 6 of this report. Overall groundwater in bore D4 is generally reflective of the water quality Springvale Mine with lesser influences from KVAR / KVAD. Due to the complexity of the water quality at D4, potential impacts from KVAR cannot be evaluated, however the current engineering mechanisms and near neutral pH indicate that the KVAR is unlikely to be affecting water quality at bore D4.

#### **Boreholes Upgradient SSCAD**

A single groundwater sample was collected over the 2018-2019 monitoring period from Borehole D1– Located in the middle-upper portions of the SSC catchment, upgradient of the SSCAD. This sample was taken in February 2019. The bore was either dry or inaccessible for the period preceding and succeeding this.

The chemical signature of groundwater samples from Bore D1 are distinctly different from those within and downgradient of the KVAR area, with pH being the only parameter not meeting the adopted WQGVs. Groundwater quality in D1 is reflective of the catchment conditions that are unaffected by the SSCAD, KVAR and KVAD.

# 5 Surface Water and Groundwater Trends

## 5.1 Surface Water Trends 1992 – 2019

To assess effects of the dry ash emplacement within the KVAR on surface water quality it is necessary to analyse both recent concentrations and long-term trends in concentrations of key physical and chemical stressors / toxicants within the selected surface water monitoring sites.

As outlined in Section 2.5, surface water and groundwater flows through the site are complexly modified by the extensive engineering aspects influencing the site, including:

- Diversion drains through the KVAR / KVAD draining surface water and groundwater to various sumps (i.e. Sumps 1-3), Ponds, Return Water Canal and to Lidsdale Cut
- Recirculation pumping of SSCAD seepage collected through the SSCAD V-notch back to the SSCAD Pond via the Return Canal
- Recirculation pumping of water from Lidsdale Cut to the SSCAD Pond via the Return Canal

The 95<sup>th</sup> Percentile of results have been tabulated for periods corresponding with pre-dry ash emplacement (1991-2003), syn-dry ash emplacement / pre-stoppage of pumping into SSC from LC (2003-2012) and post dry-ash emplacement (2012-2019) / LC to SSCAD recirculation. These key events mark periods of marked water quality changes for the surface water receiving site (WX7) and other surface water sampling points.

It is also noted that blockage of the KVAD toe drains (2006), unblocking of the KVAD toe drains (2010), commencement of pumping from Lidsdale Cut to SSCAD via the Return Canal (July 2012) and commencement of discharge from Springvale Mine to SSC at LDP009 (July 2013) have had marked effects on surface water quality, these aspects are discussed within the evaluation of the long-term surface water trends.

Sample Location         Date Range           Springvale (158)         2011-2018           SSC WX7 (41)         1991-2003           SSC WX7 (41)         2003-2012	nge pH	Cond	TDS	SO4	Ū	AI*	As	Ag	Ba Be	e e	B	ບັ	Сп	u.	Fe-F	Hg	Mn	Mo	ī	Pb	Se	Zn*
																						-
								Sprin	Springvale Discharge	arge												
	18 8.2	1200	611	45.8	10.1	0.45	0.032	0.0005	0.03 0.0005	0.13	3 0.0001	0.002	0.004	1.3	0.52	0.00002	0.02	0.05	0.005	0.001 0	0.001	0.024
							Saw	'yers Swar	awyers Swamp Creek (Receiving Site)	ceiving Si	te)											
2003-201	03 7.8	847	603	345	48.4	0.57	0.001	0.001	0.04 NI	ND 2.39	0.001	0.001	0.009	1.34	0.742	0.0002	0.920	QN	QN	0.003 0	0.003	0.18
	12 8.6	1494	1152	710	32.1	85.8	0.025	0.001	0.08 0.005	05 3.21	1 0.0054	0.005	0.010	2.12	0.224	0.0001	5.04	0.02	0.45	0.014 0	0.003	0.83
2012-2019	19 8.8	1260	780	116	12.1	1.33	0.030	0.001	0.04 ND	D 0.34	4 0.0002	0.002	0.004	1.40	0.08	0.00005	0.38	0.05	0.03	0.003 0	0.001	0.09
							Saw	rers Swam	Sawyers Swamp Creek (Additional Sites	ditional Sit	es)											
Upstream SSCAD WX1 (92) 1992	6.2	3000	QN	QN	ø	0.12	QN	QN	N	ND 0.042	ND 2	QN	Q	QN	0.435	QN	0.068	QN	QN	QN	QN	0.04
[Dry since April 2017] 2003-2012	12 ND	QN	Q	Q	Ð	Q	QN	QN	N	DN DN	Q	Q	Q	Q	QN	QN	QN	QN	QN	QN	QN	QN
2012-2017	17 6.8	162	152	31.5	12	3.55	0.001	0.001	DN DN	D 0.06	6 0.0002	0.003	0.009	0.1	2.98	0.00006	0.523	0.01	0.01	0.005 C	0.002	0.05
Downstream v-notch (93) 2012-2019	19 8.7	1260	780	62	13.4	0.88	0.030	0.001	0.04 ND	D 0.21	1 0.0002	0.002	0.005	1.40	0.13	0.00005	0.50	0.05	0.01	0.002 0	0.001	0.03
Downstream KVAR (83) 2010-2012	12 8.6	1030	QN	346	33	1.7	0.004	0.001	0.09 0.002	02 1.23	3 0.0002	0.003	0.003	1.08	0.618	0.00005	1.5	0.02	0.01	0.002 C	0.002	0.04
2012-2019	19 8.7	1252	793	234	21.0	0.9	0.030	0.001	0.06 0.002	02 0.86	6 0.0002	0.002	0.002	1.48	0.31	0.00005	0.56	0.05	0.01	0.001 0	0.002	0.03
Spillway (225) 2013-2019	19 8.5	1260	760	38.9	6.7	0.8	0.030	0.001	0.03 NI	ND 0.15	5 0.0001	0.002	0.003	1.48	0.05	0.00005	0.50	0.05	0.01	0.002 0	0.001	0.03
									SSCAD													
SSCAD (38) 1996-2003	03 6.5	1946	1514	980	58	Q	0.036	0.001	0.15 0.009	09 7.87	7 0.0141	0.0154	0.017	11.2	0.345	0.0002	1.57	0.19	0.15	0.005 C	0.316	0.54
2003-2012	12 7.2	2456	1941	1391	42.1	7.37	0.050	0.01	0.1 0.008	08 7.90	0.0108	0.01	0:030	10.15	QN	0.0001	1.82	60.0	0.14	0.01 0	0.171	0.47
2012-2019	19 4.6	1700	1288	855	21.1	13.6	0.005	0.001	0.08 ND	D 3.50	0.007	0.002	0.019	4.54	0.26	0.00005	3.12	0.04	0.20	0.002	0.007	0.58
SSCAD V-Notch (79) 2010-2012	12 8.0	2015	1580	970	52.8	1.58	0.001	0.001	0.06 0.001	01 2.88	0.0009	0.002	0.005	1.5	0.03	0.00005	0.376	0.01	0.02	0.002 0	0.002	0.12
2012-2019	19 8.1	2456	1918	1331	56.3	10.0	0.016	0.001	0.06 ND	D 2.38	8 0.008	0.003	0.014	2.43	2.31	0.00005	8.74	0.04	0.27	0.005 0	0.002	0.41
								×	KVAR / KVAD													
West KVAD seepage left (81) 2010-2012	12 3.1	2949	2300	1500	30.8	71.1	0.003	0.001	0.02 0.017	17 8.90	0.0017	0.008	0.047	3.88	68.7	0.00005	16.8	0.010	1.2	0.009 C	0.002	1.59
2015-2017	17 3.1	2794	2066	1392	27.1	39.7	0.006	0.0005	0.02 NI	ND 5.92	0.0008	0.007	0.026	15.2	70.6	0.0001	8.54	0.0005	0.39	0.007 0	0.005	0.84
West KVAD seepage right (80) 2010-2012	12 3.2	3265	2580	1700	39.8	22.8	0.001	0.001	0.02 0.017	17 8.90	0.0013	0.001	0.007	7.1	13.8	0.00005	19	0.010	1.6	0.011 0	0.002	2.08
2015-2019	19 2.9	4783	4203	2943	36.7	50.5	0.002	0.001	0.01 NI	ND 15.3	3 0.002	0.001	0.002	21.1	63.4	0.00002	24.8	0.002	2.76	0.002 0	0.003	3.75
Nth Wall collection (86) 2012	12 4.8	1094	740	447	21.9	3.0	0.007	0.001	0.04 0.002	02 2.29	0.0002	0.001	0.005	0.4	10	0.00005	3.69	0.010	0.06	0.005 0	0.002	0.13
2013-2019	19 2.9	5097	4380	2921	41.3	115	0.018	0.001	0.02 ND	D 13.2	2 0.032	0.008	0.028	59.9	99.3	0.00005	18.2	0.003	1.40	0.001 0	0.004	3.60
Surface water runoff (87) 2010-2012	12 5.0	2395	1895	1580	25	126	0.001	0.001	0.07 0.002	02 3.18	8 0.002	0.009	0.013	1.97	22.6	0.00005	8.94	0.010	0.20	0.001 0	0.004	0.48
2015-2019	19 3.2	5090	5150	3407	29.3	93.5	0.049	0.001	0.01 ND	D 12.9	0.001	0.003	0.006	90.8	189	0.00002	17.0	0.002	1.62	0.001	0.064	4.66
								_	Lidsdale Cut													
Lidsdale Cut WX5 (40) 1991-2003	03 6.0	1061	657	383	60.4	3.12	0.001	0.001	0.04 ND	D 2.17	7 0.001	0.008	0.005	2.11	0.85	0.0002	2.255	QN	QN	0.0038 0	0.001	0.35
2003-2012	12 7.3	2385	1920	1410	35.5	20.5	0.050	0.01	0.07 0.026	126 7.10	0.005	0.01	0.010	13.5	14.1	0.0001	11.1	0.038	0.94	0.01 0	0.006	1.22
2012-2019	19 3.1	4196	4290	3660	33.8	180	0.030	0.001	0.08 ND	D 13.9	9 0.044	0.022	0.047	35.3	21.0	0.00005	17.1	0.001	1.59	0.033 0	0.085	3.16
								-	Dump Creek													
Dump Creek WX11 (39) 1991-2003	03 8.0	1025	006	458	59.3	0.34	0.001	0.001	0.05 ND	D 1.97	7 0.001	0.008	0.002	1.16	5.26	0.0002	1.89	QN	QN	0.001 0	0.003	0.28
2003-2012	12 5.9	1695	1195	749	25.0	1.6	0.050	0.01	0.03 0.005	05 2.90	0.002	0.01	0.010	1.1	6.39	0.0001	7.26	0.01	0.45	0.01 0	0.006	1.1
2012-2019	19 3.1	2028	1500	1046	35.2	6.13	0.001	0.001	0.04 ND	D 3.71	0.001	0.002	0.016	11.4	13.2	0.00005	8.10	0.01	0.70	0.009 0	0.002	1.83
									WQGVs									-	-	-		
Surface Water WQGV	6.5-8.0	8.0 2200	1500^	1000++	350+	5.25^^	0.024 0	0.00005 0	0.7+++ 0.1	1 1.25	<u>5</u> 0.0015	0.005	0.005	1.5+++	0.3+++	0.00006	1.9	0.01+	0.05	0.005 C	0.005	0.153
Additional notes: See Table 4-2																						

Table 5-1 Summary Statistics Long Term Surface Water Monitoring Results (mg/L) – 95th Percentiles

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# 5.1.1 WX7 – Surface Water Receiving Site

# 1991-2003

# Sawyers Swamp Creek (WX7 / Site 41)

Surface water samples collected for WX7 during this period represent surface water quality of SSC receiving site concurrent with emplacement of wet ash within SSCAD, post KVAD wet ash emplacement and pre KVAR dry ash emplacement.

The results presented in Table 5-1 indicate that the 95<sup>th</sup> percentile concentrations in surface waters of WX7 were generally below the adopted WQGVs during the 1991-2003 monitoring period, with the exception of B, Fe, and Zn which marginally exceeded the WQGVs.

Figure A1 Appendix A presents a time-series chart of the concentrations of indicator parameters AI, Mn, B, Ni, SO<sub>4</sub>, and conductivity for the period between 1991 and 2018 for WX7. There is a gap in available data between January 1998 and April 2002. The chart shows a rising trend in conductivity and concentrations of SO<sub>4</sub>, Mn and B in the period between 1991 and 1998. Additional parameters including Ca, CI, F, K, Mg, & Na (not presented) show similar rising trends during this period.

Water quality trends in the 1998-2002 period cannot be determined due to the gap in available data. However, the elevated concentration of water quality parameters (including indicator parameters Conductivity, SO<sub>4</sub>, B, Mn) and reduced pH in 2002, relative to concentrations in 1991, indicates that land use activities pre-dating KVAR dry ash emplacement (i.e. SSCAD wet ash emplacement) have influenced surface water quality in SSC at WX7.

2003-2012

### Sawyers Swamp Creek (WX7 / Site 41)

Surface water samples collected for WX7 during this period represent surface water quality of SSC receiving site concurrent with emplacement of dry ash for Stages 1 and 2 of the KVAR and up to the cessation of pumping from LC to SSC.

The results presented in Table 5-1 indicate that the 95<sup>th</sup> percentile concentrations of water quality parameters in surface waters of WX7 generally increased from baseline values (1991-2003) during the 2003-2012 period including concentrations of SO<sub>4</sub>, Cl, Al, As, B, Cu, F, Mn, and Zn. 95<sup>th</sup> Percentile concentrations of Al, As, Cd, Cu, F, Mn, and Pb now exceed the WQGVs, in addition to B and Zn. Additional parameters including Mo and Ni are now reported and noted to also exceed the WQGVs. Concentrations of Fe have dropped below the WQGV.

Figure A1 Appendix A presents a time-series chart of the concentrations of indicator parameters AI, Mn, B, Ni, SO<sub>4</sub>, and conductivity for the period between 1991 and 2019 for WX7. The chart shows that concentrations of SO<sub>4</sub> increased gradually during the 2003-2012 monitoring period, whilst concentrations of B and Ni remained relatively stable and Mn gradually decreased up to 2009. The observed signal of indicator parameters from 2003 to 2009 indicates that dry ash placement within the KVAR did generally not affect water quality in SSC at WX7 during this period, as observed trends are consistent with pre-KVAR water quality trends.

Following April 2009 concentrations of indicator parameters conductivity, SO<sub>4</sub>, Mn, B, and Ni fluctuate significantly relative to average variance resulting in higher average and 95<sup>th</sup> percentile concentrations. As, Ba, Cd, and F also show increased concentrations and rising trends following April 2009. There is also a significant increase in pH (pH 8.6) resulting in moderately alkaline conditions in SSC at WX7, which is indicative of a bottom ash type signature (Ward et al., 2009).

The observed shift in concentrations and increase in variability of water quality following is concurrent with completion and capping of the Stage 1 KVAR area and subsequent commencement of ash emplacement in the Stage 2 KVAR area. These results indicate that Stage 2A KVAR dry ash placement activities may have contributed to an increase in overall average and 95<sup>th</sup> percentile concentrations, and increased variability in

concentrations of a number of water quality parameters in Sawyers Swamp Creek, at WX7 between 2009 and 2012 – which until June 2012 received water directly from Lidsdale Cut Pond.

Due to the complexity of current and historic land use activities, including local chitter deposits, pumping and discharge regimes for the KVAD and SSCAD, it is not considered conclusive to directly attribute any impacts observed to surface water quality changes in WX7 solely to a single source such as the KVAR without further investigation.

# 2012-2019

### Sawyers Swamp Creek (WX7 / Site 41)

Surface water samples collected for WX7 during this period represent surface water quality of SSC receiving site at the cessation of pumping from LC to SSC and commencement of return circulation to LC to SSCAD via the Return Canal in June / July 2012. Commencement of discharge from Springvale colliery also occurred during this period along with completion of the Stage 2A KVAR.

The results presented in Table 5-1 indicate that the 95<sup>th</sup> percentile concentrations of water quality parameters in surface waters of WX7 generally decreased following the cessation of pumping from LC to SSC in June 2012. As a result, the 95<sup>th</sup> percentile concentrations of all parameters were below WQGVs with the exception of Mo and As which remained marginally above the adopted WQGVs, and pH which exceeded the upper limit.

Figures A1 and A2 in Appendix A presents two time-series charts of the concentrations of indicator parameters AI, Mn, B, Ni, SO<sub>4</sub>, and conductivity for the period between 1991 and 2019 for WX7. The chart shows that concentrations of all water quality parameters dropped significantly immediately following the June 2012 event when pumping from Lidsdale Cut to SSC ceased. It is noted that the declining trends for AI, B, Ni and SO<sub>4</sub> are acutely interrupted, and/ or reversed (i.e. Aluminium) in July 2013, at which point discharge from Springvale Mine commences and subsequently dominates water quality characteristics at WX7.

With cessation of pumping from Lidsdale Cut to SSC in June 2012, indication of impacts on water quality at WX7 as a result of dry ash emplacement associated with the Stage 2A KVAR emplacement are no longer evident. Furthermore, due to the influence of discharge from Springvale Mine, the concentrations of several parameters, including indicator parameters Mn, B and SO<sub>4</sub> are lower than the pre-dry ash emplacement (1991-2003) values. As such, in accordance with recent 2018-2019 monitoring results, it can be determined that the KVAR is not currently affecting water quality in SSC at WX7 at a quantifiable level.

# 5.1.2 Sawyers Swamp Creek Additional Sites

1992

#### Upstream SSCAD - WX1 (Site 92)

Surface water samples collected for WX1 during this period represent water quality at the upper-middle portions of the SSC catchment, upgradient of the SSCAD adjacent to groundwater monitoring point D1, during wet ash emplacement in SSCAD. The site is located downgradient of Springvale Mine.

The results presented in Table 5-1 indicate that the 95<sup>th</sup> percentile concentrations in surface waters of WX1 were generally below the adopted WQGVs during the 1992 monitoring period, with the exception of Fe, which was recorded at roughly twice the adopted WQGV (0.76mg/L) and conductivity ( $3000\mu$ s/cm). pH was below the lower limits of the adopted WQGVs.

No data is available for WX1 between 1992 and March 2012.

#### Downstream SSCAD V-Notch (site 93), Downstream KVAR (Site 83), Spillway 225

No water quality data is available for these sample sites prior to 2010.

# WX1 (Site 92), Downstream V-Notch (site 93), Spillway 225

No water quality data is available for these sites during the 2003-2012 monitoring period.

#### Downstream KVAR (Site 83)

Surface water quality data is available for Downstream KVAR (Site 83) during the period between 2010 and 2012, corresponding with Stage 2A dry ash emplacement. The site samples surface water immediately north of the KVAR and upgradient (east) of Lidsdale Cut and represents surface water in SSC.

The results presented in Table 5-1 indicate that the 95<sup>th</sup> percentile concentrations in surface waters of Downstream KVAR are all below the adopted WQGVs, with the exception of Fe and Mo, which are marginally elevated above the WQGV.

Figure A4 Appendix A presents a time-series chart of the concentrations of indicator parameters AI, Mn, B, Ni, SO<sub>4</sub>, and conductivity for the period between 2010 and 2012 for the Downstream KVAR monitoring site (Site 83). The chart shows a variable trend in the concentration of water quality parameters during this period, characterised by a distinct decreasing trend in concentrations of water quality parameters between Feb 2010 and December 2010, followed by an overall rise in concentrations between December 2010 and November 2011.

Results from this period may reflect the particularly wet conditions in early 2011, which resulted in localised flooding of the KVAR and potential impacts on SSC at Site 83; or the installation of subsurface drains in the KVAR and unblocking of the KVAD toe drains causing subsequent limited seepage into SSC adjacent to the KVAD toe drains. Regardless of the cause, water quality parameters in SSC at Site 83 were generally below the adopted WQGVs during this period and therefore limited to negligible impact from KVAR on Site 83 are observed.

2012-2019

### Upstream SSCAD WX1 (Site 92)

This site has been dry since April 2017.

The results presented in Table 5-1 indicate that the 95<sup>th</sup> percentile concentrations of water quality parameters in surface waters of WX1 were generally below the adopted WQGVs during the 2012-2019 monitoring period, with the exception of Cu, Fe and Hg, which marginally exceeded WQGVs.

Figures A3 and A4 in Appendix A presents the time-series charts of the concentrations of indicator parameters AI, Mn, B, Ni, SO<sub>4</sub>, and conductivity for the period between 1992 and 2017 for WX1. The charts show relatively stable trends for all parameters during this monitoring period, with a slight increase in concentrations of Aluminium and slight drop in concentrations of Nickel.

WX1 is located upgradient of both the KVAR and the SSCAD, therefore exceedances of water quality parameters and observed water quality trends are not influenced by the KVAR.

### Downstream V-Notch (Site 93)

Surface water samples collected for Downstream V-Notch (Site 93) represent surface water quality of SSC cross-gradient and north of the KVAR Sedimentation Area and downgradient and west of the SSCAD / downgradient-north of the Springvale Mine Discharge Point (LDP009).

The results presented in Table 5-1 indicate that the 95<sup>th</sup> percentile concentrations of water quality parameters in surface waters at the Downstream V-Notch monitoring point (Site 93) are generally below the adopted WQGVs, with the exception of As, Cu and Mo which are marginally elevated above the WQGVs. pH is moderately alkaline at pH 8.7.

Figures A5 and A6 in Appendix A presents time-series charts of the concentrations of indicator parameters AI, Mn, B, Ni, SO<sub>4</sub>, and conductivity for the period between 2012 and 2019 for Downstream V-Notch. The charts show relatively stable to slightly decreasing trends of all indicator parameters, with the exception of conductivity, which shows a slight increasing trend that corresponds with increasing concentrations of K, Na and F.

The elevated water quality parameters and observed water quality trends at Site 93 during the 2012-2019 monitoring period are attributed to discharge from Springvale Mine at LDP009, which since 2013 has dominated the water quality in SSC. As such the concentrations of water quality parameters at Site 93 are reflective of the water quality sample at the discharge point (Site 158). The results indicate that the KVAR does not have a measurable effect on water quality in SSC at Site 93.

# Downstream KVAR (Site 83)

The results presented in Table 5-1 indicate that the 95<sup>th</sup> percentile concentrations of water quality parameters in surface waters at the Downstream KVAR monitoring point generally decreased during the 2012-2019 monitoring period, compared to 2010-2012 records for Downstream KVAR, with the exception of As, Mo, F and overall conductivity, which increased marginally. The increase in conductivity is attributed to a general increase in the concentrations of potassium, which is not considered in the current key water quality parameters. pH is moderately alkaline at pH 8.7.

Figures A7 and A8 in Appendix A presents the time-series charts of the concentrations of indicator parameters AI, Mn, B, Ni, SO<sub>4</sub>, and conductivity for the period between 2012 and 2019 for Downstream KVAR. The chart shows relatively stable to decreasing trend for all parameters, but with slight increase in conductivity as a result of increasing potassium (K) concentrations.

The elevated water quality parameters and observed water quality trends at Site 83 during the 2012-2019 monitoring period are attributed to discharge from Springvale Mine at LDP009, which since 2013 has dominated the water quality in SSC. As such the concentrations of water quality parameters at Site 83 are reflective of the water quality sample at the discharge point (Site 158). The results indicate that the KVAR does not have a measurable effect on water quality in SSC at Site 83.

# Spillway (Site 225)

Surface water samples collected for Spillway 225 represent surface water quality of the SSC at the SSCAD Spillway (Site 225).

The results presented in Table 5-1 indicate that the 95<sup>th</sup> percentile concentrations of water quality parameters in surface waters at the SSCAD Spillway are generally below the adopted WQGVs with the exception of As and Mo, which are marginally above the WQGVs.

Figures A9 and A10 in Appendix A present time-series charts of the concentrations of indicator parameters Al, Mn, B, Ni, SO<sub>4</sub>, and conductivity for the period between 2013 and 2019 for Spillway 225 (2012 data not available). The chart shows generally stable to declining concentrations for key water quality parameters with the exception of conductivity which presents a slight increasing trend. Increasing conductivity is largely driven by rising concentrations of K, Cl and Na which show distinct increasing trends over the monitoring period (not presented) and potentially representing evaporative salinization of the SSCAD Pond due to recent dry (El Nino type) conditions.

The elevated water quality parameters and observed water quality trends at Site 225 during the 2013-2019 monitoring period are primarily attributed to discharge from Springvale Mine at LDP009, which since 2013 has dominated the water quality in SSC. As such the concentrations of water quality parameters at Site 225 are reflective of the water quality sample at the discharge point (Site 158). The results indicate that the KVAR does not have a measurable effect on water quality in SSC at Site 225.

# 5.1.3 SSCAD Sites

1996-2003

# SSCAD (Site 38)

Surface water samples collected for SSCAD 38 represent surface waters of the return canal that have been pumped from LC or have been received from the SSCAD v-notch and are to be pumped to the SSCAD. Surface water samples collected for this monitoring period represent conditions pre-KVAR dry ash placement.

The results presented in Table 5-1 indicate that the 95<sup>th</sup> percentile concentrations of water quality parameters in surface waters at the SSCAD 38 monitoring site generally exceeded the adopted WQGVs during the 1996-2003 monitoring period, including concentrations of As, B, Cd, Cr, Cu, F, Fe, Mo, Ni, Se and Zn.

Figures A11 and A12 in Appendix A present time-series charts of the concentrations of indicator parameters AI, Mn, B, Ni, SO<sub>4</sub>, and conductivity for the period between 1996 and 2019 for SSCAD 38. The results show generally increasing concentrations up to 2003 for SO<sub>4</sub>, Mn, B, Ni and conductivity (SO<sub>4</sub> being the primary contributor to salinity). No data is available for aluminium trends during this monitoring period.

Water quality trends for the 1996-2003 monitoring period indicated generally elevated concentrations of water quality parameters and increasing concentrations in several indicator parameters up to 2003 and preceding dry ash placement in the KVAR.

# SSCAD V-Notch (Site 79)

Surface water samples collected for SSCAD V-Notch (Site 79) represent surface water quality representative of the SSCAD Seepage Collection System. No data is available for the SSCAD V-Notch (Site 79) prior to 2010.

2003-2012

### SSCAD (Site 38)

The results presented in Table 5-1 indicate that the 95<sup>th</sup> percentile concentrations of water quality parameters in surface waters at the SSCAD 38 monitoring site were generally higher during the 2003-2012 monitoring period than preceding 1996-2003 monitoring period, including concentrations of SO<sub>4</sub>, As, B, Cu, Mn, and conductivity. Concentrations of other water quality parameters remained stable or decreased marginally. It is noted that although 95<sup>th</sup> percentile concentrations are higher during the 2003-2012 monitoring period than the preceding 1996-2003 monitoring period, the elevated concentrations are a result of the increasing trends during the 1996-2003 monitoring period, and therefore do not directly reflect an influence by the KVAR, but are coincident with SSCAD ash placement activities.

Figures A11 and A12 in Appendix A present time-series charts of the concentrations of indicator parameters AI, Mn, B, Ni, SO<sub>4</sub>, and conductivity for the period between 1996 and 2019 for SSCAD 38. The results show a steady decreasing trend in all parameters between 2003 and February 2010, following which point concentrations of Mn, Ni, AI, and B become stable to increasing in trend with greater variability in concentrations.

The shift in trends and increased variability in concentrations of indicator parameters is coincident with unblocking of the KVAD toe drains being and commencement of Stage 2 dry ash emplacement, and suggests leachate migration through sub-surface drains directly to the Return Canal, where the SSCAD 38 sample point is located.

### SSCAD V-Notch (Site 79)

The results presented in Table 5-1 indicate that the 95<sup>th</sup> percentile concentrations of water quality parameters in surface waters at the SSCAD V-Notch (Site 79) monitoring point (available for the period between 2010 and 2012) indicate that concentrations of water quality parameters were generally below the adopted WQGVs during 2010-2012, with the exception of B, and overall TDS.

Figures A13 and A14 in Appendix A present time-series charts of the concentrations of indicator parameters AI, Mn, B, Ni, SO<sub>4</sub>, and conductivity for the period between 2010 and 2019 for SSCAD V-Notch (Site 79). Concentrations of indicator water quality parameters are generally stable with minor fluctuations during the 2010-2012 monitoring period for SSCAD V-Notch (Site 79).

The water quality at the SSCAD V-Notch Site is reflective of the SSCAD and is not directly affected by the KVAR.

2012-2019

# SSCAD (Site 38)

The results presented in Table 5-1 indicate that the 95<sup>th</sup> percentile concentrations of water quality parameters in surface waters at the SSCAD 38 monitoring site generally decreased during the 2012-2019 monitoring period, with the exception of AI, Mn, Ni, and Zn. Concentrations of AI, B, Cd, Cu, F, Mn, Mo, Ni, Se and Zn were above the WQGVs.

Figures 11 and 12 in Appendix A present time-series charts of the concentrations of indicator parameters Al, Mn, B, Ni, SO<sub>4</sub>, and conductivity for the period between 2013 and 2019 for SSCAD 38. Data is not available for the period between February 2012 and April 2013.

The results show a decrease in  $SO_4$  and overall conductivity continuing the trend from the 2003-2012 monitoring period, however rising trends in Mn, Ni, Al and B are observed in the 2012-2018 monitoring period, in contrast to earlier declining trends. Review of the available data indicates an alternate or combination of two possible causes of the rising trend: a) Stage 2 dry ash emplacement; and/or b) pumping from LC to SSCAD via the Return Canal from July 2012.

Following July 2013, the concentrations of water quality parameters become highly volatile within the observed rising / falling trends. This volatility is attributed to the commencement of discharge from Springvale Mine at LDP009, affecting water quality in SSCAD 38.

As of January 2018, the observed concentrations of all water quality parameters have been declining.

# SSCAD V-Notch (Site 79)

The results presented in Table 5-1 indicate that the 95<sup>th</sup> percentile concentrations of water quality parameters in surface waters at the SSCAD V-Notch (Site 79) monitoring site generally increased during the 2012-2019 monitoring period in comparison to the 2003-2012 monitoring period for SO<sub>4</sub>, Cl, Al, As, Cd, Cr, Cu, F, Fe, Mn, Mo, Ni, Pb, and Zn. Other water quality parameters remained stable or decreased during this monitoring period.

Figures A13 and A14 in Appendix A present time-series charts of the concentrations of indicator parameters Al, Mn, B, Ni, SO<sub>4</sub>, and conductivity for the period between 2012 and 2019 for SSCAD V-Notch (Site 79). Data is not available for the period between February 2012 and April 2013. Results show that concentrations of water quality parameters are generally stable up to July 2013, following which point the concentrations of indicator parameters become highly volatile with an overall stable trend.

# 5.1.4 KVAR / KVAD Sites

### 1988-2010

No information is available for KVAR/KVAD monitoring sites during this period.

### 2010-2012

### West KVAD Wall Seepage Left (Site 81)

Surface water samples collected for KVAD Seepage Left (Site 81) sample the KVAD Toe Drain along the north-western wall of the Stage 2 KVAR area. The results presented in Table 5-1 indicate that the 95<sup>th</sup> Project number 502838 File 20190624\_502838\_KVAR\_WQ\_Assessment\_2019.docx 2019-06-24 Revision 1 **38**  percentile concentrations of water quality parameters in surface waters at Site 81, during the 2010-2012 monitoring period, generally exceeded WQGVs (by a significant amount) with the exceptions of Cl, As, Ba, Be, Hg and Se, which were below the adopted WQGVs. pH was below the lower limit of the WQGVs and highly acidic with pH 3.1.

Figures A15 and A16 in Appendix A present time-series charts of the concentrations of indicator parameters AI, Mn, B, Ni, SO<sub>4</sub>, and conductivity for the period between February 2010 and July 2017 for Site 81. For the period between March 2010 and February 2012, the chart shows broad fluctuations for all indicator parameters during this monitoring period with a noticeable decline in all parameters (with the exception of AI) in October 2010 – corresponding with installation of subsurface drains to the Stage 2 area in 2010 and unblocking of the KVAD toe drains in 2011. With the exception of aluminium, concentrations of indicator parameters rose gradually following October 2010 up to February 2012.

The results from Site 81 between 2010 and 2012 indicate that the KVAR dry ash possibly affecting water quality at Site 81. This is evident from the low pH values, typical of a fresh dry ash along with elevated concentration of Al, B, Cr, Zn and relatively low Mo (Ward et al., 2009).

# West KVAD Wall Seepage Right (Site 80)

Surface water samples collected for KVAD Seepage Right (Site 80) sample the KVAD Toe Drain along the north-western wall of the Stage 2 KVAR area. The results presented in Table 5-1 indicate that the 95<sup>th</sup> percentile concentrations of water quality parameters in surface waters at Site 80 generally exceeded the WQGVs, with the exceptions of Cl, As, Ba, Be, Cd, Cr, Hg, Mo and Se, which were below the WQGVs. pH was below the lower limit of the WQGVs and highly acidic with pH 3.2.

Figures A17 and A18 in Appendix A present time-series charts of the concentrations of indicator parameters AI, Mn, B, Ni, SO<sub>4</sub>, and conductivity for the period between February 2010 and March 2019 for Site 80. For the period between March 2010 and February 2012, the chart shows a broad fluctuation for all indicator parameters during this monitoring period, characterised by a declining trend up to October 2010 which is followed by a rising limb up to February 2012. The shift in trend is attributed to installation of subsurface drains to the Stage 2 area and unblocking of the KVAD toe drains, which took place between October 2010 / February 2011.

The results from Site 80 between 2010 and 2012 indicate that the KVAR dry ash possibly affecting water quality at Site 80. This is evident from the low pH values, typical of a fresh dry ash along with elevated concentration of Al, B, Cr, Ni, Zn and relatively low Mo (Ward et al., 2009).

### North Wall Collection (Site 86)

Surface water samples collected for North Wall Collection (Site 86) sample groundwater through flow and subsequent seepage along the northern wall of the KVAD, north of the Stage 2 KVAR. The results presented in Table 5-1 indicate that the 95<sup>th</sup> percentile concentrations of water quality parameters in surface waters at Site 86 were historically generally below the WQGVs, with the exceptions of B, Fe, Mn, and Ni. pH was below the lower limit of the WQGVs and moderately acidic with pH 4.78. The water quality seems to have significantly deteriorated over the recent years.

Figures A19 and A20 in Appendix A present time-series charts of the concentrations of indicator parameters AI, Mn, B, Ni, SO<sub>4</sub>, and conductivity for the period between March 2010 and March 2019 for Site 86. For the period between March 2010 and February 2012, the chart shows a variable series of rising (AI, Mn), falling (SO<sub>4</sub>, B, Cond), and stable (Ni) trends up to November 2010 at which point there is a significant temporary drop in concentrations of all parameters. Following this event, concentrations recover and SO<sub>4</sub>, B and conductivity begin a rising trend, AI and Mn continue to rise, whilst Ni recovers before beginning a gradual declining trend. The shift in trend is attributed to installation of subsurface drains to the Stage 2 area and unblocking of the KVAD toe drains, which took place in October 2010 - February 2011.

The results from Site 86 between 2010 and 2012 indicate that the KVAD is likely to be the primary influence on water quality at Site 86. This is indicated by the relatively less acidic pH value (pH 4.78), and generally lower concentration of water quality parameters, which is indicative of long stored ash (Ward et al., 2009). The observed rising trend in water quality parameters since October 2010 is indicative of increasing influence of the KVAR on water quality at Site 86.

# Surface Water Runoff / West KVAD Wall Subsurface (Site 87)

Surface water samples collected for Surface Water Runoff (Site 87) sample groundwater through flow and subsequent seepage for the West KVAD wall. The results presented in Table 5-1 indicate that the 95<sup>th</sup> percentile concentrations of water quality parameters in surface waters at Site 87 historically generally exceeded the adopted WQGVs with the exceptions of CI, Ba, Be, Hg, Mo, Pb and Se. pH was below the lower limit of the WQGVs and moderately acidic with pH 4.99.

Figures A21 and A22 in Appendix A present time-series charts of the concentrations of indicator parameters AI, Mn, B, Ni, SO<sub>4</sub>, and conductivity for the period between April 2010 and March 2019 for Site 87. For the period between April 2010 and February 2012, the chart shows a broad fluctuation for the majority of indicator parameters (excluding SO<sub>4</sub> and Cond) characterised by stable / declining trends up to October 2010, following which point concentrations of water quality parameters shift into steady rising trends at variable rates of rise. SO<sub>4</sub> and conductivity exhibit a rising trend throughout the monitoring period. The shift from stable / falling to rising trends in concentrations of indicator parameters is attributed to installation of subsurface drains to the Stage 2 area and unblocking of the KVAD toe drains, which took place in October 2010.

The results from Site 87 between 2010 and 2012 indicate that the KVAD is likely to be the primary influence on water quality at Site 87. This is indicated by the relatively less acidic pH value (pH 4.99), and generally lower concentration of water quality parameters, which is indicative of long stored ash (Ward et al., 2009). The observed rising trend in water quality parameters since October 2010 is indicative of increasing influence of the KVAR on water quality at Site 87.

2012-2019

# West KVAD Wall Seepage Left (Site 81)

No data is available for Site 81 between the end of January 2012 and start of April 2015, and after July 2017 (dry). The results presented in Table 5-1 indicate that the 95<sup>th</sup> percentile concentrations of water quality parameters in surface waters at Site 81 (for the period between April 2015 and March 2018) generally decreased in comparison to 2010-2012 concentrations, with the exceptions of As, Ba, F, Fe, and Se, which increased slightly. Despite the overall shift to lower concentrations, the majority of water quality parameters remained above the WQGVs, with the exceptions of (as previous) Cl, As, Ba, Cd, Mo and Se. pH increased slightly but remained highly acidic at pH 3.14.

Figures A15 and A16 in Appendix A present time-series charts of the concentrations of indicator parameters AI, Mn, B, Ni, SO<sub>4</sub>, and conductivity for the period between April 2010 and July 2017 for Site 81. For the period between April 2015 and July 2017, the chart shows that concentrations of key parameters remained relatively stable or with slight decreasing trends with subordinate fluctuations.

The results from Site 81 between 2015 and 2017 indicate that the KVAR dry ash is affecting water quality at Site 81. This is evident from the low pH values, typical of a fresh dry ash along with elevated concentration of Al, B, Cr, Zn and relatively low Mo (Ward et al., 2009).

# West KVAD Wall Seepage Right (Site 80)

No data is available for Site 80 between the end of January 2012 and start of April 2015. The results presented in Table 5-1 indicate that the 95<sup>th</sup> percentile concentrations of water quality parameters in surface waters at Site 80 (for the period between April 2015 and March 2019) generally increased in comparison to 2010-2012 concentrations, with the exceptions of Cl, Ba, Cr, Cu, Hg, Mo, and Pb. Due to changes in water quality, concentrations of Cd rose above WQGVs, whilst Cu and Pb dropped below the WQGVs.

Figures A17 and A18 in Appendix A present time-series charts of the concentrations of indicator parameters AI, Mn, B, Ni, SO<sub>4</sub>, and conductivity for the period between February 2010 and March 2019 for Site 80. For the period between April 2015 and March 2019, the chart shows generally stable concentrations of all indicator parameters. However, it is noted that concentrations of all indicator parameters are higher than 2010-2012 concentrations, indicating a rising trend occurring during the data gap between the end of February 2010 and start of April 2012, likely as a result of installation of subsurface drains to the Stage 2 area and unblocking of

the KVAD toe drains, which took place in October 2010-February 2011, at which time rising trends commenced.

The results from Site 80 between 2015 and 2019 indicate that the KVAR dry ash is affecting water quality at Site 80. This is evident from the low pH values, typical of a fresh dry ash along with elevated concentration of Al, B, Cr, Ni, Zn and relatively low Mo (Ward et al., 2009).

#### North Wall Collection (Site 86)

No data is available for Site 86 between the end of January 2012 and start of April 2013. The results presented in Table 5-1 indicate that the 95<sup>th</sup> percentile concentrations of water quality parameters in surface waters at Site 86 (for the period between April 2014 and March 2019) significantly increased in comparison to 2010-2012 concentrations with the exceptions of Ba, Mo and Pb, which decreased slightly. pH decreased to highly acidic conditions at pH 2.9. The shift in water quality between the 2010-2012 and 2014-2019 monitoring periods is considerable at site 86. During the 2010-2012 monitoring period, the majority of water quality parameters were below the adopted WQGVs, whereas, during the 2014-2019 monitoring period, the majority of water quality of water quality parameters exceeded the WQGVs, with the exceptions of Cl, As, Ba, Hg, Mo, Pb and Se.

Figures A19 and A20 in Appendix A present time-series charts of the concentrations of indicator parameters AI, Mn, B, Ni, SO<sub>4</sub>, and conductivity for the period between February 2010 and March 2019 for Site 86. For the period between April 2014 and March 2019, the chart shows rising trends in all water quality indicator parameters which appear to be levelling off toward the end of 2017 / start of 2018 (with the exception of aluminium, which appears to be rising steadily). The rising trends observed in the majority of indicator parameters (nickel excluded) may be attributed to installation of subsurface drains to the Stage 2 area and unblocking of the KVAD toe drains, which took place in October 2010 - February 2011.

As of January 2018, the observed concentration of SO<sub>4</sub> and the conductivity have been declining.

The results from Site 86 between 2013 and 2019 indicate that the KVAR dry ash possibly affecting water quality at Site 86. This is evident from the low pH values, typical of a fresh dry ash along with elevated concentration of Al, B, Cr, Ni, Zn and relatively low Mo (Ward et al., 2009).

### Surface Water Runoff (Site 87)

No data is available for Site 87 between the end of January 2012 and start of April 2015. The results presented in Table 5-1 indicate that the 95<sup>th</sup> percentile concentrations of water quality parameters in surface waters at Site 87 (for the period between April 2015 and March 2019) generally increased significantly, with the exceptions of Al, Ba, Cd, Cr, Cu, Hg and Mo. pH decreased significantly to highly acidic conditions at pH 3.2. As a result of the increased concentrations in water quality parameters, As and Se joined other water quality parameters exceeding the WQGVs; whilst Cd and Cr concentrations decreased to below the WQGVs.

Figures A21 and A22 in Appendix A present time-series charts of the concentrations of indicator parameters AI, Mn, B, Ni, SO<sub>4</sub>, and conductivity for the period between April 2010 and March 2019 for Site 87. For the period between April 2015 and March 2019, the chart shows shallow rising - stable trends for all indicator parameters. The rate of rise in concentrations of indicator parameters is shallower than the rate of rise observed during the 2010-2012 period indicating a shift towards system equilibrium. The rising trends observed in the majority of indicator parameters may be attributed to installation of subsurface drains to the Stage 2 area and unblocking of the KVAD toe drains, which took place in October 2010- February 2011.

The results from Site 87 between 2013 and 2019 indicate that the KVAR dry ash possibly affecting water quality at Site 87. This is evident from the low pH values, typical of a fresh dry ash along with elevated concentration of Al, B, Cr, Ni, Zn and relatively low Mo (Ward et al., 2009).

# 5.1.5 Lidsdale Cut (WX5)

During the first two periods (1991-2012), water sampling was actually performed at the discharge v-notch from Lidsdale Cut Pond. Once the v-notch was sealed, to halt discharges into SSC, samples were taken from the inlet to the pond.

# Lidsdale Cut (WX5 / Site 40)

Surface water samples collected for Lidsdale Cut at Site WX5 represent water quality within the Lidsdale Cut Pond, sampled at the discharge v-notch from Lidsdale Cut Pond to SSC for the 1992-2003 monitoring period.

The results presented in Table 5-1 indicate that the 95<sup>th</sup> percentile concentrations of water quality parameters in surface waters at the WX5 sampling site were generally below the WQGVs for the period between 1992-2003, with the exception of B, Cr, F, Fe, Mn and Zn. pH was below the lower limit of the WQGVs and mildly acid at pH 5.98.

Figures A23 and A24 in Appendix A present time-series charts of the concentrations of indicator parameters AI, Mn, B, Ni, SO<sub>4</sub>, and conductivity for the period between April 1992 and March 2019. There is a significant data gap between the end of August 1992 and start of February 2002. No data is available for nickel prior to 2006. For the period between August 1992 and October 2002, the chart shows generally stable concentrations of key water quality parameters. Between 2002 and 2003, recorded concentrations of all key parameters are broadly equivalent to 1992 concentrations, indicating minimal historical changes to water quality at WX5, concurrent with wet ash emplacement within the SSCAD.

The results from WX5 during the 1991-2003 monitoring period reflect water quality conditions in Lidsdale Cut Pond at the outlet to SSC preceding dry ash placement in the KVAR, which commenced in 2003. Accordingly, the observed exceedances of the WQGVs can be attributed to other land uses (i.e. KVAD / SSCAD / Chitter) locally affecting water quality in WX5, and therefore not representative of influences from the KVAR.

2003-2012

# Lidsdale Cut (WX5 / Site 40)

Surface water samples collected for Lidsdale Cut at Site WX5 represent water quality within the Lidsdale Cut Pond, sampled at the discharge v-notch from Lidsdale Cut Pond to SSC for the 2003-2012 monitoring period.

The results presented in Table 5-1 indicate that the 95<sup>th</sup> percentile concentrations of water quality parameters in surface waters at the WX5 sampling site, for the period between January 2003 and June 2012, increased relative to the 1991-2003 concentrations, with the exception of chloride, which decreased relative to 1991-2003 concentrations. As a result of the change in water quality the majority of water quality parameters increased to levels exceeding the adopted WQGVs, with the exception of CI, Ba, and Be which remained below the WQGVs. pH became more neutral at pH 7.3.

Figures A23 and A24 in Appendix A present time-series charts of the concentrations of indicator parameters AI, Mn, B, Ni, SO<sub>4</sub>, and conductivity for the period between April 1992 and March 2019. For the period between January 2003 and June 2012, there are significant fluctuations in water quality within an overall rising trend. Noticeably, concentrations of all water quality indicator parameters drop immediately following capping of the KVAD and commencement of Stage 1 dry ash emplacement and fluctuate with high volatility but stable trend between January 2003 and January 2006. Following January 2006, the volatility continues but an underlying rising trend in concentration of water quality indicator parameters is observed. The shift to increasing trends is concurrent with blockage of the KVAD toe drains in 2006, and is also concurrent with a rise in groundwater levels in D3 to an elevation greater than 920m, indicating potential groundwater migration into the KVAR dry ash affecting water quality in Lidsdale Cut as a result of leachate generation.

In 2009, there is a sharp rise and increase in variability in concentrations of water quality indicator parameters, concurrent with commencement of Stage 2 dry ash emplacement. In May 2010, there is a sharp drop in concentrations of water quality indicator parameters, concurrent with installation of SSCAD seepage collection system.

In February 2011, there is another rise in concentrations of water quality indicator parameters, concurrent with unblocking the KVAR toe drains to LC, which is subsequently followed by a decline in overall concentrations, likely associated with the Springvale Mine Discharge Water Leak and subsequent dilution effects in WX5.

Overall and based on the available data set, the results for the monitoring period (2003-2012) appear to suggest that the KVAR placement is considered likely to have influenced water quality in Lidsdale Cut Pond (WX5) a result of groundwater migration into the KVAR at Bore D3. The KVARs possible role as a source of impact to Lidsdale Cut pond (WX5) is identified through both timing of changes to water quality in Lidsdale Cut, along with the elevated concentration of key indicator parameters.

Historical impacts on Lidsdale Cut cannot be discounted, however it is noted that concentrations increased beyond and in contrast to historical trends and concentrations, and pH decreased to highly acidic conditions following KVAR emplacement and groundwater rise in bore D3. However, due to the complexity of current and historic land use activities, including local chitter deposits, pumping and discharge regimes for the KVAD and SSCAD, it is not suitable (based on the data set available) to directly attribute water quality impacts observed in groundwater in Bore D6 solely to a single source such as the KVAR.

# 2012-2019

# Lidsdale Cut (WX5 / Site 40)

There is a large gap in available data between June 2012 and October 2013. During which time, both pumping from LC to SSCAD, and discharge from Springvale Mine to SSC at LDP009 commenced.

The results presented in Table 5-1 indicate that the 95<sup>th</sup> percentile concentrations of water quality parameters in surface waters at the WX5 sampling site, for the period between October 2012 and March 2019, increased relative to the 2003-2012 values, with the exceptions of Cl, As, and Mo, with Mo dropping below the WQGV trigger value. pH became significantly more acidic, becoming highly acidic at pH 3.1.

Figures A23 and A24 in Appendix A present time-series charts of the concentrations of indicator parameters AI, Mn, B, Ni, SO<sub>4</sub>, and conductivity for the period between April 1992 and March 2019. For the period between October 2012 and March 2019, values of all indicator parameters increased significantly and are entering into relatively stable (e.g. SO<sub>4</sub>, Cond, B, AI) to gradually rising trends (e.g. Ni, Mn).

Overall and based on the available data set, the results for the monitoring period (2012-2019) appear to suggest that the KVAR placement may have influenced water quality in Lidsdale Cut Pond (WX5) a result of groundwater migration into the KVAR at Bore D3. The KVARs possible role as a source of impact to Lidsdale Cut is identified through both timing of changes to water quality in Lidsdale Cut, along with the elevated concentration of key indicator parameters, low pH and Mo.

The cause of the noted shift in concentrations is a result of a change in the sampling location from the outlet which leads to SSC, to the inlet to Lidsdale Cut Pond. As a result, the observed water quality from 2012-2019 represents water entering the Lidsdale Cut Pond.

Due to the complexity of current and historic land use activities, including local chitter deposits, pumping and discharge regimes for the KVAD and SSCAD, it is not considered conclusive to directly attribute any impacts observed in WX5 solely to a single source such as the KVAR without further investigation.

# 5.1.6 Dump Creek (WX11) – Site 39

### 1991-2003

### Dump Creek (WX11) - Site 39

Surface water samples collected for Dump Creek (WX11) – Site 39 represent catchment surface water quality at the catchment outlet / discharge point within a creek that discharge to SSC (WX7), downgradient and west of the KVAR and Lidsdale Cut.

There is a significant gap in available data for the 1991-2003 monitoring period, between the end of September 1992 and November 2001. The results presented in Table 5-1 indicate that the 95<sup>th</sup> percentile concentrations of water quality parameters in surface waters at the WX11 sampling site are generally below the WQGVs for the 1991-2003 monitoring period, with the exceptions of B, Cr, Fe, and Zn.

Figures A25 and A26 in Appendix A present time-series charts of the concentrations of indicator parameters AI, Mn, B, Ni, SO<sub>4</sub>, and conductivity for the period between October 1991 and March 2019 at WX11. As previously stated, there is a significant data gap between the end of September 1992 and start of November 2001. No data is available for nickel prior to 2006.

For the period between October 1991 and October 2002, the chart shows generally low concentrations of key water quality parameters between 1991 and 1992. Between 2002 and 2003, recorded concentrations of all key parameters are higher than 1991-1992 records. Historical changes to water quality at WX11 associated with the 1992-2003 monitoring period are concurrent with wet ash emplacement within the SSCAD and predate the KVAR dry ash emplacement.

2003-2012

# Dump Creek (WX11) - Site 39

The results presented in Table 5-1 indicate that the 95<sup>th</sup> percentile concentrations of water quality parameters in surface waters at the WX11 sampling site for the period between January 2003 and June 2012 generally increased relatively to 1991-2003 concentrations, with the exceptions of Cl, Ba, and F. pH decreased to mildly acidic conditions at pH 5.9. As a result of the changes in water quality As, Cd, Cu, Mn, Pb, and Se rose above their respective WQGVs. Concentrations of nickel (available from 2006) show values exceeding the WQGV.

It is noted that although 95<sup>th</sup> percentile concentrations are higher during the 2003-2012 monitoring period than the preceding 1996-2003 monitoring period, the elevated concentrations at the start of the 2003-2012 monitoring period are a result of the increasing trends during the 1996-2003 monitoring period.

Figures A25 and A26 in Appendix A present time-series charts of the concentrations of indicator parameters AI, Mn, B, Ni, SO<sub>4</sub>, and conductivity for the period between October 1991 and March 2019 at WX11. For the period between January 2003 and June 2012, there is a broad fluctuation in water quality, characterised by a falling limb between 2003 and 2006 (Boron excepted), and rising limb between 2006 and 2012. The shift in trend to rising concentrations may be attributed to a rise in groundwater levels in D3 to an elevation greater than 920 mAHD, resulting in potential groundwater migration into the KVAR dry ash and therein potentially affecting water quality in Dump Creek as a result of leachate generation.

The increase in concentrations of water quality parameters from 2006 – 2012 continues through Stage 2A dry ash placement in the KVAR. There is increased variability in concentrations of key water quality parameters within the rising trend following commencement of Stage 2A dry ash emplacement in April 2009.

Overall, the results for the 2003-2012 monitoring period appear to suggest that the KVAR placement may have potentially influenced water quality in Dump Creek (WX11) as a result of groundwater migration into the KVAR at Bore D3. The KVARs possible role as a source of impact to Dump Creek is identified through both timing of changes to water quality in Dump Creek, along with the elevated concentration of key indicator parameters, low molybdenum and low pH (pH c. 3.7 post 2009) (Ward et al., 2009).

Historical impacts on Dump Creek cannot be discounted, however it is noted that concentrations increased beyond and in contrast to historical trends and concentrations, and pH decreased to highly acidic conditions following KVAR emplacement and groundwater rise in D3. However, due to the complexity of current and historic land use activities, including local chitter deposits, pumping and discharge regimes for the KVAD and SSCAD, it is not considered conclusive to directly attribute any impacts observed in groundwater in Bore D6 solely to a single source such as the KVAR without further investigation.

2012-2019

### Dump Creek (WX11) - Site 39

The results presented in Table 5-1 indicate that the 95<sup>th</sup> percentile concentrations of water quality parameters in surface waters at the WX11 sampling site for the period between June 2012 and March 2019 generally increased relative to 2003-2012 values, with the exceptions of As, Cd, Cr, Pb and Se. pH decreased to highly

acidic conditions at pH 3.1. As a result of the changes in water quality, SO<sub>4</sub>, AI, and F rose above their respective WQGVs, whilst As, Cd, Cr, and Se dropped below their respective WQGVs.

Figures A25 and A26 in Appendix A present time-series charts of the concentrations of indicator parameters AI, Mn, B, Ni, SO<sub>4</sub>, and conductivity for the period between October 1991 and March 2019 at WX11. For the period between June 2012 and March 2019, concentrations of indicator parameters fluctuated with significant volatility within overall stable to rising trends. The shift to volatile swings in water quality coincide with the unblocking of toe drains to LC in Feb 2011 and with further volatility introduced by the commencement of discharge from Springvale Mine to SSC via LDP009, which is believed to have further raised groundwater levels in D3 resulting in lateral groundwater migration and subsequent surface water discharge at WX11.

Overall, the results for the 2012-2019 monitoring period appear to suggest that the KVAR placement may have influenced water quality in Dump Creek (WX11) a result of groundwater migration into the KVAR. The KVARs possible role as a source of impact to Dump Creek is identified through both timing of changes to water quality in Dump Creek, along with the elevated concentration of key indicator parameters, low molybdenum and low pH (pH c. 3.7 post 2009) (Ward et al., 2009).

Historical impacts on Dump Creek cannot be discounted, however it is noted that concentrations increased beyond and in contrast to historical trends and concentrations, and pH decreased to highly acidic conditions following KVAR emplacement and groundwater rise in D3. Due to the complexity of current and historic land use activities, including local chitter deposits, pumping and discharge regimes for the KVAD and SSCAD, it is not considered suitable to directly attribute any impacts observed in groundwater in Bore D6 solely to a single source such as the KVAR without further, more detailed investigation.

# 5.1.7 Springvale 158

The results presented in Table 5-1 indicate that the 95<sup>th</sup> percentile concentrations of water quality parameters in surface waters at the Springvale (Site 158) sampling point for the period between 2011 and 2018 were generally below the adopted WQGVs, with the exception of As, Fe and Mo, which marginally exceeded the WQGVS.

Figures A27 and A28 in Appendix A present time-series charts of the concentrations of indicator parameters AI, Mn, B, Ni, SO<sub>4</sub>, and conductivity for the period between 2011 and March 2018 for Springvale 158. The chart shows that concentrations have remained relatively stable over time, though with a slight reduction in concentrations of sulfate.

Water quality at Springvale (Site 158) is not affected by the KVAR.

# 5.2 Groundwater Trends 1988 - 2019

To assess effects of dry ash emplacement within the KVAR on groundwater quality, it is necessary to analyse both recent concentrations and long-term trends in concentrations of key physical and chemical stressors / toxicants within the selected groundwater monitoring sites.

As outlined in Section 2.5, surface water and groundwater flows through the site are complexly modified by the extensive engineering aspects influencing the site, including:

- Diversion drains through the KVAR / KVAD draining surface water and groundwater to various sumps (i.e. Sumps 1-3), Ponds, Dirty Water Pond, Return Water Canal and to Lidsdale Cut
- Recirculation pumping of SSCAD seepage collected through the SSCAD V-notch back to the SSCAD Pond via the Return Canal
- Recirculation pumping of water from Lidsdale Cut to the SSCAD Pond via the Dirty Water Pond

The 95<sup>th</sup> Percentile of results have been tabulated for periods corresponding with pre-dry ash emplacement (1991-2003), dry ash emplacement / pre-unblocking of the KVAD toe drains (2003-2010) and post unblocking of the KVAD toe drains / post dry-ash emplacement (2010-2019). These key events mark periods of marked water quality changes for the groundwater receiving site (D5) and other groundwater sampling points.

It is also noted that blockage of the KVAD toe drains (2006), unblocking of the KVAD toe drains (2010), commencement of pumping from Lidsdale Cut to SSCAD via the Return Canal (July 2012) and commencement of discharge from Springvale Mine to SSC at LDP009 (July 2013) have had marked effects on groundwater quality, these aspects are discussed within the evaluation of the long-term groundwater trends.

Sample Location	Date	На	Cond (us/cm)	TDS	so:	0	AI*	As	Ad	Ba	Be	*	Cd	c	Cu		Fe-F H	На	Mn	Mo	iN	Pb	Se	Zn*
					•				Groundwater Receiving Site	ar Receivin	g Site							)						
Groundwater Bore WGM1/D5 (36)	1988-2003	4.7	864	576	336	26	Ð	0.011	0.001	0.622	0.006	1.76	0.042	0.05	0.07	0.77	15.96 (	0.0006	3.045	Q	0.137	0.07	0.002	0.69
	2003-2010	4.1	2341	1995	1490	27.6	41.2	0.048	0.00955	0.0379	0.02935	6.3	0.011	0.005	0.04	1.3	25.9 (	0.0001	13.85	0.01	-	0.03	0.006	2.09
	2010-2019	3.7	1400	1100	720	36.0	30.7	0.01	0.001	0.08	QN	2.9	0.068	0.013	0.055	1.2	6.2	0.0001	8.7	0.010	0.57	0.11	0.005	3.3
									KVA	KVAR / KVAD														
Groundwater Bore WGM1/D6 (37)	1988-2003	5.6	1220	770	400	80	QN	0.006	0.001	0.78	0.001	-	0.006	0.03	0.036	0.35	130 (	0.0008	5.015	QN	0.20	0.017	0.071	0.32
	2003-2010	4.6	1423	784	440	70.5	5.96	0.05	0.01	0.04	0.016	0.89	0.002	0.016	0.01	0.7	85.7 (	0.0001	4.65	0.066	0.55	0.015	0.006	1.95
	2010-2019	3.1	1984	1760	1100	57.6	6.8	0.01	0.001	0.03	QN	1.3	0.004	0.004	0.016	0.70	201	0.0001	9.4	0.010	0.62	0.022	0.002	1.8
Groundwater Bore AP09 (77)	2010-2019	5.9	3000	2541	1650	41.7	93.0	0.09	0.001	0.03	QN	3.3	0.0004	0.001	0.004	5.22	121 (	0.0001	12.1	0.201	1.37	0.003	0.002	1.3
Groundwater Bore AP17 (78)	2010-2019	3.3	5511	5686	3851	22.9	25.0	0.11	0.001	0.03	QN	14.4	0.002	0.008	0.048	108	236 (	0.0001	16.1	0.100	1.91	0.005	0.157	5.9
KVAD Seepage (94)	2015-2019	3.1	5578	6418	4370	43.6	294	0.05	0.001	0.03	QN	19.3	0.077	0.037	0.067	51.6	45.2 0	0.00002	24.8	0.003	2.45	0.007	0.062	4.7
Groundwater Bore GW6 (85)	2010-2016	7.4	4474	3286	1690	608	14.4	0.007	0.001	0.301	QN	0.224	0.0003	0.011	0.025	1.64	14 0	0.0001	26.3	0.01	0.37	0.114	0.002	0.344
Groundwater Bore GW10 (75)	2010-2013	6.6	1745	1345	866	168	50.2	0.04	0.001	0.354	ND	1.59	0.010	0.011	0.055	7.79	6.38 0	0.00007	9.78	0.24	2.08	0.17	0.010	2.97
Groundwater Bore GW11 (76)	2010-2016	7.4	1040	744	436	27.08	20	0.015	0.001	0.202	QN	1.514	0.0004	0.01	0.025	0.44	4.81 0	0.00009	4.42	0.04	0.03	0.06	0.002	0.238
								Downgra	Downgradient SSCAD - Upgradient KVAR	AD - Upgr	adient KV#	R												
Groundwater Bore WGM1/D3 (34)	1988-2003	6.5	740	487	124	86	Q	0.03	0.001	0.254	0	0.2	0.001	0.02	0.01	0.46	11	0.0008	0.731	QN	0.09	0.017 0	0.0024	0.14
	2003-2010	6.6	807	526	130	110	0.72	0.05	0.01	0.129	0.001	0.049	0.002	0.01	0.01	0.1	4.89 (	0.0001	1.095	0.01	0.20	0.01	0.006	0.11
	2010-2019	5.2	1490	1130	749	150	7.6	0.01	0.001	0.12	ND	1.9	0.010	0.003	0.018	0.94	12.9 (	0.0001	3.7	0.010	0.73	0.005	0.002	0.72
Groundwater Bore WGM1/D4 (35)	1988-2003	6.8	730	520	222	56.2	QN	0.008	0.001	0.514	0.0009	0.5	0.004	0.016	0.05	0.37	93.5	0.003	7.24	0	0.02	0.014	0.046	0.098
	2003-2010	6.3	1582	1300	954	35	0.085	0.05	0.01	0.069	0.01	1.6	0.002	0.01	0.01	0.1	70.8	0.0001	20	0.01	0.05	0.01	0.006	0.1
	2010-2019	5.7	1711	1391	896	46.9	0.1	0.003	0.001	0.03	ND	1.9	0.0002	0.002	0.004	0.10	61.0	0.0001	19.0	0.010	0.05	0.001	0.002	0.09
Groundwater Bore WGM1/D2 (33)	1988-2003	5.5	320	277	67.1	61.1	QN	0.002	0.001	0.144	QN	0.14	0.001	0.045	0.038	0.32	2.26 (	0.0008	0.534	QN	0.03	0.031	0.001	0.13
	2003-2010	5.0	461	309	158	43.9	Q	0.05	0.01	0.071	0.001	0.129	0.002	0.01	0.01	0.19	5.29 (	0.0001	0.624	0.01	0.06	0.01	0.006	0.13
	2010-2019	3.6	650	388	183	39.0	0.5	0.001	0.001	0.05	QN	0.3	0.0002	0.003	0.007	0.10	3.20 (	0.0001	0.80	0.010	0.09	0.003	0.002	0.13
								Upgrad	pgradient of SSCAD and KVAR / KVAD	CAD and K	VAR / KVA	0												
Groundwater Bore WGM1/D1 (32)	1988-2003	6.2	322	247	13.7	82.6	Q	0.005	0.0091	0.185	0	0.175	0.003	0.043	0.054	0.55	7.70 (	0.0005	0.7475	QN	QN	0.019	0.003	0.150
	2003-2010	6.1	141	179	11.7	21	7.42	0.003	0.001	0.105	0.001	0.047	0.0015	0.006	0.028	0.1	2.24 0	0.00009	0.498	0.01	0.01	0.013	0.002	0.144
	2010-2019	5.2	149	169	18.9	28.7	7.0	0.001	0.001	0.09	QN	0.1	0.0002	0.005	0.021	0.10	1.56 (	0.0001	0.67	0.010	0.01	0.013	0.002	0.18
									Groundv	Groundwater WQGVs	Vs													
Groundwater WQGV		6.5-8.0	2600	2000++	1000++	350+	5.1 ^ ^	0.024	0.00005	0.7+++	0.1	1.7	0.001	0.004	0.005	1.5 +++	<u>1.7</u> 0	0.00006	1.9	0.01+	0.137	0.01	0.005	0.505
Additional notes: See Table 4-4																								

Table 5-2 Summary Statistics Long Term Groundwater Monitoring Results (mg/L) – 95th Percentiles

# 5.2.1 Groundwater Bore D5 – Receiving Site (Site 36)

# 1988-2003

Groundwater samples collected for D5 during this period represent groundwater quality concurrent with emplacement of wet ash within SSCAD, post KVAD wet ash emplacement, and pre-date dry ash emplacement in the KVAR.

The results presented in Table 5-2 indicate that the 95<sup>th</sup> percentile concentrations of a number of key parameters in groundwaters of the receiving site (D5) exceeded the adopted WQGV's for B, Cd, Cr, Cu, Fe, Hg, Mn, Pb, Zn, and for pH (below lower limits). Conductivity, SO<sub>4</sub>, Cl, As, Ba, Be, F, Ni and Se were below the adopted WQGVs.

Figures B1 and B2 in Appendix B presents time-series charts of the concentrations of indicator parameters AI, Mn, B, Ni, SO<sub>4</sub>, and conductivity, along with the recorded groundwater levels, for the period between 1988 and 2019 for D5, which show that concentrations of key parameters in groundwater are relatively stable during the period between 1988 and 2003.

# 2003-2010

Groundwater quality results in Table 5-2 indicate that the 95<sup>th</sup> percentile concentrations of key parameters increased from baseline values (1988-2003) during the 2003-2010 period for SO<sub>4</sub>, Cl, As, Be, B, F, Fe, Mn, Ni, Se, and Zn resulting in an increase in overall conductivity and rise in acidity (reduced pH). Changes for Al and Mo cannot be determined due to lack of data during the baseline period.

Indicator parameters shown in Figures B1 and B2 in Appendix B indicate increased concentrations of key parameters and a rising trend of concentrations in groundwater between 2007 and 2010 for groundwaters in receiving site D5. The noted increase in concentrations of water quality parameters and rising trend in water quality parameters corresponds with the timing of and therefore may be directly attributed to) a rise in groundwater levels in Bore D3, (located upgradient of the KVAR / downgradient of the SSCAD) to an elevation greater than 920 mAHD. The rise in groundwater levels around Bore D3 potentially resulted in groundwater migration into the KVAR dry ash resulting in generation of dry ash leachate.

Due to the complexity of current and historic land use activities, including local chitter deposits, pumping and discharge regimes for the KVAD and SSCAD, it is not considered conclusive to directly attribute any impacts observed in groundwater in Bore D6 solely to a single source such as the KVAR without further investigation.

Influence from the KVAR on groundwater quality in D5 during this period is evident from the shift in concentration of water quality parameters, including reduced pH, and elevated SO<sub>4</sub>, Ca, and Zn and other parameters, at concentrations significantly above pre-KVAR levels.

# 2010-2019

The results presented in Table 5-2 indicate that the 95<sup>th</sup> percentile concentrations of key parameters in D5 decrease for TDS, SO<sub>4</sub>, Al, As, B, F, Fe, Mn, Mo, Ni, & Se during the 2010-2019 period. Concentrations of Cl, Ba, Cd, Cr, Cu and Pb increased in 95<sup>th</sup> percentile concentrations. pH becomes slightly more acidic (pH 3.7), while overall conductivity decreases.

Time series records for indicator parameters (presented in Figures B1 and B2 in Appendix B) show that concentrations of Mn, B, SO<sub>4</sub>, Ni, and overall conductivity decrease initially following completion of Stage 1 dry ash emplacement in the KVAR (February 2009), and again in Feb 2010 following the unblocking of the toe drains. The trend of decreasing concentrations is interrupted in July 2013, following commencement of discharge from Springvale Mine to SSC at LDP009. It is observed that concentrations of key parameters fluctuate significantly following July 2013, with stable to rising trends for key parameters.

Overall, the results for the 2003-2010 monitoring period appear to suggest that the KVAR placement may have potentially influenced water quality in Bore D5 a result of groundwater migration into the KVAR. The KVARs possible role as a source of impact to Bore D5 is identified through both timing of changes to water quality in

Bore D5, along with the elevated concentration of indicator parameters, above historic background concentrations, and rising groundwater levels in Bore D3.

Water quality in Bore D5 generally improved following February 2010, indicating possible unblocking of the Stage 1 KVAD toe drains resulted in an improvement of groundwater quality. Subsequently, the concentrations of water quality parameters in Bore D5 generally decreased towards pre-KVAR concentrations until July 2013, following which point there are significant fluctuations in water quality, with 95<sup>th</sup> percentile concentrations of water quality parameters greater than historical background (1988-2003) values. The observed fluctuations in water quality parameters are observed in conjunction with fluctuations and an overall rise in groundwater levels in bore D3, which is considered likely to be attributed discharge from Springvale Mine upgradient of the KVAR.

The results at Bore D5 are interpreted to be potentially influenced by seepage from SSC, however this is likely to have a dilutive rather than additive effect on the concentrations of water quality parameters as SSC is relatively reduced in concentrations of indicator parameters. The relative effect of SSC dilution on groundwater quality downgradient of the KVAR / KVAD can be observed comparison of Bore D5 with Bore D6, which is located downgradient of the Stage 1 KVAR area and away from SSC, and shows a similar relationship between groundwater levels in Bore D3 and water quality trends post 2007.

Due to the complexity of current and historic land use activities, including local chitter deposits, pumping and discharge regimes for the KVAD and SSCAD, it is not considered suitable to directly attribute any impacts observed in groundwater in Bore D6 solely to a single source such as the KVAR without further, more detailed investigation.

# 5.2.2 KVAR / KVAD Monitoring Bores

# 1988-2003

### D6 - Site 37

Bore D6 is a seepage detection bore for the KVAD. Groundwater quality data for D6 is available from 1988.

Groundwater samples collected for D6 during this period represent groundwater quality concurrent with emplacement of wet ash within SSCAD, post KVAD wet ash emplacement, and pre-date dry ash emplacement in the KVAR.

The groundwater quality data for D6, presented in Table 5-2 shows that the 95<sup>th</sup> percentile concentrations of a number of key water quality parameters in groundwater exceeded the adopted WQGVs for Ba, Cd, Cr, Cu, Fe, Hg, Mn, Ni, Pb, Se, and pH (below lower limits). Conductivity, TDS, SO<sub>4</sub>, Cl, As, Be, B, F, and Zn did not exceed WQGVs. No data was available for Al or Mo.

Figures B3 and B4 in Appendix B presents time-series charts of the concentrations of indicator parameters AI, Mn, B, Ni, SO<sub>4</sub>, and conductivity for the period between 1988 and 2019 for D6, which show that concentrations of key parameters in groundwater are relatively stable during the period between 1988 and 2003, with no significant fluctuations.

### AP09 (77), AP17 (78), GW10 (75), GW11 (76)

Groundwater quality data for GW10, GW11, AP9 and AP17 are only available for the period between 2010 and 2019.

### 2003-2010

#### D6 - Site 37

The Groundwater quality results in Table 5-2 indicate that the 95<sup>th</sup> percentile concentrations of key parameters increased from baseline values (1988-2003) at D6 during the 2003-2010 period for SO<sub>4</sub>, As, F, Be, Ni, Zn and conductivity, with As, Zn subsequently exceeding WQGVs and pH becoming more acid (pH 4.6). Other water quality parameters including Cl, Ba, B, Cd, Cr, Cu, Fe, Hg, Mn, Pb, and Se reduced in concentration, however

remained above WQGVs with the exception of Ba which dropped below its WQGV and B which remained below its WQGV. Relative changes for Al and Mo cannot be determined due to lack of baseline data, however are noted to exceed WQGVs during the 2003-2010 period.

Time series records of indicator parameters Al, Mn, B, Ni, SO<sub>4</sub>, and conductivity for the period between 2003 and 2010 for D6 (presented in Figures B3 and B4 in Appendix B), show a sudden drop in concentrations directly after Feb 2003, potentially associated with additional capping of the KVAD (through stage 1 Ash emplacement) and reduction of infiltration to groundwater at D6. A large data gap is present between 2004 and 2007. However, records indicate concentrations of key indicator parameters similar to baseline concentrations between 2007 and 2009.

From 2009 to 2010 there is a noted trend of reduced pH, and increasing concentrations and variability in water quality parameters. The observed shift in trends to rising concentrations of key parameters is coincident with both Stage 2A dry ash emplacement, and a rise in groundwater levels in Bore D3, (located upgradient of the KVAR / downgradient of the SSCAD) to an elevation greater than 920 mAHD. The rise in groundwater levels around Bore D3 potentially resulted in groundwater migration into the KVAR dry ash resulting in generation of dry ash leachate.

Due to the complexity of current and historic land use activities, including local chitter deposits, pumping and discharge regimes for the KVAD and SSCAD it is not considered conclusive to directly attribute any impacts observed in groundwater in Bore D6 solely to a single source such as the KVAR without further investigation.

# 2010-2019

### D6 – Site 37

The results presented in Table 5-2 indicate that the 95<sup>th</sup> percentile concentrations of key water quality parameters in groundwater of D6 increased for SO<sub>4</sub>, AI, B, Cd, Cu, Fe, Mn, Ni, and Pb during the 2010-2019 monitoring period with a corresponding increase in conductivity and TDS and a decrease in pH (pH 3.1). Concentrations of Cl, As, Ba, Cr, Mo, Se, and Zn dropped in the same period.

Time series records of indicator parameters AI, Mn, B, Ni, SO<sub>4</sub> and conductivity for the period between 2010 and 2019 for D6 (presented in Figures B3 and B4 in Appendix B B) show volatile fluctuations but relatively stable concentrations up to July 2012 for heavy metals and an increasing trend for SO<sub>4</sub> and conductivity. Following July 2012 and the commencement of pumping from LC to the Return Water Canal, there is greater volatility in water quality parameters, along with increased concentrations and stable to increasing trends. From July 2013, following commencement of discharge from Springvale Mine at LDP009, there is a further increase in trend, volatility and concentrations of indicator parameters in Bore D6.

Overall, the results for the 2010-2019 monitoring period appear to suggest that the KVAR placement may have potentially influenced water quality in Bore D6 a result of groundwater migration into the KVAR. The KVARs possible role as a source of impact to Bore D6 is identified through both timing of changes to water quality in Bore D6, along with the elevated concentration of indicator parameters, above historic background concentrations, and rising groundwater levels in Bore D3. Additional fluctuations and a continued rise in both groundwater levels in Bore D3 and concentrations of water quality parameters in Bore D6 may be associated with discharge from Springvale Mine and subsequent groundwater mounding upgradient of / migration into the KVAR, resulting in dry ash leachate impacts on groundwater quality in Bore D6.

Due to the complexity of current and historic land use activities, including local chitter deposits, pumping and discharge regimes for the KVAD and SSCAD it is not considered conclusive to directly attribute any impacts observed in groundwater in Bore D6 solely to a single source such as the KVAR without further investigation.

### AP09 (77), AP17 (78), GW10 (75), GW11 (76), and KVAD Seepage (94)

The bores GW10, GW11, AP9 and AP17, sample the groundwater in the KVAD beneath the KVAR.

The results presented in Table 5-2 indicate that the 95<sup>th</sup> percentile concentrations of key parameters in AP09, AP17, GW10, GW11 and KVAD Seepage are highly variable and strongly affected by relative position to the various toe drains that drain the KVAR, with AP09, AP17, GW6 and KVAD Seepage showing close similarities.

No data has been available for GW10 from 2013, for GW6 from Nov 2016 and for GW11 from Sept 2016 due to drying out of the monitoring points.

Concentrations of key water quality parameters in AP09, AP17, GW6, GW11 and KVAD Seepage generally exceed the WQGVs for SO<sub>4</sub>, Al, As, B, Cd, Cr, Cu, F, Fe, Mn, Ni, and Zn, along with variable exceedances of Hg, Mo, Pb and Se.

Figures B5 through B16 in Appendix B present time series records for indicator parameters for AP09, AP17, GW6, GW11 and KVAD Seepage. Consistent records of water quality data are available for 2010-2019 for AP09 and AP17. Records for GW6 present significant data gaps, whilst records for KVAD Seepage are only available for years 2015-2019.

Figures B5 through B8 in Appendix B present the time series records for AP09 and AP17, located along the northern catchment of the KVAR Stage 2 Area and west of the Sedimentation Control Area. Records indicate rising concentrations of key parameters for AP09 from February 2010 up to February 2011, corresponding with Stage 2 and Stage 2A dry ash emplacement, and generally stable or declining concentrations in AP17.

Following February 2011, there is a decline in concentrations of indicator parameters for AP09 and AP17 in correspondence with the timing of the clearing of the KVAD toe drains for the Stage 2 Area.

There is a gap in available data between June 2013 and April 2015, however concentrations of key parameters are notably higher at the start of April 2015, with a reversal of the decreasing trend to increasing concentrations of indicator parameters. The marked increase in concentrations and reversal to rising trends correlates with the commencement of pumping from LC to the SSCAD via the return Canal, indicating potential subsequent seepage back into the KVAR. However, it is noted that concentrations appear to rise prior to this event for AP17 (Feb 2012), which suggests another mechanism has affected water quality at these monitoring points.

# 5.2.3 Downgradient of SSCAD / Upgradient of KVAR

# 1988-2003

# D2 – Site 33

Groundwater monitoring point D2 is located south (cross-gradient) of the KVAR Stage 1 area, downgradient of the SSCAD and adjacent to the return Canal. Groundwater samples collected for D2 during this period represent groundwater quality concurrent with emplacement of wet ash within SSCAD, post KVAD wet ash emplacement, and pre-date dry ash emplacement in the KVAR.

The results presented in Table 5-2 indicate that the 95<sup>th</sup> percentile concentrations of key parameters in D2 were generally below the adopted WQGVs with the exceptions of Cr, Cu, Fe and Pb. pH was also below the lower limit of the WQGVs at pH 5.51. The greatest exceedance of WQGVs included concentrations of Cr and Cu which were up to 10 times their corresponding WQGVs.

Figures B17 and B18 in Appendix B present time-series charts of the concentrations of indicator parameters AI, Mn, B, Ni, SO<sub>4</sub> and conductivity for the period of 1988-2019 for D2. The results show a gradual rising trend at D2 for conductivity, SO<sub>4</sub> and Mn during the 1988-2003 monitoring period, potentially corresponding with effects from Stage 1 dry ash emplacement.

### D3 – Site 34

Groundwater monitoring point D3 is located east of the KVAR, adjacent to the Stage 2B emplacement area and immediately west / downgradient of SSCAD and SSC proximal to LDP009. Groundwater samples collected for D3 during this period represent groundwater quality concurrent with emplacement of wet ash within SSCAD, post KVAD wet ash emplacement, and pre-date dry ash emplacement in the KVAR.

The results presented in Table 5-2 indicate that the 95<sup>th</sup> percentile concentrations of key parameters in D3 were generally below the adopted WQGVs with the exceptions of As, Cr, Cu, Fe, Hg and Pb, which variably exceeded the WQGVs. The greatest exceedance of WQGVs included concentrations of Fe, Cr and Cu which are observed at up to 10 times their corresponding WQGVs.

Figures B19 and B20 in Appendix B present time-series charts of the concentrations of indicator parameters AI, Mn, B, Ni, SO<sub>4</sub> and conductivity for the period of 1988-2019 for D3. The results show that concentrations of key water quality parameters were relatively stable during the 1988-2003 monitoring period at D3.

# D4 – Site 35

Groundwater monitoring point D4 is located north of the KVAR, beyond SSC and west of / downgradient of SSCAD. Groundwater samples collected for D4 during this period represent groundwater quality concurrent with emplacement of wet ash within SSCAD, post KVAD wet ash emplacement, and pre-date dry ash emplacement in the KVAR.

The results presented in Table 5-2 indicate that the 95<sup>th</sup> percentile concentrations of key parameters in D4 were generally below the adopted WQGVs with the exceptions of Cd, Cr, Cu, Fe, Hg, Mn, Pb, and Se, which variably exceeded the WQGVs. The greatest exceedances of the WQGVs included concentrations of Cr, Cu, Fe, Mn and Se which were generally 10 times their respective WQGV, with the exception of Fe which is observed at over 50 times the WQGV. pH was below the lower limit at pH 5.51.

Figures B21 and B22 in Appendix B present time-series charts of the concentrations of indicator parameters AI, Mn, B, Ni, SO<sub>4</sub> and conductivity for the period of 1988-2019 for D4. The results show that concentrations of key water quality parameters SO<sub>4</sub>, Mn and B gradually increased over the 1988-2003 monitoring period at D4, similar to bores D5 and D6. No records are available for AI during this period. The noted increase in concentration of key water quality parameters at D4 corresponds with the timing of ash emplacement within SSCAD.

# 2003-2010

### D2 – Site 33

The Groundwater quality results in Table 5-2 indicate that the 95<sup>th</sup> percentile concentrations of key parameters increased from baseline values (1988-2003) at D2 during the 2003-2010 for Fe, SO<sub>4</sub>, Mn, Ni and Se, with a relative drop in pH towards more acidic condition (pH 4.99). Remaining parameters dropped or remained stable during this period. Accordingly, fewer parameters exceeded the WQGVs with only Cr, Fe, Hg, Se and pH exceeding / failing the WQGVs. No records are available for AI during this period.

Time series records of indicator parameters AI, Mn, B, Ni, SO<sub>4</sub> and conductivity or the period between 1988 and 2019 for D2 (presented in Figures B17 and B18 in Appendix B), continue to show a gradual rising trend during the 2003-2010 monitoring period, consistent with the rising trend observed during the 1988-2003 monitoring period.

The groundwater quality trends in Bore D2 do not exhibit any shifts in quality between 2003 and 2010 that may indicate effects on groundwater quality as a result of dry ash emplacement in the KVAR.

### D3 – Site 34

The Groundwater quality results in Table 5-2 indicate that the 95<sup>th</sup> percentile concentrations of key parameters increased marginally from baseline values (1988-2003) at D3 during the 2003-2010 for SO<sub>4</sub>, Cl, As, Cd, Mn, Ni, and Se, and an overall increase in conductivity, with other parameters showing decreasing or stable trends. Cd, Ni and Se increased to concentrations exceeding WQGVs, whilst Pb dropped below.

Time series records of indicator parameters AI, Mn, B, Ni, SO<sub>4</sub> and conductivity for the period between 2003 and 2010 for D3 (Figures B19 and B20 in Appendix B), show a generally stable to indistinctly increasing trend in key water quality parameters.

The groundwater quality trends in Bore D3 do not exhibit any shifts in quality between 2003 and 2010 that may indicate effects on groundwater quality as a result of dry ash emplacement in the KVAR.

# D4 – Site 35

The Groundwater quality results in Table 5-2 indicate that the 95<sup>th</sup> percentile concentrations of key parameters increased from baseline values (1988-2003) at D4 during the 2003-2010 for SO<sub>4</sub>, As, B, Be, Ni and Mn, but with a relative decrease or stable trend in other parameters, with Pb and Se dropping below their respective WQGV trigger values. pH decreased to marginally below lower limit of WQGV range at pH 6.3.

Time series records of indicator parameters AI, Mn, B, Ni, SO<sub>4</sub> and conductivity for the period between 1988 and 2019 for D4 (Figures B21 and B22 in Appendix B), show a continuation of the rising trend in concentrations of SO<sub>4</sub>, Mn and B with corresponding rise in overall groundwater conductivity at D4 for the 2003-2010 monitoring period.

The groundwater quality trends in Bore D4 do not exhibit any shifts in quality between 2003 and 2010 that are likely to be attributed to the KVAR. The increasing trend preceding and up to 2010 appear to be concurrent with ash emplacement in SSCAD and likely reflect seepage to bore D4, until the SSCAD seepage collection system was installed, following which point stable to decreasing trends are observed for many contaminants.

# 2010-2019

# D2 - Site 33

The results presented in Table 5-2 indicate that the 95<sup>th</sup> percentile concentrations of key water quality parameters in groundwater at D2 increased marginally for SO<sub>4</sub>, B, Mn, Ni during the 2010-2019 monitoring period, with a corresponding increase in overall conductivity. Remaining parameters generally decreased or remained stable with a decrease in overall pH (pH 3.6) and Cr and Se dropped to concentrations below their relevant WQGVs.

Figures B7 and B18 in Appendix B presents time-series charts of the concentrations of indicator parameters AI, Mn, B, Ni, SO<sub>4</sub> and conductivity for the period of 1988-2019 for D2. The results show a noticeable increase in the rate of the rising trend at D2 for conductivity, SO<sub>4</sub>, Mn, Ni, and B during the period between July 2012 and March 2014, corresponding with the timing of pumping from LC to SSCAD via the Return Canal, which is proximal to D2. Following March 2014, KVAR ceased operation and ash production and concentrations of key water quality parameters in D2 subsequently stabilised.

# D3 – Site 34

The results presented in Table 5-2 indicate that the 95<sup>th</sup> percentile concentrations of key water quality parameters in groundwater at D3 increased for SO<sub>4</sub>, Cl, Al, B, Cu, F, Fe, Mn, Ni, and Zn during 2010-2019 monitoring period, with a corresponding increase in overall conductivity. Remaining parameters generally decreased or remained stable with a drop in overall pH (pH 5.2). As, Ba, Cr, Pb and Se dropped to concentrations below the WQGVs.

Figures B19 and B20 in Appendix B present time-series charts of the concentrations of indicator parameters AI, Mn, B, Ni, SO<sub>4</sub> and conductivity for the period of 1988-2019 for D3. The results show a drop in SO<sub>4</sub> and overall conductivity between October 2011 and Feb 2012, corresponding with pipe leakage from Springvale Mine and subsequent localised groundwater recharge. Following July 2013, and the commencement of discharge from Springvale Mine at LDP009, there is a gradual increase in concentrations of SO<sub>4</sub>, Ni, AI and conductivity along with a trend of rising groundwater levels at D3, contrary to general trends.

The water quality results for D3 from the 2010-2019 monitoring period indicate that the commencement of discharge from Springvale Mine at LDP009, has likely resulted in increased mixing between the SSCAD / KVAR / KVAD and groundwaters at D3. This has resulted in increasing concentrations of water quality parameters in D3 and decreasing pH.

Since February 2017, concentrations of key water quality parameters in groundwater from D3 have risen substantially at a significant rate, however generally remain below the WQGVs. The cause of the recent increase in concentrations is currently unknown, however may be related to the continuing rise in groundwater levels and subsequent interactions with groundwaters of the KVAR / KVAD and / or SSCAD.

### D4 – Site 35

The results presented in Table 5-2 indicate that the 95<sup>th</sup> percentile concentrations of key water quality parameters in groundwater at D4 have generally remained stable or decreased during the 2010-2019 monitoring period, with the exception of CI, AI and B, which have increased marginally with B increasing to concentrations above its WQGV.

Figures B21 and B22 in Appendix B present time-series charts of the concentrations of indicator parameters AI, Mn, B, Ni, SO<sub>4</sub> and conductivity for the period of 1988-2019 for D4. The results show stable to decreasing trends for SO<sub>4</sub>, Mn, and Ni during the 2010-2019 monitoring period.

The timing of erratic signals observed in Al at D4 correspond with the timing of decreasing concentrations of SO<sub>4</sub>, Mn, and Ni, which in turn correspond with the timing of commencement of discharge of Springvale Mine Water at LDP009. These results indicate that the discharge from Springvale Mine is locally influencing groundwater quality at D4.

The groundwater quality trends in Bore D4 do not exhibit shifts in quality that can be directly attributed to the KVAR due to the trend of increasing concentrations in the preceding monitoring period.

# 5.2.4 Upgradient of SSCAD and KVAR / KVAD

### 1988-2003

#### D1 – Site 32

The results presented in Table 5-2 indicate that the 95<sup>th</sup> percentile concentrations of key parameters in D1 were generally below the adopted WQGVs with the exceptions of Cd, Cr, Cu, Fe and Pb. pH was also below the lower limit of the WQGVs at pH 6.16. The greatest exceedance of WQGVs included Cr, Cu and Fe, which were up to 10 times their corresponding WQGVs. The results also show that unlike locations proximal / within and downgradient of the KVAR / KVAD, SO4, Mn, B, and Ni are not significant components of the composition of groundwater.

Figures B23 and B24 in Appendix B present time-series charts of the concentrations of indicator parameters AI, Mn, B, Ni, SO<sub>4</sub> and conductivity for the period of 1988-2019 for D1. The results show that concentrations of key water quality parameters are generally stable to decreasing during the 1988-2003 monitoring period. Water quality in D1 is not affected by the KVAR.

2003-2010

#### D1 – Site 32

The results presented in Table 5-2 indicate that the 95<sup>th</sup> percentile concentrations of key water quality parameters in groundwater at D1 generally remained stable or decreased marginally during the 2003-2010 monitoring period. Records for concentrations of AI become available during this monitoring period and are recorded at levels exceeding the WQGVs.

Figures B23 and B24 in Appendix B present time-series charts of the concentrations of indicator parameters AI, Mn, B, Ni, SO<sub>4</sub> and conductivity for the period of 1988-2019 for D1, with the exception of SO<sub>4</sub> which shows a slight increasing trend towards the latter half of the monitoring period. The results show that concentrations of key water quality parameters are generally stable to decreasing during the 2003-2010 monitoring period. Water quality in D1 is not affected by the KVAR.

# D1 – Site 32

The results presented in Table 5-2 indicate that the 95<sup>th</sup> percentile concentrations of key water quality parameters in groundwater at D1 generally remained relatively stable or decreased during the 2010-2019 monitoring period, with the exception of SO<sub>4</sub>, Cl, B, Mn and Zn which increased marginally alongside overall conductivity. Concentrations of Cd and Fe subsequently dropped below the adopted WQGVs as a result of the declining trend.

Figures B23 and B24 in Appendix B present time-series charts of the concentrations of indicator parameters AI, Mn, B, Ni, SO<sub>4</sub> and conductivity for the period of 1988-2019 for D1. In general, concentrations of indicator parameters show decreasing trends but higher volatility in results during the 2010-2019 monitoring period, likely as a result of declining groundwater levels and increasing importance of rainfall recharge on groundwater quality at D1. Contrary to general trends of declining concentrations of water quality indicator parameters, SO<sub>4</sub> and B show slightly increasing trends. The noted increase in these parameters may be as a result of oxidation of local pyrite bearing strata and subsequent development of sulfuric, acidic leachate, however the exact cause of the trend is not yet known. Water quality in D1 is not affected by the KVAR.

# 6 Summary

This 2018-2019 water quality monitoring report is required for the NSW Department of Planning and Environment's Development Consent Conditions for the Kerosene Vale Ash Repository and because the Wallerawang Power Station's Environment Protection Licence (EPL 766) as of 1 January 2019 has been retained.

# 6.1 KVAR Impacts on Surface Water Quality

In general, the surface water quality monitoring over the last year (2018-2019) indicates quasi-stable or slight improving trends in all the key water quality parameters observed at the various surface water monitoring locations.

# **Surface Water Receiving Site**

Review of both recent (2018-2019) and historical (1991-2019) data for surface water monitoring associated with the KVAR has identified that the KVAR is currently not having a measurable impact on surface water quality in Sawyers Swamp Creek (SSC) at the designated surface water receiving site (WX7). Results indicate that the current water quality in SSC at WX7 is dominated by discharge from Springvale Mine at LDP009, which discharges approximately 18ML/d to SSC.

The historical available data indicates that generally the 95<sup>th</sup> percentile concentrations of arsenic, iron and molybdenum within the adjacent mine discharge exceed the adopted water quality guidelines. This is likely contributing to the resultant 95<sup>th</sup> percentile exceedances in concentrations of arsenic and molybdenum at WX7.

# **Additional Sites**

Review of additional surface water monitoring sites associated with the KVAR has identified that the KVAR is having a quantifiable impact to surface water quality at the Lidsdale Cut, along with the surface water seepage sites (Sites 80, 81, 86 and 87). It is noted however that these sites do not represent identified receiving water sites and therefore the surface water quality results are not directly relevant to development consent conditions or water quality in SSC.

Review of the long-term water quality data (Table 5-1) for Dump Creek (WX11/monitoring point 39) indicates that concentrations of B, Cr, Fe, and Zn exceeded WQGVs during the pre-KVAR period (1991-2003), whilst pH was relatively neutral (pH 8.0). Between 2003 and 2010 there is a noted trend of increasing concentrations in water quality parameters in Dump Creek, including SO<sub>4</sub>, Al, B, Cd, Cr, Cu, Fe, Mn, Ni, Pb, Se and Zn, resulting in further exceedances of water quality parameters. The increasing trend in water quality parameters occurs in conjunction with rising groundwater levels in Bore D3 (monitoring point 34), located upgradient of the KVAR / KVAD.

Between 2012 and 2019 concentrations of water quality parameters continue to rise in apparent correlation with groundwater levels in bore D3. Accordingly, the 95<sup>th</sup> percentile concentrations of water quality parameters at Dump Creek currently exceed water quality parameters for AI, B, Cd, Cu, F, Fe, Mn, Ni, Pb and Zn, whilst pH is now highly acidic (pH 3.1); (Table 4-2).

The long-term water quality and recent monitoring results (2018-2019) for Dump Creek indicate a possible impact from the KVAR on surface water quality. However, due to the complexity of current and historic land use activities, including local chitter deposits, pumping and discharge regimes for the KVAD and SSCAD, it is not considered suitable to directly attribute any impacts observed to a single source such as the KVAR. The observed results do however suggest that further hydrogeological investigation is required to provide an improved resolution on the factors contributing to water quality in Dump Creek, including isolating potential contributions from SSC, SSCAD, and the KVAD to groundwater and surface water quality.

Interpretation of long term water quality data (Table 5-1) for Lidsdale Cut Pond (WX5/monitoring point 40) is complicated by the re-location of sampling points used to sample Lidsdale Cut Pond. It is noted however that an overall similar trend of rising concentrations is observed in Lidsdale Cut Pond (WX5), with an overall increase in the number of parameters exceeding WQGVs along with an increased relative magnitude of exceedances. Similar to Dump Creek, the complexity of current and historic land use activities, including local chitter deposits, the KVAD and SSCAD suggest that it is not suitable (based on the data set available) to directly attribute any impacts observed solely to a single source such as the KVAR. It should be noted however that the Lidsdale Cut Pond forms part of the operational water reticulation system and is not classified as a "receiving environment" location.

The KVAR does not appear to be affecting water quality for sites 225, 93, or 83 (which are dominated by discharge from Springvale Mine); sites 38 and 79 (which are dominated by water quality from SSCAD) or site 92 which is located in the middle-upper portions of the catchment upgradient of the SSCAD and KVAR.

Water quality data collected at Site 38 (representing the SSCAD Water Input from the Return Canal) has shown a significant improvement since December 2017, with the concentrations of all tracked parameters (Figures A11 and A12) steadily decreasing over this time. Operational discharge into this canal has ceased and natural runoff has now become the dominant contributor to the flows observed.

Both the recorded SO<sub>4</sub> concentrations and the conductivity levels have been decreasing at Site 86 (KVAR / KVAD North Wall runoff collection) since May 2018 (Figure A19). Further investigation into this improvement would be required to determine the cause.

# 6.2 KVAR Impacts on Groundwater Quality

In general, the groundwater quality trends have been less consistent compared to the surface water quality trends over the last year. A mix of steady, fluctuating and upward/downward trends have been observed on the site. The demarcated "receiving environment" location (D5 / 36) has shown a fluctuating but stable trend with regards to the key parameters which are being tracked.

# **Groundwater Receiving Site**

A review of groundwater quality in Bore D5 (Site 36) in correlation with groundwater levels in Bore D3 (Site 34) has found that:

- Between 1988 and 2003 (pre-KVAR emplacement) 95<sup>th</sup> percentile concentrations of water quality indicator parameters Mn, B, and Al exceeded water quality guideline values (WQGVs), whilst SO<sub>4</sub> and Ni were notably elevated above background, and pH was moderately acidic at pH 4.7. Time series data on groundwater elevations in D3 indicates a rise and fall in groundwater elevations during this period (1988-1994), which show little effect on the concentrations of water quality parameters.
- Concentrations of water quality parameters in Bore D5 generally remained stable until 2008, following which point there is a noted rise in concentrations of water quality indicator parameters SO<sub>4</sub>, Mn, B, Al, Ni, and conductivity (to concentrations greater than historic results), along with a drop in pH to more acidic conditions (pH 4.09). The observed rise in concentrations in Bore D5 occurs in conjunction with a groundwater level rise in Bore D3 to elevations exceeding 920 mAHD. As this pattern is not observed in historic data for Bore D5, the results indicate a possible influence from the KVAR, associated with groundwater migration into the KVAR upgradient of Bore D5.
- Water quality in Bore D5 generally improved following February 2010, indicating possible unblocking of the Stage 1 KVAD toe drains resulted in an improvement of groundwater quality. Subsequently, the concentrations of water quality parameters in Bore D5 generally decreased towards pre-KVAR concentrations until July 2013, following which point there are significant fluctuations in water quality, with 95<sup>th</sup> percentile concentrations of water quality parameters greater than historical background (1988-2003) values. The observed fluctuations in water quality parameters are observed in conjunction with fluctuations and an overall rise in groundwater levels in bore D3, which is likely to be attributed discharge from Springvale Mine upgradient of the KVAR.

relatively reduced in concentrations of indicator parameters. The relative effect of SSC dilution on groundwater quality downgradient of the KVAR / KVAD can be observed comparison of Bore D5 with Bore D6, which is located downgradient of the Stage 1 KVAR area and away from SSC, and shows a similar relationship between groundwater levels in Bore D3 and water quality trends post 2007.

For the current monitoring period (2018-2019) groundwater at D5 currently exceeds WQGVs for Al, B, Cd, Cr, Cu, Fe, Hg, Mn, Ni, Pb and Zn.

The concentrations of indicator parameters in Bore D5 are notably elevated above pre-KVAR values following the rise in groundwater levels in 2008 to elevations >920 mAHD. Decreased pH, and increased Ni and SO<sub>4</sub> are potentially indicative of a fresh dry ash source. Comparison of water quality data in Bore D5 with that of Bore D6 suggests that discharge through SSC as a result of Springvale Mine Discharge from LDP009 is having a potential effect (likely dilutive) on water quality in D5 through local seepage to groundwater adjacent to SSC.

# Additional Sites: D1, D2, D3, D4, D6, AP09, AP17

Review of additional groundwater monitoring sites associated with the KVAR has identified elevated concentrations of water quality parameters in Bore D6, along with KVAD monitoring bores AP09, AP17, KVAD Seepage.

The long-term water quality monitoring results for Bore D6 show a recent rising trend in concentrations of key water quality parameters in the period following 2008 and in conjunction with a groundwater level rise in Bore D3 (located upgradient of the KVAD / KVAR). The observed trend in rising concentrations in Bore D6 has continued since 2008 in conjunction with a trend of rising groundwater levels in Bore D3, which is sustained artificially by discharge from Springvale Mine at LDP009.

Similar to bore D5, historic pre-KVAR water quality (1988-2003) in D6 was elevated with respect to a number of water quality parameters including indicator parameters Ni and Mn, and displayed a relatively reduced pH (pH 5.6). An increasing trend for several indicator parameters are subsequently observed for D6 between 2003 and 2010, concurrent with the start of rising groundwater levels in Bore D3. Between 2010 and 2019 with the continued rising trend groundwater at Bore D3, there is a correlated rising trend in water quality parameter concentrations at Bore D6, including concentrations of SO<sub>4</sub>, Al, B, Mn and Ni between, along with a further reduction in pH. Subsequently the 95<sup>th</sup> percentile concentrations of water quality parameters within bore D6 currently exceed WQGVs for several parameters, including indicator parameters TDS, SO<sub>4</sub>, Al, Mn, Ni, and conductivity. Zinc is above WQGVs and pH is below the lower WQGVs limits (pH 4.5).

Groundwater quality within the KVAR / KVAD shows variable response due to the complex system of toe drains, canals and pumping regimes. Overall groundwater quality at AP09 and AP17 representing the northern wall of the KVAD has deteriorated since 2010, along with groundwater quality at D6 located downgradient of the KVAR / KVAD. This is attributed to recirculation and concentration of water through the return canal in July 2012 for D6 and rise in water levels, flooding the KVAR as a result of Springvale Mine Discharge for AP09 and AP17.

Groundwater monitoring site D4 appears to have historic water quality impacts, potentially associated with the KVAR, however, is currently dominated by water quality from SSC and Springvale Mine Discharge.

Groundwater monitoring Site D2 is not quantifiably impacted by the KVAR and concentrations of key water quality parameters are generally below the WQGVs, with the exception of pH which is below the lower limits.

Groundwater quality at site D1 reflects conditions in the middle-upper portions of the catchment, upgradient of the SSCAD and KVAR. pH is below the lower limit and concentrations of Al, Cr, Cu and Pb generally exceed WQGVs.

# 7 Limitations

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The report should not be applied for any purpose other than that originally specified at the time the report was issued.

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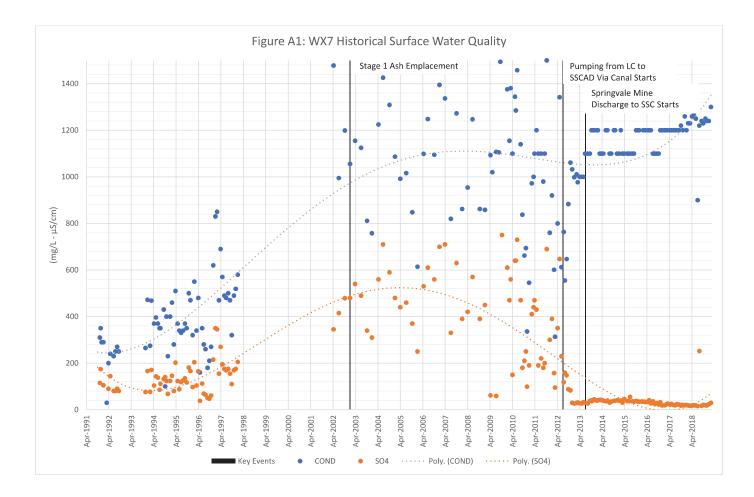
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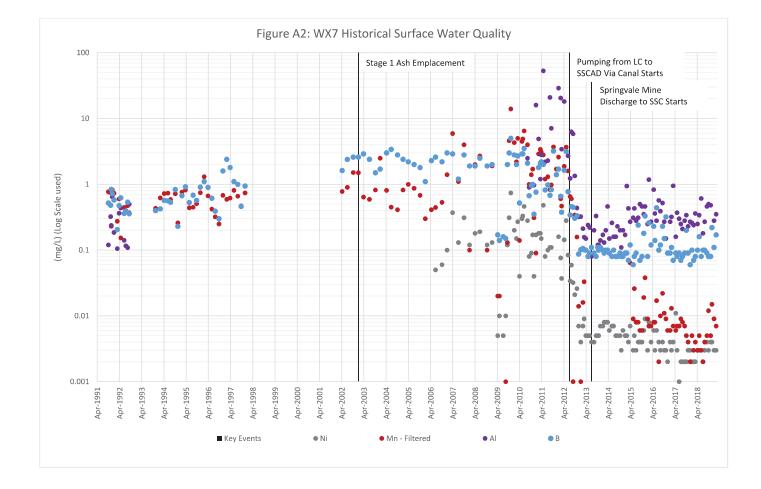
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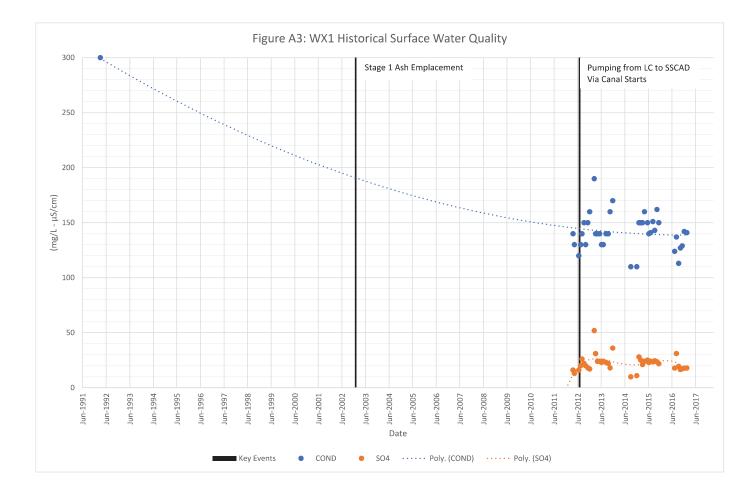
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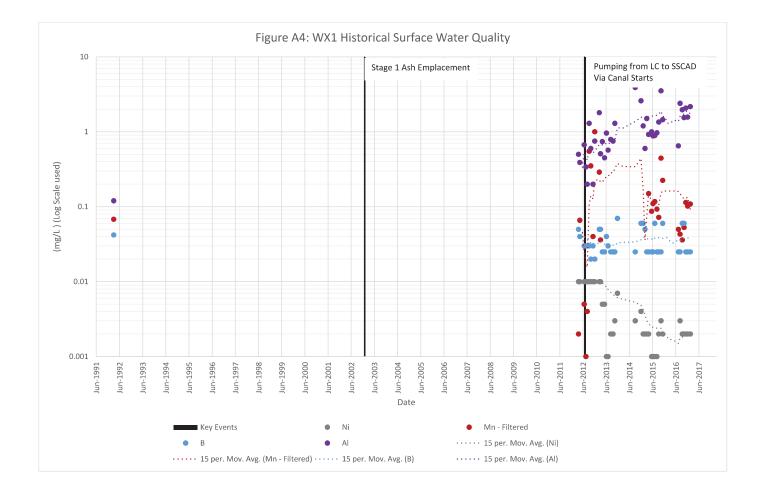
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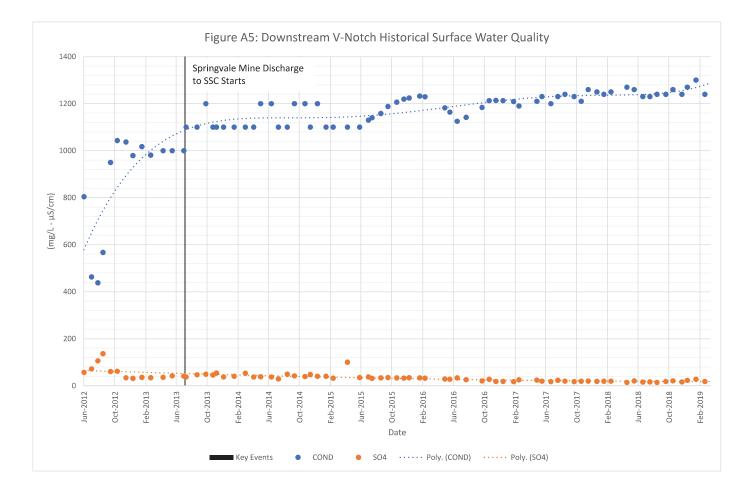
Appendix A Surface Water Quality Trends 1991-2019

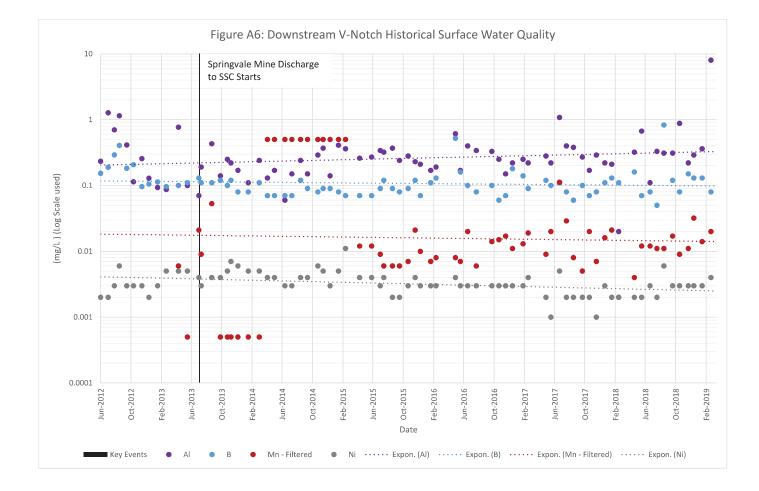


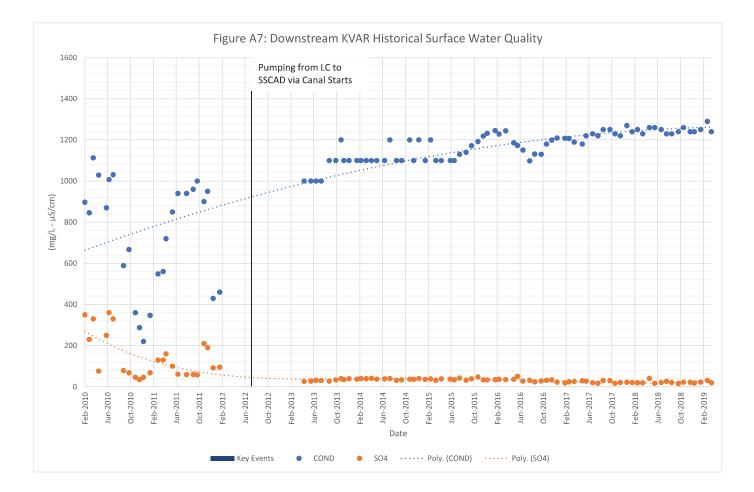


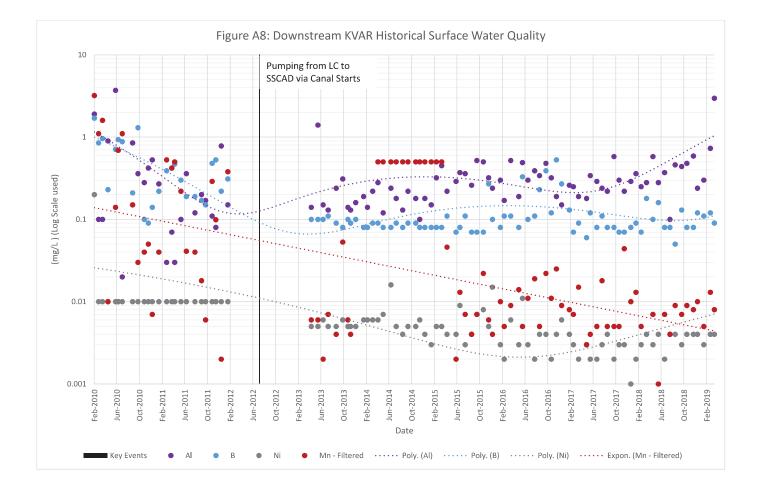


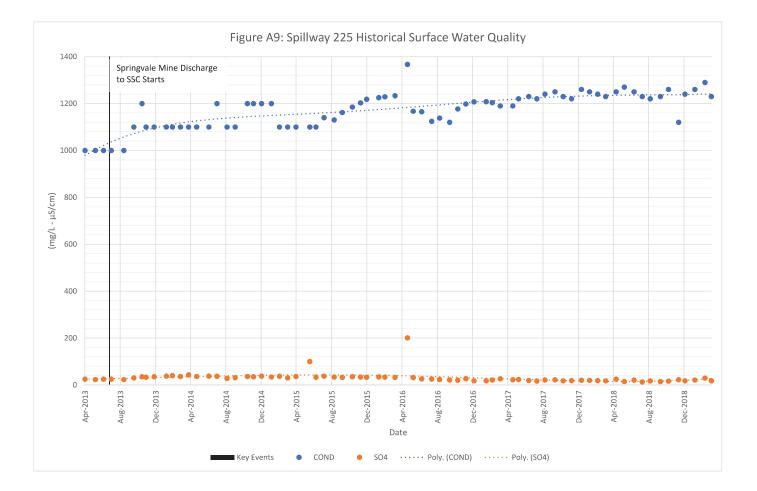


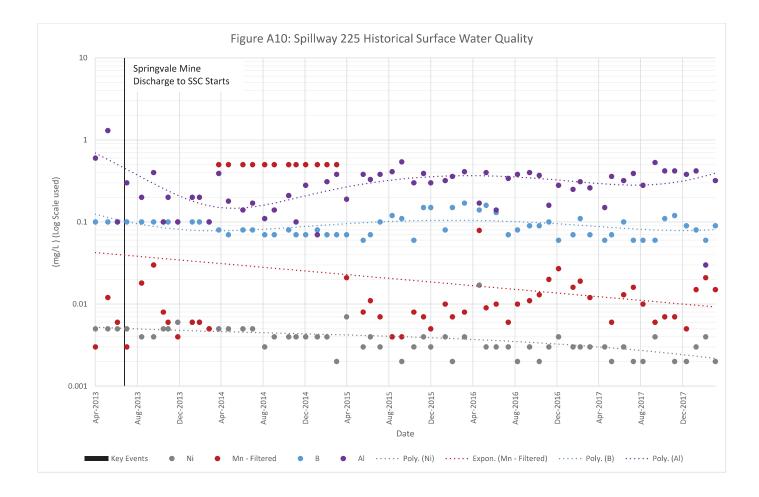


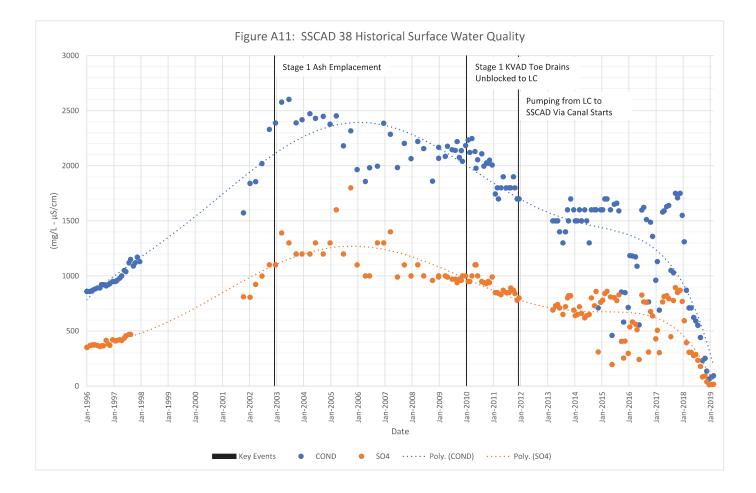


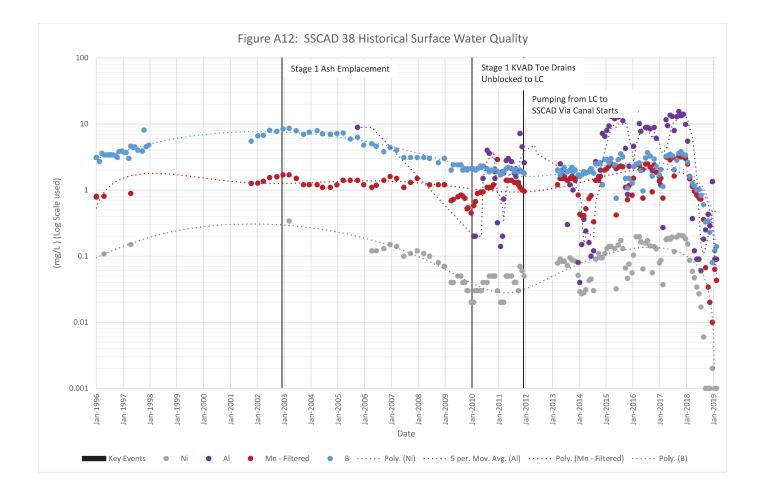


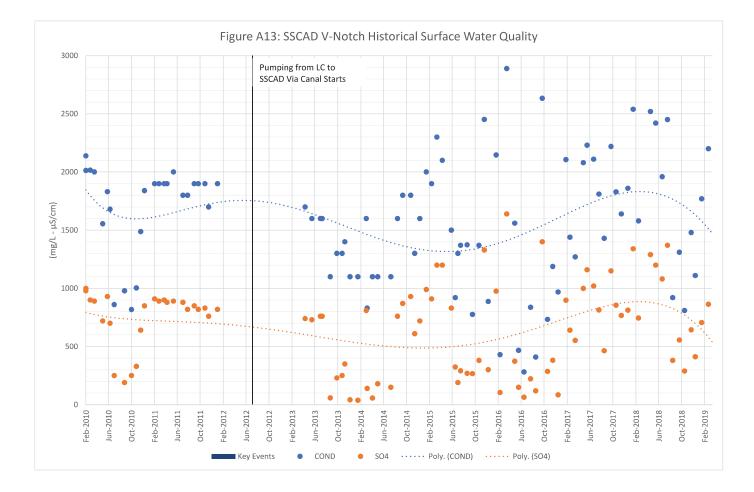


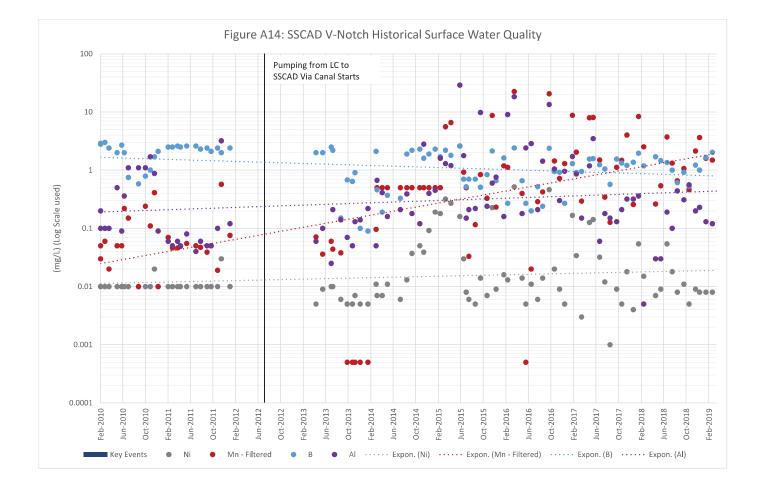


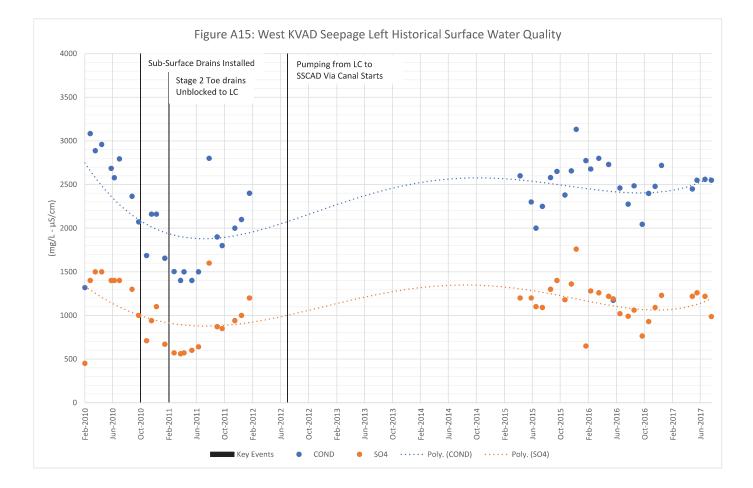


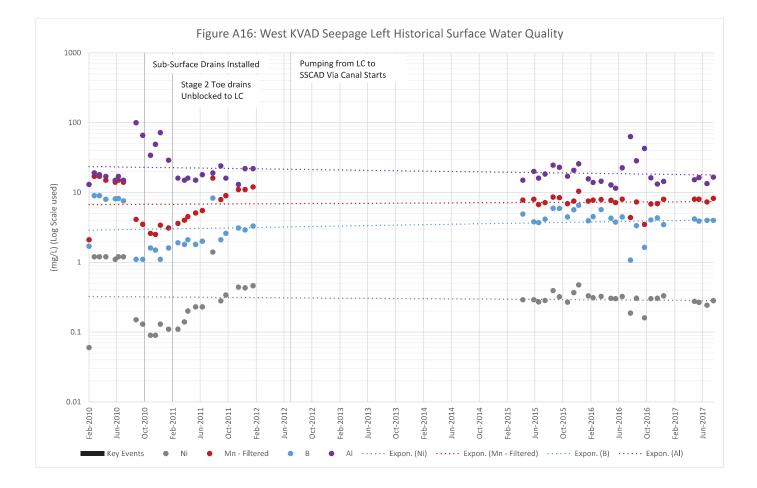


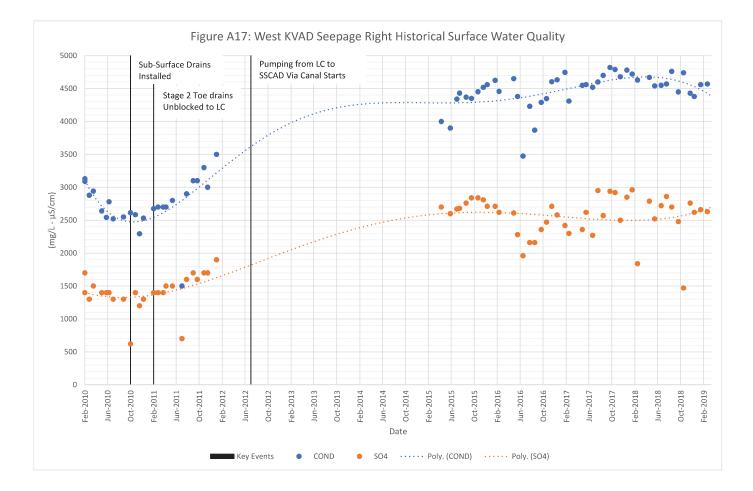


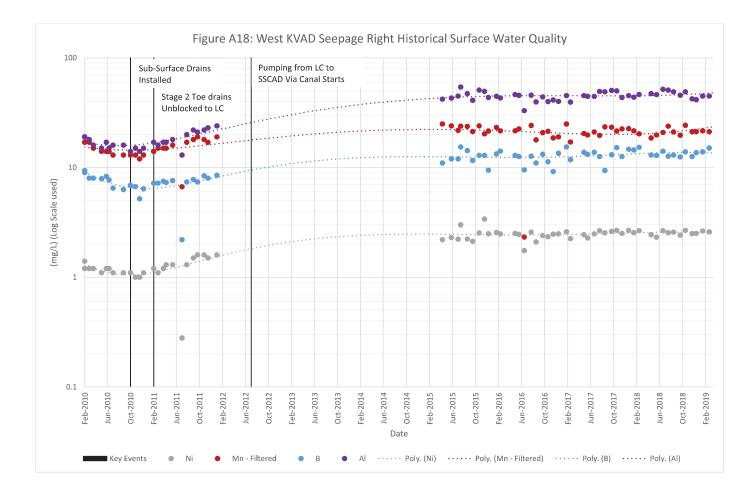


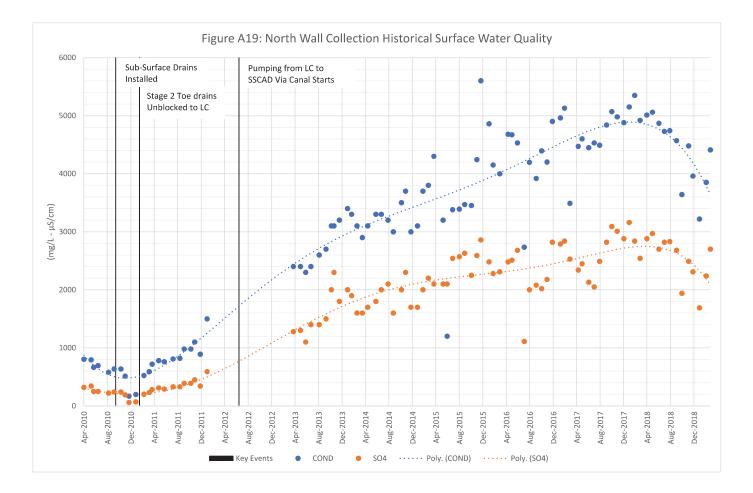


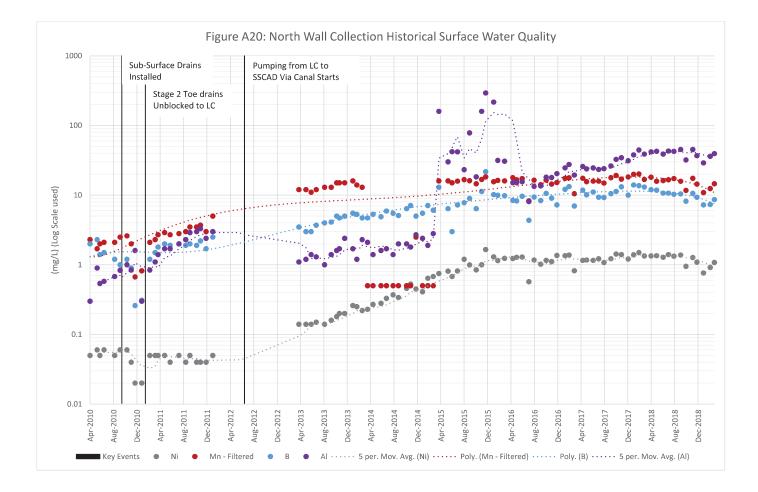


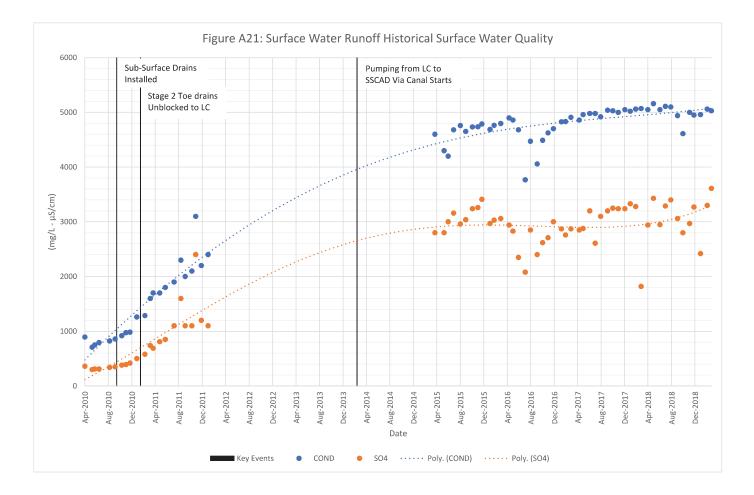


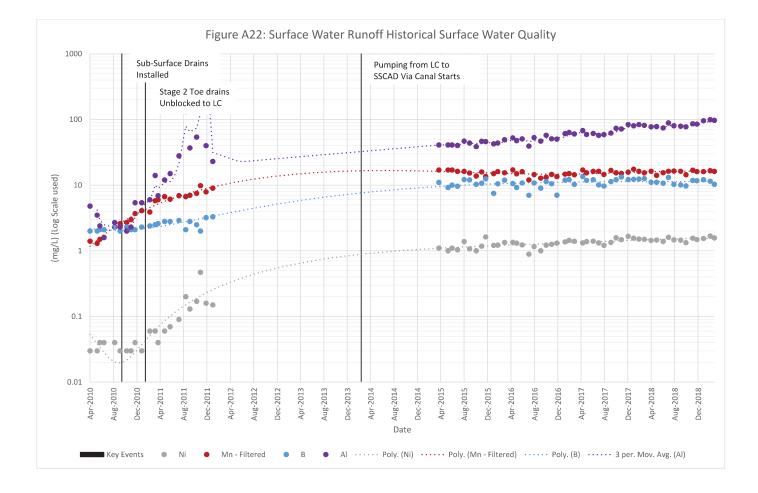


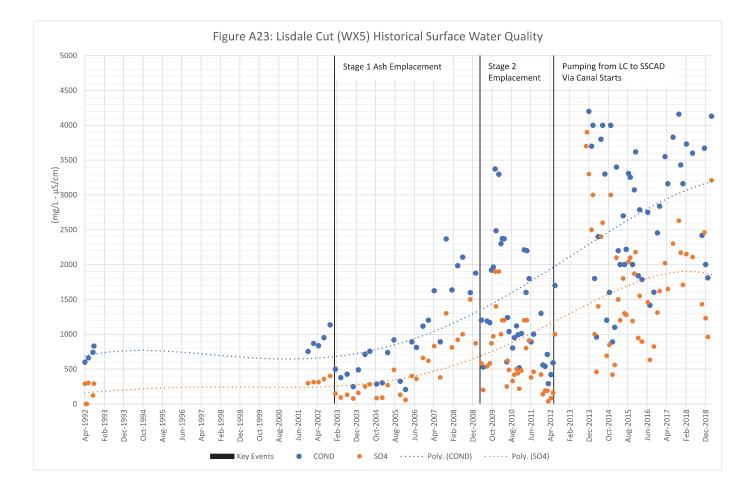


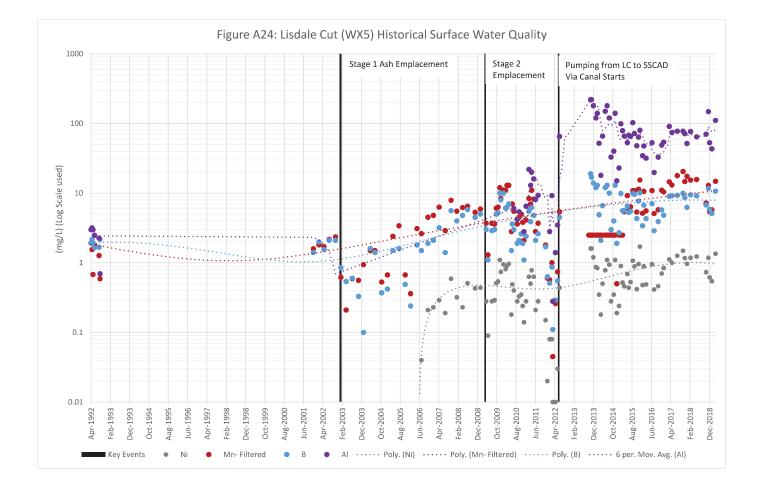


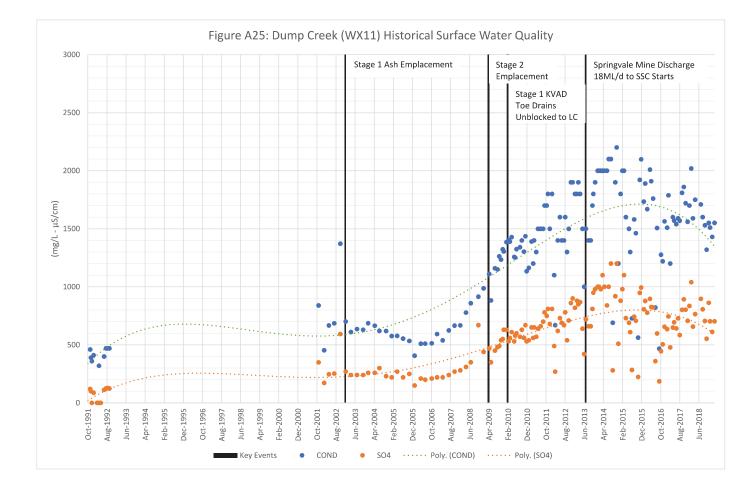


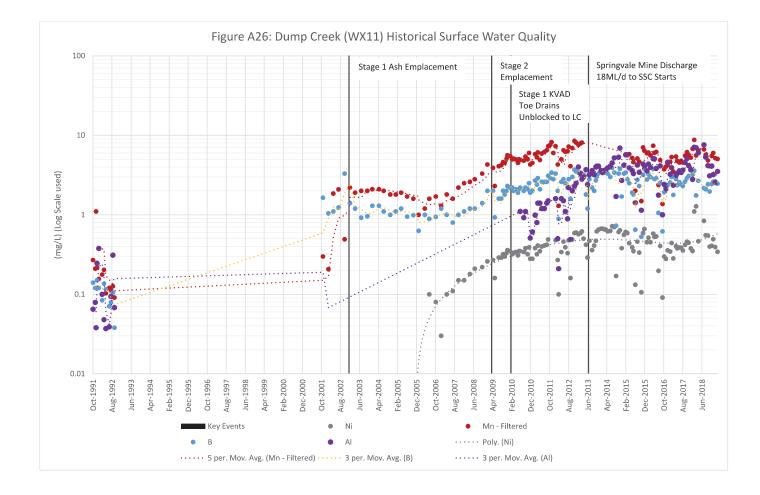


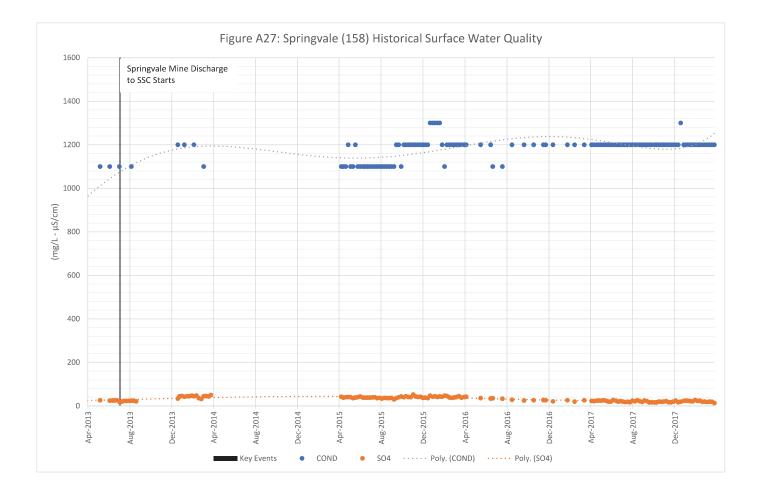


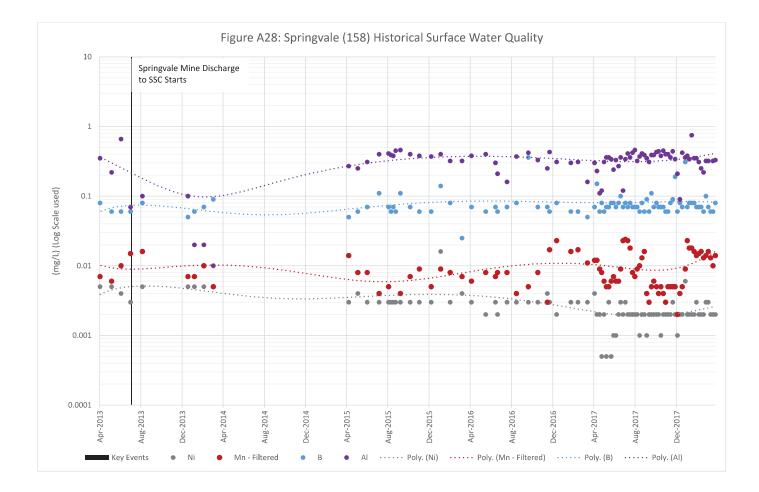




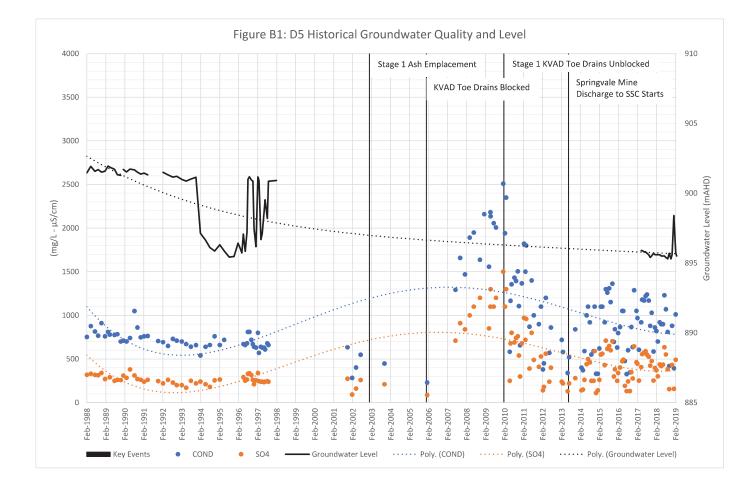


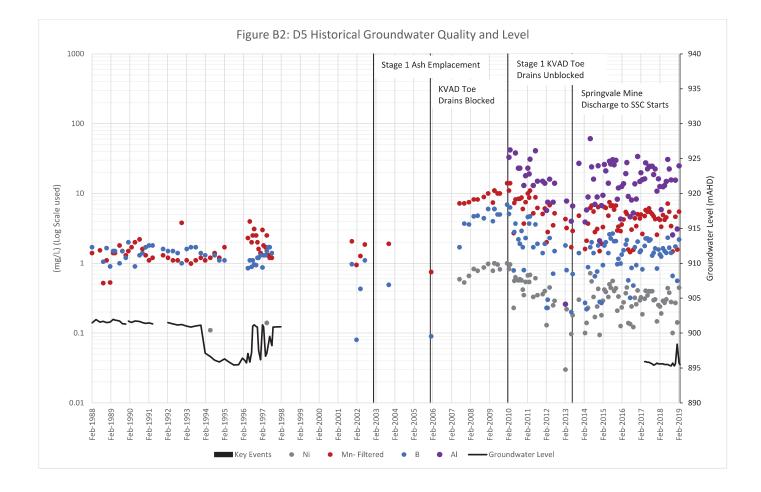


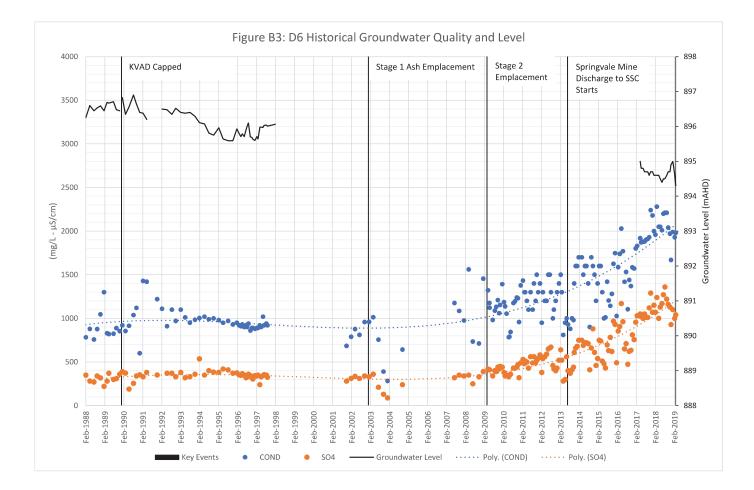


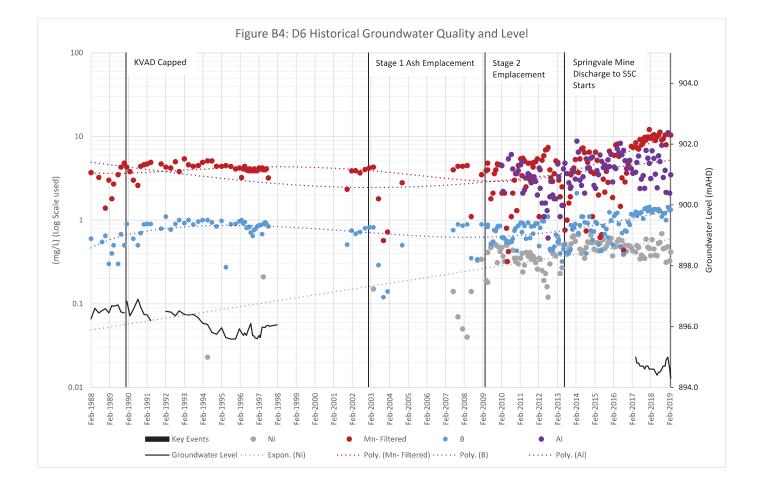


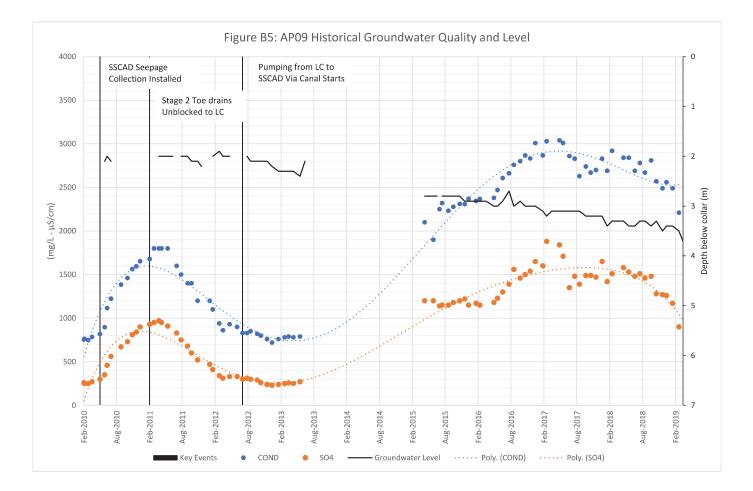
## Appendix B Groundwater Quality Trends 1988-2019

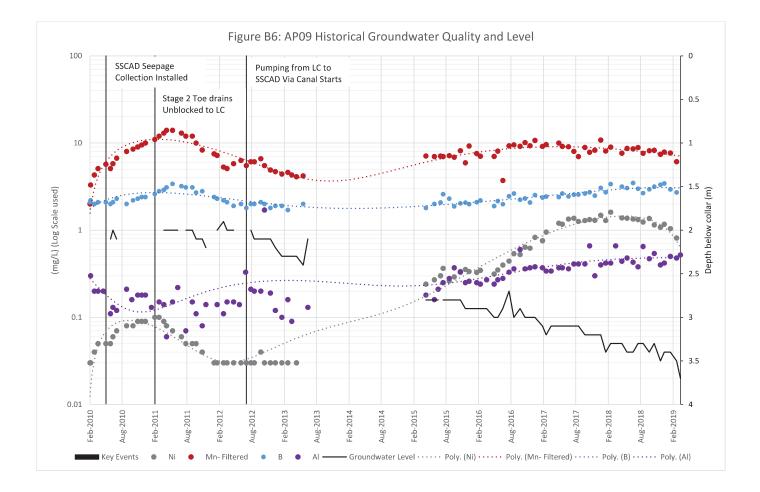


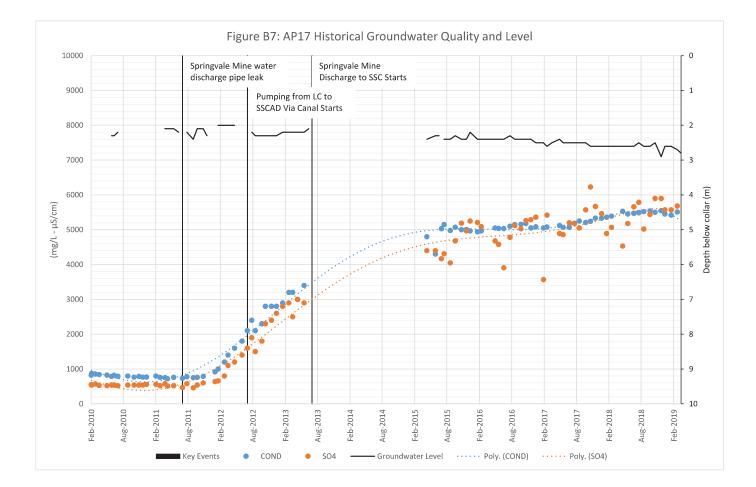


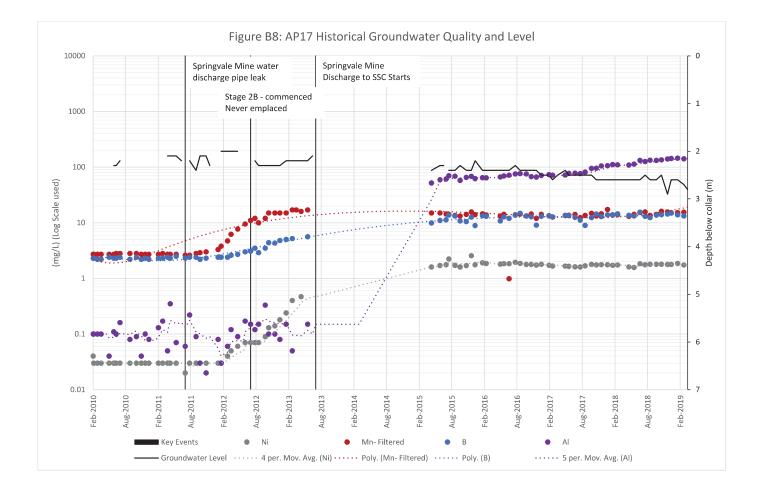


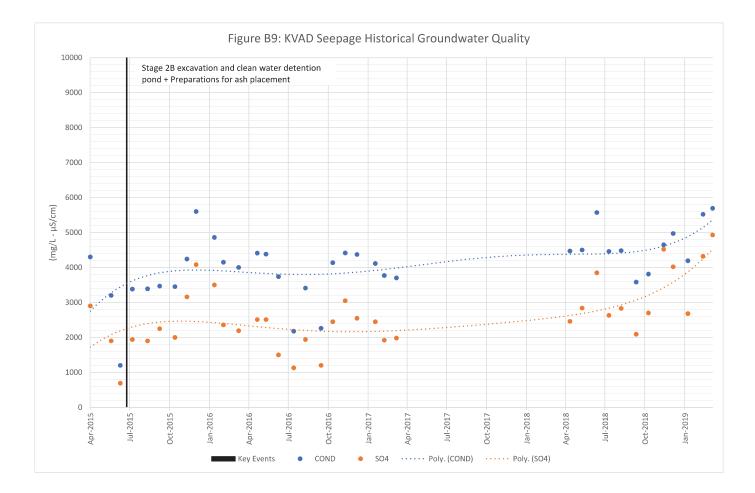


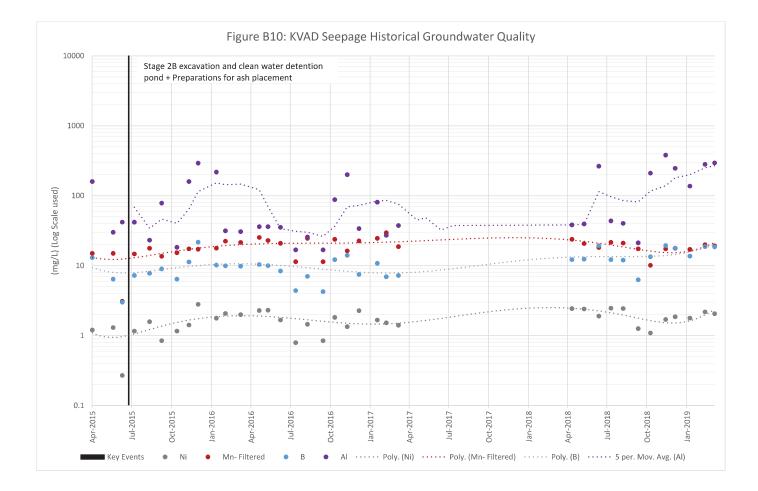


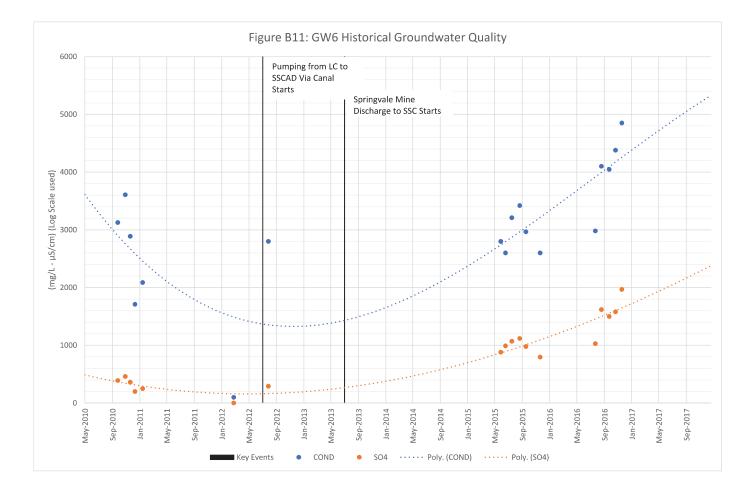


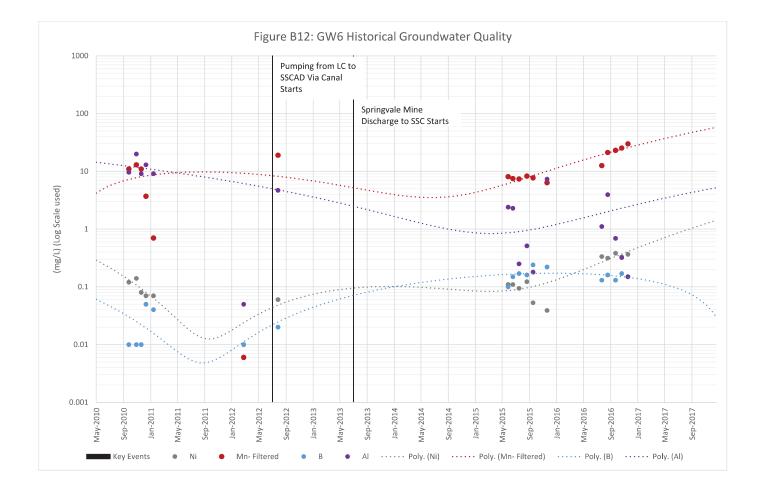


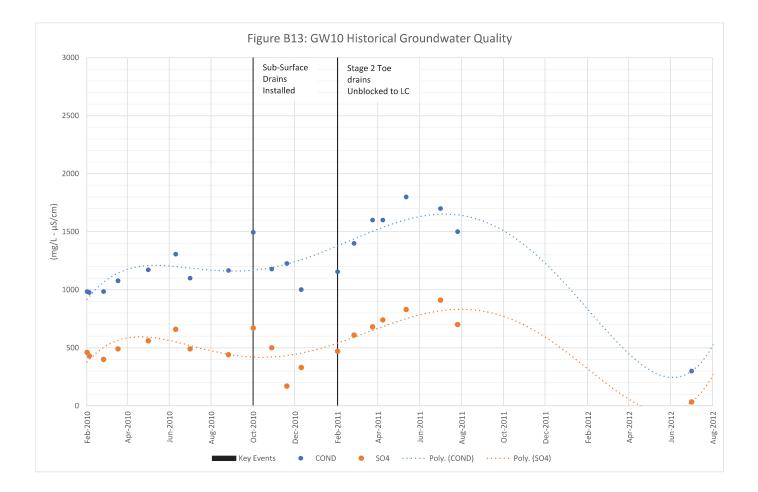


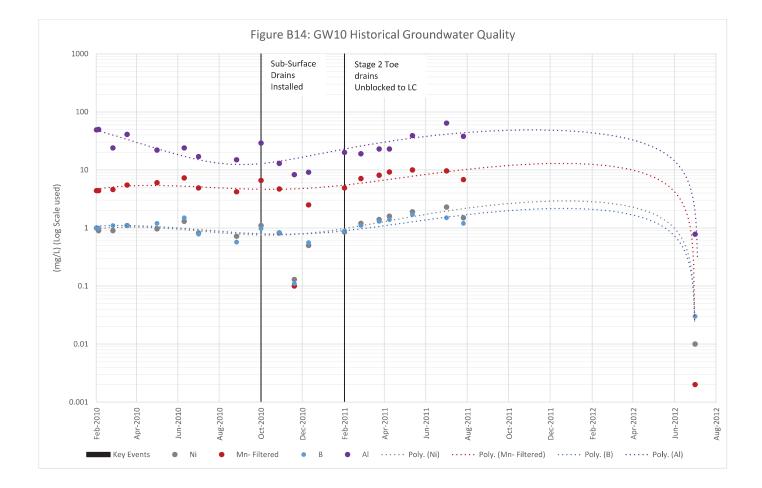


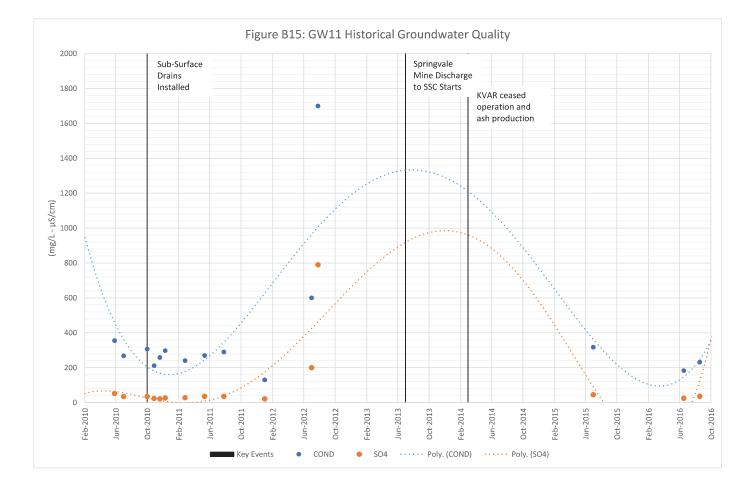


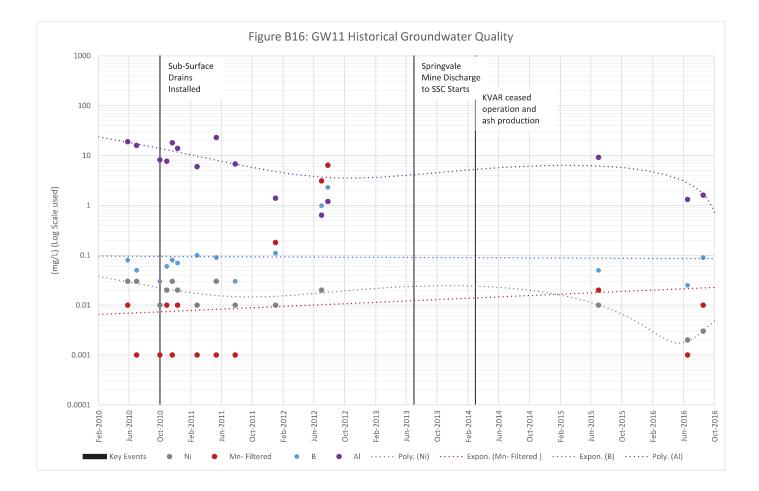


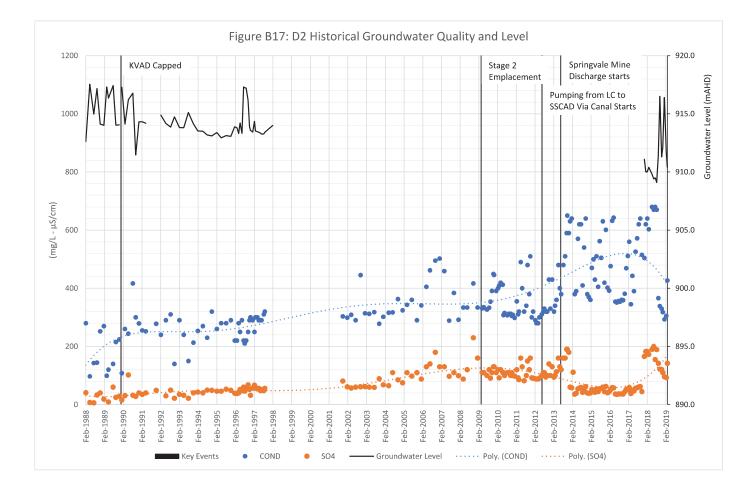


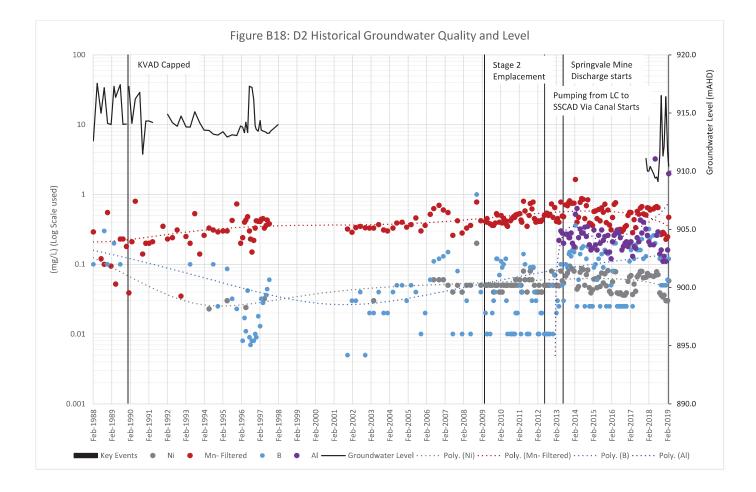


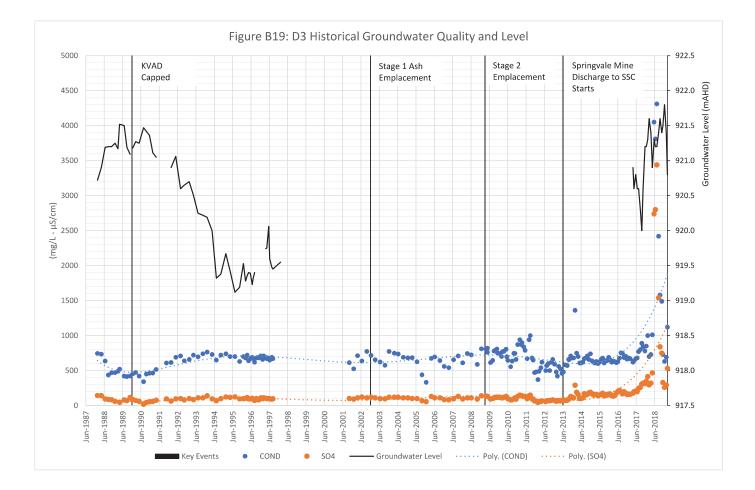


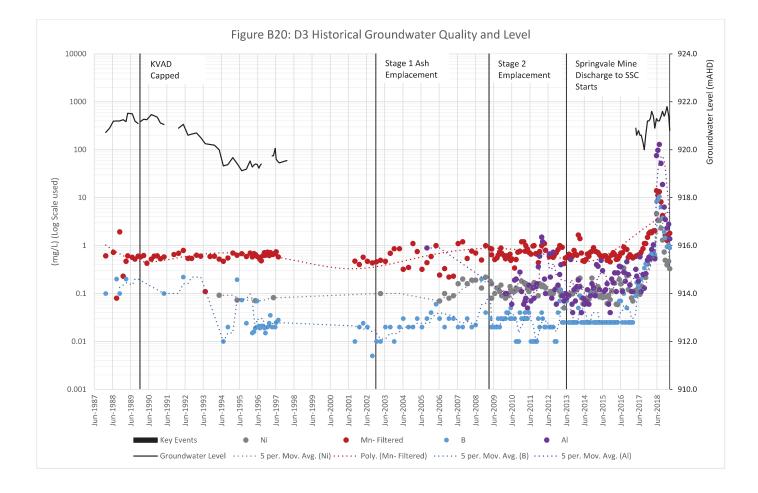


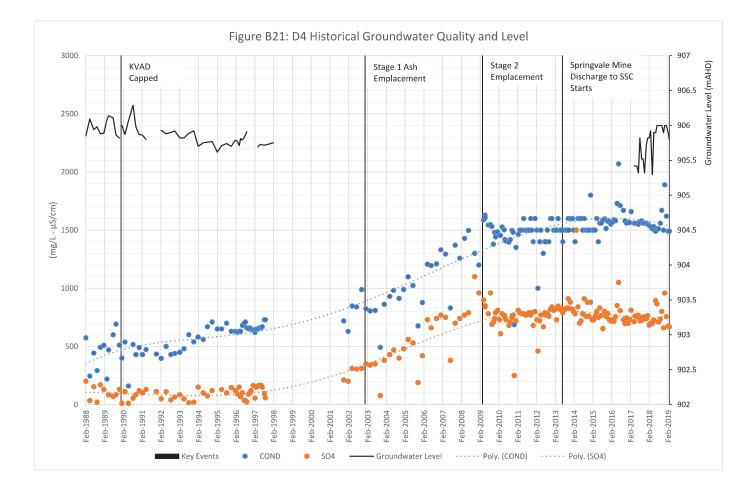


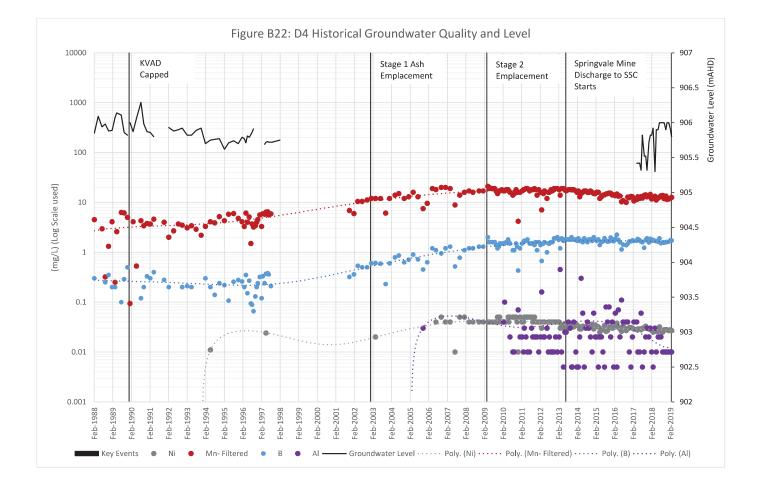


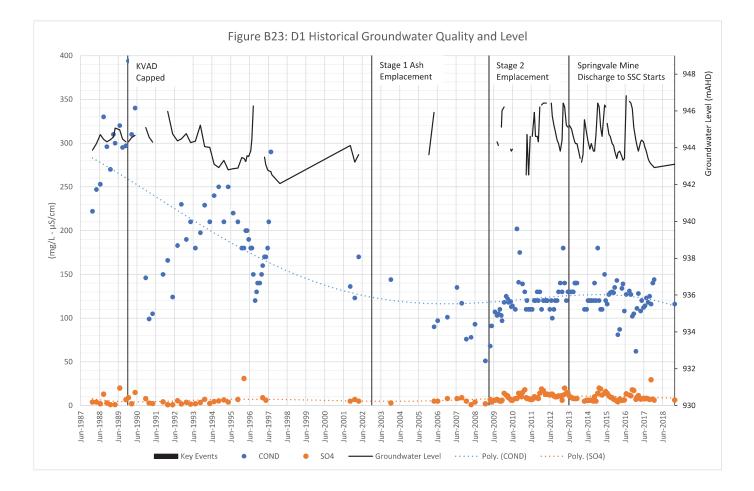


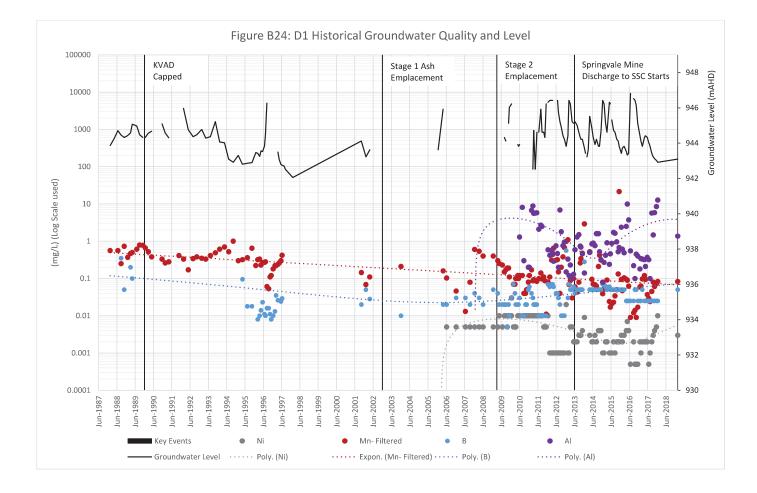












Appendix C 2018 – 2019 Surface Water / Groundwater Monitoring Results and Summary Statistics

41. Sawyers Swamp Creek Lower (WX7)	Lower (WX7)																						
Sample Date	Hd	Cond (µs/cm)	TDS	SO4	ū	AI*	As	Ag	Ba	Be	*n	8	c	C	u.	Fe-F	Hg	Мn	Mo	ïz	Pb	Se	Zn*
19/04/2018		1260	728	18	5.65	0.03	0.015	<0.001	0.019	Q	0.100	<0.0001	<0.001	<0.001	1.2			0.003	0.038	0.003	Η		<0.005
18/05/2018	-	1270	718	19	6.36	0.03	0.014	<0.001	0.018	Q	0.160	<0.0001	<0.001	<0.001	0.9	-	_	0.005	0.032	0.003	-	_	<0.005
20/06/2018		1250	820	18	4.80	0.03	0.013	<0.001	0.009	Q	0.080	<0.0001	<0.001	<0.001	0.7			0.003	0.028	0.003		_	<0.005
18/07/2018	+	006	722	15	4.78	0.02	0.024	<0.001	0.022	Ð	0.100	<0.0001	<0.001	<0.001	1.0	0.064		0.002	0.043	0.002	+	_	<0.005
15/08/2018	+	1220	746	252	5.23	0.03	0.019	<0.001	0.023	Q	0.100	<0.0001	<0.001	<0.001	1.4	+	_	0.004	0.043	0.003	+	+	<0.005
20/09/2018	+	1240	808	17	4.85	0.03	0.025	<0.001	0.027	9	0.090	<0.0001	<0.001	<0.001	0.8	+	+	+	0.044	0.004	+	+	<0.005
17/10/2018	8.63	1230	744	21	5.05	0.05	0.019	<0.001	0.022	Q	0.080	<0.0001	<0.001	<0.001	0.9	0.024	_	0.012	0.042	0.003	<0.001	0.0003	<0.005
21/11/2018	-	1250	757	19	4.43	0.04	0.027	<0.001	0.025	Ð	0.080	<0.0001	<0.001	<0.001	1.1	+	_	+	0.044	0.004	-	+	0.007
13/12/2018	-	1240	750	19	5.36	0.06	0.020	<0.001	0.024	Ð	0.220	<0.0001	<0.001	0.001	0.9	0.022	<0.00004	0.015	0.049	0.004	<0.001	0.0004	<0.005
16/01/2019		1240	620	23	5.07	0.04	0.012	<0.001	0.013	Q	0.110	<0.0001	<0.001	<0.001	0.7		_		0.037	0.003	<0.001	0.0004	0.007
20/02/2019	8.66	1300	785	29	6.50	0.04	0.016	<0.001	0.014	Q	0.170	<0.0001	<0.001	<0.001	0.9	0.035	<0.00004	0.007	0.049	0.003	<0.001	0.0014	0.010
//2019		1220	755	24	12.20	0.06	0.010	<0.001	0.016	Q	0.080	<0.0001	<0.001	<0.001	0.8		_	_	0.038	0.005	0.003	0.0007	0.010
41. Sawyers Swamp Creek Lower (WX7)	Lower (WX7)																						
Sample Date	Hd	Cond	TDS	SO4	ū	Al*	As	Ag	Ba	Be	*	8	٦	Сu	Ľ	Fe-F	Р	Mn	Mo	ī	Pb	Se	Zn*
Minimum	8.53	900	620	15	4.43	0.02	0.010	<0.001	0.00	g	0.080	<0.0001	<0.001	<0.001	0.7	0.006	<0.00004	0.002	0.028	0.002	<0.001	<0.0002	<0.005
Maximum		1300	820	252	12.20	0.06	0.027	<0.001	0.027	Ð	0.220	<0.0001	<0.001	0.001	1.4				0.049	0.005	-	0.0014	0.010
Mean		1218	746	40	5.86	0.04	0.018	<0.001	0.019	Q	0.114	<0.0001	<0.001	<0.001	0.9	$\vdash$			0.041	0.003		0.0004	0.006
Median		1240	748	19	5.15	0.04	0.018	<0.001	0.021	QN	0.100	<0.0001	<0.001	<0.001	0.9	0.023		0.005	0.043	0.003	0.001	0.0003	0.005
95th Percentile	_	1287	815	154	9.69	0.06	0.026	<0.001	0.026	Q	0.198	<0.0001	<0.001	<0.001	1.3		<0.00004	_	0.049	0.005	0.002	0.0011	0.010
20th Percentile	8.65																						
_																-							
Surface Water WQGV (	6.5-8.0	2200	1500^	1000++	350+	5.25^^	0.024	0.00005	0.7+++	0.1	1.25	0.0015	0.005	0.005	1.5+++	0.3+++	0.00006	1.9	0.01+	0.05	0.005	0.005	0.153
93. SSC Downstream V-notch	tch																						
Sample Date	Ξ	Cond (us/cm)	TDS	SO4	ō	AI*	As	Ag	Ba	Be	*8	ß	ŗ	Cu	Ľ	Fe-F	Hg	nM	Mo	ī	РР	Se	Zn*
18/04/2018	8.66	1240	770	16.1	5.36	0.65	0.017	<0.001	0.022	g	0.100	<0.0001	<0.001	<0.001	11	0.027		0.012	0.038	0.003	<0.001	_	<0.005
17/05/2018		1270	736	14.3	5.76	0.32	0.014	<0.001	0.017	Q	0.160	<0.0001	<0.001	<0.001	1.2	Η		0.004	0.031	0.002	$\square$	$\square$	<0.005
20/06/2018	_	1260	760	20.5	5.33	0.67	0.013	<0.001	0.007	Q	0.070	<0.0001	<0.001	<0.001	0.9		<0.00004	0.012	0.028	0.002	-	_	<0.005
18/07/2018	_	1230	776	15.4	4.92	0.11	0.028	<0.001	0.025	Q	0.080	<0.0001	<0.001	0.0040	0.9			0.012	0.048	0.003		_	0.005
15/08/2018	8.59	1230	644	16.8	4.96	0.33	0.020	<0.001	0.026	Q 4	0.050	<0.0001	<0.001	<0.001	0.7	0.026	<0.00004	0.011	0.047	0.002	<0.001	0.0002	<0.005
13/10/2018	+	1240	730	17.8	5.18	0.31	0.018	<0.001	0.023	2 9	0.120	<0.0001	<0.001	<0.001	0.0	╈	+	0.017	0.044	0.003	╈	╋	<0.005
21/11/2018	-	1260	765	20.7	4.74	0.88	0.033	<0.001	0.027	9	0.080	<0.0001	<0.001	<0.001	1.2	┢			0.045	0.003	0.001	-	0.006
13/12/2018	$\vdash$	1240	811	16.0	5.01	0.22	0.018	<0.001	0.025	Ð	0.150	<0.0001	<0.001	<0.001	11	0.019		╞	0.048	0.003	<0.001		<0.005
16/01/2019	8.55	1270	775	22.8	5.60	0.29	0.010	<0.001	0.012	Q	0.130	<0.0001	<0.001	0.0050	1.1				0.036	0.003	<0.001	0.0006	0.007
20/02/2019	8.60	1300	764	27.8	6.07	0.36	0.016	<0.001	0.014	QN	0.130	<0.0001	<0.001	<0.001	1.0	0.024	<0.00004	0.014	0.050	0.003	<0.001	0.0016	0.009
14/03/2019	8.51	1240	710	18.2	13.40	8.02	0.015	<0.001	0.021	QN	0.080	<0.0001	<0.001	0.0010	0.9	0.006	<0.00004	0.020	0.033	0.004	0.002	0.0004	<0.005
03 SSC Downetream V-notch	ch A																						
	┝	1000	F							F	F				F				╞	ŀ	ŀ	$\left  \right $	
Sample Date		Cond (µs/cm)	TDS	SO4	ū	AI*	As	Ag	Ba	Be	*	8	c	Cu	u.		_	Мn	Mo	ïZ	_	_	Zn*
Minimum	+	1230	644	14.3	4.55	0.11	0.010	<0.001	0.007	Q	0.050	<0.0001	<0.001	<0.001	0.7		_	0.004	0.028	0.002		-	<0.005
Maximum	8.70 8.50	1300	811 748	27.8	13.40 5 a1	8.02	0.033	<0.001	0.027	Q Q	0.830	<0.0001	<0.001	0.005	1.6	0.076	<0.00004	0.032	0.050	0.006	0.002	0.0016	0.009
Median	-	1240	762	17.3	5.26 5.26	04	0.018	-0.001	0.023		╈	-0.001	-0.001	7000	<u>-</u> -	╈			0.044	0.003		+	0.007
95th Percentile		1287	796	25.6	10.17	4.88	0.031	<0.001	0.027	2 0	0.535	<0.0001	<0.001	0.005	1.4	0.074	<0.00004	0.027	0.049	0.005	0.002	0.0013	0.009
	0 55										╈					t		┝			┢		

0.005

0.005

0.05

0.01+

1.9

00000

0.3+++

1.5+++

0.005

0.005

0.0015

1.25

0.1

0.7+++

0.00005

0.024

5.25^^

350+

1000++

1500^

2200

 20th Percentile
 8.55

 80th Percentile
 8.63

 8urface Water WOGV
 6.5-8.0

	Zn*	Н	_	<0.005	<0.005	<0.005	<0.005	<0.005	0.007	0.006	0.007	0.010	<0.005			Zn*	<0.005	0.010	0.008	0.007	010.0		0.153		2n*	10.005	<0.005	<0.005	0.012	<0.005	<0.005	0.010	<0.005	0.008	0.011	0.006		zn*	<0.005	0.012	0.010	0.011	0.012	
	Se	<0.0002	<0.0002	0.0003	<0.0002	0.0002	0.003	0.003	0.004	0.003	0.0005	0.0016	0.0004			Se	<0.0002	0.0016	0.0005	0.0003	2100.0		0.005		ď		<0.0002	<0.0002	<0.0002	<0.0002	<0.002	2000.0	0.0004	0.0006	0.0017	0.0004		Se	<0.0002	0.0017	0.0006	0.0004	0.0015	
	Pb	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	0.001	<0.001	<0.001	0.001	0.001			Pb	<0.001	0.001	0.001	0.001	100.0		0.005		ła	0000	<0.001	0.001	<0.001	<0.001	<0.001	0.001	<0.001	<0.001	<0.001	0.002		Pb	<0.001	0.002	0.002	0.002	0.002	
	ïZ	0.003	0.004	0.002	0.004	0.004	0.003	0.004	0.004	0.004	0.003	0.004	0.004			Z	0.002	0.004	0.004	0.004	0.004		0.05		ï	0000	0.003	0.002	0.003	0.003	0.002	0.004	0.004	0.003	0.003	0.004		ïZ	0.002	0.004	0.003	0.003	0.004	
	Mo	0.041	0.033	0.027	0.046	0.047	0.045	0.044	0.044	0.046	0.036	0.056	0.035			Mo	0.027	0.056	0.042	0.044	0.052		0.01+		Mo	0000	0.034	0.028	0.046	0.046	0.044	0.046	0.048	0.037	0.052	0.036		Mo	0.028	0.052	0.042	0.044	0.050	
	ЧN	0.007	<0.001	0.007	0.004	0.009	0.007	0.009	0.008	0.010	0.005	0.013	0.008			ЧИ	0.004	0.013	0.008	0.008	210.0		10		Mn	0000	0.008	0.013	0.013	0.014	0.010	0.024	0.015	0.011	0.021	0.010		ЧU	0.008	0.024	0.014	0.013	0.023	
	Hg	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004			Hg	<0.00004	<0.00004	<0.00004	<0.00004	<0.0004		90000		Ŧ	P00000	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	-0.0004	<0.00004	<0.00004	<0.00004	<0.00004		Нg	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	
	Fe-F	0.024	0.005	0.016	0.061	0.014	0.010	0.022	0.047	0.020	0.019	0.023	0.013			Fe-F	0.005	0.061	0.023	0.020	0.00		1 1 1 1		Fo-F	0000	0.013	0.003	0.054	0.005	0.004	0.055	0.007	0.005	0.014	0.006		Fe-F	0.003	0.055	0.015	0.007	0.055	
	u.	1.2	1.2	0.8	0.7	0.7	0.8	1.5	1.1	1.1	1.0	1.1	0.9			L.	0.7	1.5	1.0	= ;	1.4		1 5			. c.	12	2.2	1.5	1.2	1.5	0. 1	1.2	1.0	1.1	0.9		Ľ	6.0	2.2	1.4	1.2	2.0	
	C	<0.001	<0.001	<0.001	<0.001	0.0020	<0.001	<0.001	0.0010	<0.001	<0.001	0.0010	<0.001			Cu	<0.001	0.002	0.001	0.001	0.002		0.005		ō	0.0160	<0.001	<0.001	<0.001	<0.001	<0.001	-0.001	0.0010	<0.001	0.0020	0.0020		G	<0.001	0.016	0.005	<0.001	<0.001	
	ċ	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001			ð	<0.001	<0.001	<0.001	<0.001	L00.0>		0.005		č	0.001	<0.001	<0.001	<0.001	<0.001	<0.001	20.001	<0.001	<0.001	<0.001	<0.001		స	<0.001	<0.001	<0.001	<0.001	<0.001	
	8	<0.0001	<0.0001	<0.0001	<0.0001	<0.0001	<0.0001	<0.0001	<0.0001	<0.0001	<0.0001	<0.0001	<0.0001			ਲ	<0.0001	+	<0.0001	+	1000.05		0.0015		5	0000	0.0001	<0.0001	<0.0001	<0.0001	<0.0001	-0.0001	-	$\vdash$	<0.0001	<0.0001		8	+	-	┢	$\left  \right $	<0.0001	
	ň	Η	-		-	<0.05		0.080	-	0.120		0.120	-					+	0.105	+	╈		1 25		ů		+	0.070	┢	<0.05	+	0 100	+	┢┤		0.100		å			┢	0.100	+	
	Be	QN	Q	QN	Q	Q		-	-		+	+	_			Be	Q	g		+	R		5		Be	e e		Q	Q	Q		+		QN	g	Q		Be	Ð	Q	Q	Q	Q	
	Ba	0.021	0.017	0.008	0.023	0.025	0.027	0.022	0.027	0.023	0.011	0.017	0.013			Ba	0.008	0.027	0.020	0.022	0.027				Ba		0.016	0.006	0.026	0.023	0.025	0.024	0.023	0.008	0.014	0.013		Ba	0.006	0.026	0.018	0.022	0.026	
	Ag	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001		+	_	<0.001			Ag	<0.001	<0.001	<0.001	<0.001	LUU.U>		0 0005		40	-000	<0.001	<0.001	<0.001	<0.001	<0.001	-0.001	<0.001	<0.001	<0.001	<0.001		Ag	<0.001	<0.001	<0.001	<0.001	<0.001	
	As	0.016	_	_	0.025			_	_		+	-	0.008			_	_	-	0.018	╈	0.028		0.024		Δc					-	0.026	╈			-	0.014		As	0.010	╞	-	$\left  \right $	0.029	
	Al*	0.58	_	_	0.10		0.44	-	0.59		+	+	2.97					+	0.63	╉	1.98		5 25.00		Al*			1.00		+	0.45	+			-	8.46		Al*	0.07	┢			5.18	
	ū	5.23	_	_	_	_	_	-	-	_	-	_	13.90				-	+	5.97	+	10.60		3501		-		-	4.77		+	4.57	+		5.06	_	13.70		ō	4.57			$\left  \right $	10.53	
	SO4		_		27	-	_	22	-	-	23		_					+		21			10001		so.			21		-	14	╞			+	18		SO4	13		19		27 1	
	TDS	762	660		727	_	_	728	_	748	760	796	681				660	796	729	728	/83		1500 15		TDS		704	728	728	644		728		710	748	736		TDS	634	748	713	728	743	
	Cond T [µs/cm] T				1230 7				1240 7		-		1240 6		Cond			_	-	1245			1			us/cm)		1250 7		_	1230	+		1260 7	_	1230 7		Cond T	-	$\vdash$			1281 7	
	DH Hd	8.65 11	_		8.53 11			-	-	8.63 11	-	-	8.69 13		-	_	-	-	8.63	+	+	8.65			Ŭ H			8.19 11		8.25 1;		╈		8.80 11	-	8.20 11		DH Hq	8.12 1.	$\vdash$	-	8.23 11		8.17
ream KVAR			_		_	-							_	oam KVAR		_	_			+	+		+					-				┢					way		00			$\left  \right $	_	
83. SSC Downstream KVAR	Sample Date	18/04/2018	17/05/2018	20/06/2018	18/07/2018	15/08/2018	19/09/2018	17/10/2018	21/11/2018	13/12/2018	16/01/2019	20/02/2019	14/03/2019	83 SSC Downstream KVAR		Sample Date	Minimum	Maximum	Mean	Median	95th Percentile	20th Percentile 80th Percentile	Surface Water WOGV	225. SSCAD Snillwav	Sample Date	10/04/2010	17/05/2018	20/06/2018	18/07/2018	15/08/2018	19/09/2018	21/11/2018	13/12/2018	16/01/2019	20/02/2019	14/03/2019	225. SSCAD Spillway	Sample Date	Minimum	Maximum	Mean	Median	95th Percentile	20th Percentile

	zn*	3.540	3.450	3.330	3.890	3.730	3.780	3.550	3.820	3.750	3.600	3.760	3.620		Zn*	3.330	3.890	3.652	3.675	3.859			0.153		Zn*	3.60	3.73	3.34	3.65	3.40	2.35	3.10	2.61	1.87	2.31	0/.7		Zn*	1.87	3.73	3.02	3.22	3.69		
	Se	0.0013	0.0016	0.0017	0.0015	0.0017	0.0018	0.0015	0.0012	0.0013	0.0009	0.0012	0.0013		Se	0.0009	0.0018	0.0014	0.0014	0.0018			0.005		Se	0.0042	0.0043	0.0035	0.0037	0.0048	0.0025	0.0038	0.0036	0.0017	0.0036	1 000.0		Se	0.0017	0.0051	0.0038	0.0038	0.0050		
	ЧЧ	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	0.001	<0.001	<0.001	<0.001	<0.001	<0.001		Pb	<0.001	0.001	<0.001	<0.001	<0.001			600.0		q	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001		Ч	<0.001	<0.001	<0.001	<0.001	<0.001		
	īZ	2.540	2.440	2.320	2.660	2.550	2.580	2.420	2.670	2.500	2.510	2.640	2.590		ī	2.320	2.670	2.535	2.545	2.666			0.05		ïz	1.340	1.350	1.280	1.400	1.330	0.949	1.270	1.090	0.762	0.915	1.000		ïZ	0.762	1.400	1.179	1.275	1.391		
	Mo	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001		Mo	<0.001	<0.001	<0.001	<0.001	<0.001			0.01+		Mo	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	200.0		Mo	0.002	0.002	0.002	0.002	0.002		
	Мn	21.3	18.6	19.8	20.9	23.8	21.1	19.7	24.3	21.2	21.2	21.6	21.2		ЧN	18.6	24.3	21.2	21.2	24.1			1.9		Mn	18.1	15.8	16.2	16.6	17.3	11.7	17.4	14.4	10.9	12.4	14.0		Mn	10.9	18.1	15.1	15.8	17.8		
	Hg	<0.00004	<0.00004	<0.00004	0.00006	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004		Hg	0.00006	0.00006	0.00006	0.00006	0.00006			0.00006		면	<0.0004	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	<0.0004		Нg	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004		
	Fe-F	21.0	25.7	33.0	38.2	37.6	24.6	21.2	52.8	61.3	83.8	53.2	42.9		Fe-F	21.0	83.8	41.3	37.9	73.9			0.3+++		Fe-F	32.6	36.0	38.8	35.8	35.9	17.0	64.6	36.6	19.6	35.8	40.0		Fe-F	17.0	64.6	36.2	35.9	57.6		
	u.	21.0	19.9	28.2	13.3	17.4	18.8	12.0	21.9	14.0	15.1	15.3	15.4		u.	12.0	28.2	17.7	16.4	25.4	T		1.5+++		u	54.1	60.0	66.3	54.4	68.2	24.7	70.8	46.4	33.6	40.1	0.24		u	24.7	70.8	51.5	51.9	69.7		
ľ	Cu	<0.001	0.0010	0.0020	0.0010	0.0010	0600.0	0.0080	0.0040	<0.001	<0.001	<0.001	0.0040		Cu	<0.001	0.009	0.004	0.003	0.009			0.005		Cu	0.002	<0.001	<0.001	0.002	0.002	0.003	0.002	0.002	0.004	0.002	200.0		Cu	0.002	0.004	0.002	0.002	0.004		
	ŗ	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001		ċ	<0.001	<0.001	<0.001	<0.001	<0.001			0.005		ŗ	0.003	0.003	0.003	0.002	0.002	0.002	0.002	0.002	0.003	0.003	c.uu3		ŗ	0.002	0.003	0.003	0.003	0.003		
	8	0.0021	0.0019	0.0020	0.0022	0.0020	0.0020	0.0021	0.0022	0.0025	0.0026	0.0024	0.0024		8	0.0019	0.0026	0.0022	0.0022	0.0026	1		0.0015		8	0.0003	0.0003	0.0004	0.0003	0.0002	0.0003	0.0002	0.0003	0.0003	0.0004	c000.0		B	0.0002	0.0004	0.0003	0.0003	0.0004		
	*œ	13.4	13.0	12.9	14.1	12.7				12.6		13.9	15.1		* 0	$\vdash$	_	13.4					1.25		*	12.0	11.8	10.7	10.7	10.3	8.2	10.6	9.3	7.3	6.7	0.7		B*	7.3	12.0	9.8	10.4	11.9		
	Be	QN	QN	ND	Q	DN	Q	Q	Q	Q	Q	Q	QN		Be	Q	ND	DN	QN	ND			1.0		Be	9	Q	Q	QN	9 g	2 2	Ð	QN	Q :				Be	Ð	Q	QN	QN	Ð		
	Ba	<0.001	0.001	0.001	0.002	<0.001	0.006	0.002	0.002	0.002	0.001	<0.001	0.001		Ba	<0.001	0.006	0.002	0.002	0.005			0.7+++		Ba	0.001	<0.001	<0.001	0.001	<0.001	0,001	<0.001	<0.001	<0.001	<0.001	100.0		Ba	0.001	0.001	0.001	0.001	0.001		
	Ag	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001		Ag	<0.001	<0.001	<0.001	<0.001	<0.001			0.00005		Ad	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001		Ag	<0.001	<0.001	<0.001	<0.001	<0.001		
	As	<0.001	<0.001	<0.001	0.001	<0.001	0.002	<0.001	0.001	<0.001	0.001	0.001	<0.001		As	0.001	0.002	0.001	0.001	0.002		+	0.024		As	0.005	0.004	0.004	0.005	0.004	0.003	0.005	0.004	0.003	0.005	0000		As	0.003	0.006	0.004	0.004	0.006		
	Al*	46.80	47.20	46.20	51.70	50.80	49.00	45.70	49.00	42.30	41.60	44.80	44.80		Al*	41.60	51.70	46.66	46.50	51.30			5.25 v v		Al*	41.80	42.70	38.80	43.00	42.50	32.00	45.10	36.90	29.10	36.10	00.80		AI*	29.10	45.20	39.39	40.65	45.16		
	ū	35.10	34.30	55.80	31.50	32.90	35.20	29.80	34.80	30.90	33.10	32.30	31.70		ū	29.80	55.80	34.78	33.00	46.74	+	+	350+		0	27.70	25.70	22.60	27.20	22.20	19.10	20.00	19.80	15.20	16.40	13.30		ū	15.20	27.70	21.58	21.10	27.48		
	SO4	2570	2790	2520	2720	2860		2480	1470	2760	2620	2660	2630		SO4	1470	2860	2565	2645	2829			1000+++		s04	2880	2970	2700	2820	2830	1940	2490	2310	1690	2240	00/2		SO4	1690	2970	$\vdash$	2690	2930		
	TDS	4010	3890	3100	3830	4030			4170	3920	3160	3760	4020		TDS	3100		3803		4108	+	╉	1500^		TDS	4330	2550	4210	3230	4060	2650	4160	3490	+	3020	3/40		TDS	2550	4330	$\vdash$	3615	4277		
	Cond (µs/cm)		4670		4550	4570						4560	4570		Cond (us/cm)	┝				4751		-	2200		Cond	5010	5060			4740			3960	+	+	4410		Cond	-		$\vdash$	4525	5038		
.	Hd		2.90		3.03	2.98			$\left  \right $	2.93		2.93	2.94	rface Right	Hd	┝		2.93	2.93		2.88	2.98	6.5-8.0		H		2.89	2.89		2.86			3.00	+	2.84	2.04		Hd	2.84		$\vdash$	2.89		2.86	
ou. West NVAD Wall Subsultace high	e Date		_			_								80. West KVAD Wall Subsurface Right	> Date	_			_	centile		_	_	86. North Wall Collection	Date					+					╈	_	86. North Wall Collection	Date							
U. WEST NY	Sample Date	18/04/2018	17/05/2018	20/06/2018	18/07/2018	15/08/2018	19/09/2	17/10/2018	21/11/2018	13/12/2018	16/01/2019	20/02/2019	14/03/2019	30. West KV	Sample Date	Minimum	Maximum	Mean	Median	95th Percentile	20th Percentile	80th Percentile	Surface Water WQGV	6. North Wa	Sample Date	18/04/2018	17/05/2018	20/06/2018	18/07/2018	15/08/2018	17/10/2018	21/11/2018	13/12/2018	16/01/2019	20/02/2019	14/03/2013	6. North Wa	Sample Date	Minimum	Maximum	Mean	Median	95th Percentile	20th Percentile	

0.019         0.001           0.019         0.001           0.019         0.001           0.019         0.001           0.019         0.001           0.019         0.001           0.019         0.001           0.019         0.001           0.019         0.001           0.019         0.001           0.019         0.001           0.019         0.001           0.023         0.001           0.035         0.001           0.035         0.001           0.035         0.001           0.035         0.001           0.035         0.001           0.035         0.001           0.036         0.001           0.036         0.001           0.036         0.001           0.036         0.001           0.036         0.001           0.036         0.001           0.036         0.001           0.037         0.001           0.036         0.001           0.036         0.001           0.036         0.001           0.046         0.01           0.056
30.4         0.4         7.30           2940         20.4         7.30           2950         20.2         7.40           3490         22.6         89.90           3290         22.6         7.40           3290         22.5         89.90           3290         22.6         77.40           3290         22.6         90.30           3600         22.6         90.30           3270         25.1         86.00           3270         25.1         86.00           3216         24.8         95.90           3610         21.6         94.40           3610         21.6         94.40           3610         21.6         94.40           3610         21.6         94.40           3610         21.6         94.40           3610         21.6         94.40           3105         22.6         94.40           3106         21.6         94.40           3101         21.0         95.40           3102         24.40         145.00           3210         28.2         40.80           3210         28.40         145

39. Dump Creek (WX11)	(11)																						
Sample Date	Hd	Cond (µs/cm)	TDS	SO4	IJ	AI*	As	Ag	Ba	Be	*a	8	ΰ	Cu	LL.	Fe-F	Hg	лМ	Mo	ï	Pb	Se	Zn*
19/04/2018	3.22	1750	1180	765	30.30	6.22	<0.001	<0.001	0.042	DN	2.68	0.0006	0.001	0.014	2.0	5.880 <	<0.00004	6.470	<0.001	0.465	0.008	0.0006	1.350
18/07/2018	3.49	1710	986	896	28.30	7.12	<0.001	<0.001	0.030	DN	2.17	0.0016	<0.001	0.017	2.6	6.050 <	<0.00004	6.650	<0.001	0.840	0.003	0.0008	2.410
15/08/2018	3.46	1600	1150	806	39.80	5.06	<0.001	<0.001	0.023	DN	2.10	0.0008	<0.001	0.024	1.1	4.270 <	<0.00004	5.700	<0.001	0.553	0.004	0.0007	1.470
20/09/2018	3.22	1530	973	206	21.20	3.79	0.001	<0.001	0.022	QN	2.43	0.0018	<0.001	0.010	0.8	5.950 <	<0.00004	4.820	<0.001	0.548	0.007	0.0006	1.610
17/10/2018	3.25	1320	756	552	20.20	2.84	<0.001	<0.001	0.021	QN	1.96	0.0009	<0.001	0.005	1.1	4.000 <	<0.00004	4.100	<0.001	0.399	0.006	0.0004	1.080
21/11/2018	3.20	1550	1000	862	20.90	4.04	<0.001	<0.001	0.029	QN	2.44	0.0007	0.001	0.007	0.7	14.200 <	<0.00004	5.520	<0.001	0.408	0.007	0.0004	1.240
13/12/2018	3.18	1510	1080	703	19.40	3.16	<0.001	<0.001	0.023	QN	2.61	0.0010	<0.001	0.006	0.7	4.870 <	<0.00004	6.000	<0.001	0.495	0.006	0.0005	1.230
16/01/2019	3.27	1430	980	612	18.70	2.42	0.001	<0.001	0.032	QN	2.64	0.0005	<0.001	0.004	0.4	6.340 <	<0.00004	5.170	<0.001	0.393	0.004	0.0003	0.888
20/02/2019	3.24	1550	1030	703	25.40	3.26	<0.001	<0.001	0.033	DN	2.47	0.0004	<0.001	0.006	0.7	5.330 <	<0.00004	5.040	<0.001	0.343	0.005	0.0003	0.812
39. Dump Creek (WX11)	(11)																						
Sample Date	Hq	Cond (µs/cm)	TDS	SO4	cı	Al⁺	As	Ag	Ba	Be	B*	Cd	cr	Cu	Ľ.	Fe-F	Hg	Mn	Mo	Ni	Pb	Se	Zn*
Minimum	3.18	1320	756	552	18.70	2.42	<0.001	<0.001	0.021	ND	1.96	0.0004	<0.001	0.004	0.4	4.000 <	<0.00004	4.100	<0.001	0.343	0.003	0.0003	0.812
Maximum	3.49	1750	1180	896	39.80	7.12	0.001	<0.001	0.042	ND	2.68	0.0018	0.001	0.024	2.6	14.200 <	<0.00004	6.650	<0.001	0.840	0.008	0.0008	2.410
Mean	3.28	1550	1015	734	24.91	4.21	0.001	<0.001	0.028	ND	2.39	0.0009	<0.001	0.010	1.1	6.321 <	<0.00004	5.497	<0.001	0.494	0.006	0.0005	1.343
Median	3.24	1550	1000	706	21.20	3.79	0.001	<0.001	0.029	DN	2.44	0.0008	<0.001	0.007	0.8	5.880 <	<0.00004	5.520	<0.001	0.465	0.006	0.0005	1.240
95th Percentile		1737	1170	885	36.76	6.83	0.001	<0.001	0.039	DN	2.67	0.0017	<0.001	0.022	2.4	11.685 <	<0.00004	6.592	<0.001	0.748	0.008	0.0008	2.154
20th Percentile	3.21																						
80th Percentile	3.35																						

	Pb Se	$\left  \right $	0.007 0.0023	┥	+	+	+	0.002 0.0004	0.024 0.0012	+	0.024 0.0018			Pb Se			0.014 0.0013	0.015 0.0014	0.024 0.0022		0.005 0.005		Pb Se	$\mid$	0.006 0.0003		0.008 0.000	+			0.004 0.0002	╈	$\square$		Pb Se	0.003 0.0002		$\vdash$	0.007 0.0004	
	ž	0.289	0.272	0.304	0.440	0.378	0.279	0.100	0.271	0.142	0.447			z	0.10	0.45	0.29	0.28	0.44		0.05		ž	0.452	0.381	0.375	0.542	069.0	0.455	0.463	0.313	0.326	0.415		ï	0.31	0.69	0.45	0.45	
	Mo	0.001	<0.001	<0.001	0.001	<0.001	0.002	0.001	0.002	<0.001	0.003			Mo	0.00	0.00	0.00	0.00	0.00		0.01+		Mo	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001		Mo	<0.001	0.001	0.001	0.001	
	ЧW	4.900	4.200	_	7.140	5.460		_	4.650	+	5.490			Mn	1.47		4.28		6.55		1.9		Mn	10.500	_	_	11.300	+	9.400		7.970	_			Mn	7.97	11.30	10.00	10.40	
	Hg	<0.00004	0.00004	<0.00004	0.00008	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004			Hg	<0.00004	0.00008	<0.00004	<0.00004	<0.00004		0.00006		Нg	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004		Hg	<0.00004	0.00006	0.00	<0.00004	
	Fe-F	2.640	1.650	1.220	0.674	1.160	0.502	0.124	2.230	2.020	7.960			Fe-F	0.12	7.96	2.02	1.44	6.04		0.3+++		Fe-F	198.000	178.000	223.000	214.000	176.000	206.000	214.000	172.000	223.000	202.000		Fe-F	172.00	251.00	204.42	204.00	
	ш	0.8	0.4	0.2	0.6	0.5	0.2	0.1	0.6	0.1	1.2			u.	0.11	1.19	0.47	0.45	1.03		1.5+++		u.	0.2	0.2	0.3	0.3	0.3	0.2	0.3	<0.100	0.1	0.2		Ľ	<0.100	0.32	0.21	0.22	
	Cu	0.004	0.008	0.007	0.013	0.007	0.018	0.002	0.019	0.002	0.017			Cu	0.002	0.019	0.010	0.008	0.019		0.005		C	0.028	0.011	0.004	0.008	0.013	0.002	0.003	0.003	0.002	0.012		С	0.002	0.037	0.013	0.010	
	ŗ	0.003	0.001	0.004	0.004	0.002	0.003	<0.001	0.004	<0.001	9000			ç	<0.001	0.001	<0.001	<0.001	L00.0>		0.005		ζ	0.002	0.002	0.002	0.002	0.002	0.002	0.003	0.002	0.003	0.002		Ċ	0.002	0.014	0.003	0.002	
	Cd	0.0015	0.0008	0.0024	0.0057	0.0090	0.0036	0.0004	0.0028	0.0003	0.0029			Cd	0.0003	0.0090	0.0029	0.0026	0.00/8		0.0015		Cd	0.0014	0.0008	0.0006	0.0008	0.0013	0.0004	0.0006	0.0003	0.0004	0.0007		Cd	0.0003	0.0014	0.0008	0.0008	1000
	В*	1.640	1.500	1.410	2.320	1.670	1.410	0.660	1.740	0.560	2.190			*B	0.56	2.32	1.51	1.57	12.2		1.25		*8	1.35	1.35	1.31	1.29	1.10	1.20	1.21	1.00	1.32	1.33		ů,	1.00	1.43	1.27	1.32	
	Be	QN	Q	Ð	2	Q	9	Q	Q	2	a			Be	ΟN	Q	2	2	N		0.1		Be	Q	Q	Q 2	2 9	Ð	QN	QN	Q 2	Q	QN		Be	Q	Q	Q	Q	2
	Ba	0.032	0.022	0.026	0.038	0.022	0.032	0.019	0.057	0.025	0.080			Ba	0.019	0.080	0.035	0.029	0.072		0.7+++		Ba	0.012	0.011	0.011	0.012	0.012	0.012	0.012	0.012	0.014	0.015		Ba	0.011	0.055	0.016	0.012	1000
	Ag	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001			Ag	<0.001	<0.001	<0.001	<0.001	L00.0>		0.00005		Ag	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001		Ag	<0.001	<0.001	<0.001	<0.001	
	SA	0.002	<0.001	0.002	0.002	0.002	0.003	<0.001	0.002	0.001	0.004			As	0.001	0.004	0.002	0.002	0.004		0.024		As	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	0.001	<0.001		As	<0.001	0.006	0.004	0.004	
	۶IK	12.50	13.00	14.90	30.70	22.40	15.60	2.55	15.50	3.10	24.90			Al*	2.55	30.70	15.52	15.20	28.61		5.25^^		AI*	5.47	3.54	2.43	5.02	7.83	3.24	3.94	2.15	2.10	3.49		Al*	2.10	10.90	4.67	3.74	
	Ū	24.50	23.60	26.20	31.00	25.40	13.20	5.66	14.40	3.91	14.60			G	3.9	31.0	18.2	19.1	59.3		350+		ō	48.6	58.8	53.8	54.0	52.0	47.7	46.4	37.1 44 E	43.4	43.40		G	37.1	58.8	48.6	48.2	
	SO4	436	418	435	634	551	384	154	432	158	491			SO4	154	634	409	434	604		1000++		SO4	1000	1130	1170	1360	1220	1160	1130	929	1000	1040		SO4	929	1360	1126	1130	0007
	TDS	703	533	610	950	787	604	302	686	296	817			TDS	296	950	629	648	206		1500^		TDS	1830	1700	1740	2090	1880	1560	1850	1500	1740	1580		TDS	1500	2090	1768	1785	0000
	Cond (µs/cm)	920	006	006	1230	1070	810	420	880	394	1010			Cond (µs/cm)	394	1230	853	006	2/11		2200		Cond (us/cm)	2050	2050	2010	2210	2210	2040	1970	1670	1930	1980		Cond	1670	2210	2026	2025	0100
VGM1/D5	Hd	4.51	4.32	4.15	4.11	4.01	3.99	3.66	4.21	3.99	4.28		VGM1/D5	Hq	3.66	4.51	4.12	4.13	3 00	4.29	6.5-8.0	VGM1/D6	Hq	3.70	4.14	4.52	3./4 4.08	3.85	4.35	4.34	4.38	4.62	4.24	VGM1/D6	Hq	3.66	4.51	4.12	4.13	-
36. Groundwater Bore WGM1/D5	Sample Date	19/04/2018	18/05/2018	21/06/2018	19/07/2018	16/08/2018	20/09/2018	19/10/2018	13/12/2018	17/01/2019	21/02/2019		36. Groundwater Bore WGM1/D5	Sample Date	Minimum	Maximum	Mean	Median	95th Percentile	80th Percentile	Surface Water WQGV	37. Groundwater Bore WGM1/D6	Sample Date	19/04/2018	18/05/2018	21/06/2018	15/08/2018	20/09/2018	19/10/2018	22/11/2018	13/12/2018	21/02/2019	14/03/2019	37. Groundwater Bore WGM1/D6	Sample Date	Minimum	Maximum	Mean	Median	

	Zn*	1.400	1.340	1.330	1.320	1.390	1.210	1.270	1.060	0.958	1.020	0.904	0.664			Zn*	0.66	1.40	1.16	1.24	1.40			0.153		Zn*	5.29	5.12	5.01	5.76	5.54 E eo	5.72	5.67	5.67	5.97	5.51		Zn*	5.01	5.97	5.55	5.64	5.88		
	Se	0.0006	0.0006	0.0006	0.0005	0.0005	0.0006	0.0005	0.0003	0.0004	0.0003	0.0004	0.0003			Se	0.0003	0.0006	0.0005	0.0005	0.0006			0.005		e.S.	0.151	0.178	0.148	0.132	0.156	0.109	0.118	0.131	0.105	0.133		Se	0.105	0.178	0.136	0.133	0.170		
	Pb	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001			Pb	<0.001	<0.001	<0.001	<0.001	<0.001			0.005		Чd	0.002	<0.001	<0.001	0.001	<0.001	<0.001	<0.001	0.002	<0.001	<0.001		Pb	<0.001	0.002	0.002	<0.001	<0.001		
	ïz	1.470	1.380	1.370	1.340	1.320	1.240	1.360	1.150	1.080	1.170	1.040	0.814			ïz	0.81	1.47	1.23	1.28	1.43			0.05		ïN	1.70	1.61	1.57	1.83	1.76	1.79	1.79	1.78	1.78	1.74		ïZ	1.57	1.85	1.75	1.78	1.84		
	Mo	0.172	0.171	0.178	0.180	0.196	0.202	0.201	0.198	0.196	0.217	0.201	0.184			Mo	0.17	0.22	0.19	0.20	0.21			0.01+		Mo	0.008	0.002	0.002	0.004	0.003	0.003	0.004	0.007	0.002	0.006		Mo	0.00	0.01	0.00	0.00	0.01		
	Mn	9.560	7.640	8.660	8.560	8.860	7.610	8.150	8.240	7.420	7.870	7.660	6.120			Мn	6.12	9.56	8.03	8.01	9.25			1.9		Mn	15.1	13.0	14.2	15.3	15.6 19.E	14.1	16.1	15.6	15.1	15.4		Mn	13.0	16.1	14.9	15.2	15.9		
	Hg	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004			Hg	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004			0.00006		PH	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004		Hg	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004		
	Fe-F	106.000	81.000			H	-				94.600	84.500				Fe-F								0.3+++		Fo.F	194				157		$\vdash$	197	╈	+		Fe-F	┢	197			┥		
	Ľ.	3.3	1.8	9.6	5.3	6.0	1.5	2.1	8.4	0.8	1.6	1.6	1.3			u.	0.79	9.55	3.60	1.95	9.03			1.5+++		u	7.67	79.4	28.8	67.6	74.4	85.1	74.1	67.4	32.5 66.1	67.4		L.	28.80	85.10	66.29	69.50	82.72		
	Cu	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001			Cu	<0.001	<0.001	<0.001	<0.001	<0.001			0.005		ō	0.005	0.006	0.005	0.009	0.010	0.008	0.006	0.008	0.008	0.007		Cu	0.005	0.010	0.007	0.008	0.010		
	ŗ	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001			ŗ	<0.001	0.001	<0.001	<0.001	<0.001			0.005		č	0.006	0.004	0.006	0.008	0.007	0.007	0.007	0.010	0.008	0.009		ċ	<0.001	0.001	<0.001	<0.001	<0.001		
	Cd	<0.0001	<0.0001	_					<0.0001		<0.0001	0.0001				Cd	<0.0001	_	0.0001	_	0.0002			0.0015		PC	0.0018	0.0018	0.0018	0.0019	0.0020	0.0021	0.0020	0.0021	0.0023	0.0023		cq	0.0018	0.0023	0.0020	0.0021	0.0023		
	*8	3.030 <									3.440 <	2.940				å.		_	3.07	_	3.46		+	1.25		č		-	$\vdash$		13.0	+	$\vdash$	14.4	+	╈		* 0	+	15.5			┥		
	Be	DN				DN	_				Q	Q				Be	DN	QN	ND	QN	Q			0.1		Be	e e	Q	DN	QN	Q Q	2 9	DN	Q	9 9	2 9		Be	g	Q	Q	QN	QN		
	Ba	0.016	0.015	0.016	0.018	0.016	0.016	0.016	0.017	0.018	0.018	0.018	0.022		-	Ba	0.015	0.022	0.017	0.017	0.020			0.7+++		Ba	0.023	0.016	0.008	0.014	0.008	600.0	0.009	0.020	0.008	0.009		Ba	0.008	0.023	0.012	0.009	0.022		
	Ag	<0.001	$\vdash$		<0.001		<0.001		<0.001	<0.001		<0.001				Ag	<0.001	_		_	<0.001		+	0.00005		Δc	E		$\vdash$		<0.001			_	<0.001	+		Ag	-	╞	<0.001	$\square$	<0.001		
	As	0.051 <	Η			$\vdash$			> 0.059 >			0.051 <				As		_	0.055 <	_	0.063 <		+	0.024 0		Δs	~		┝	_	0.073		$\vdash$	-	0.077	+		As		┢	0.082	$\left  \right $	0.105 <		
	AI*	0.44 (							0.40 (			0.48 (				Al*		_	0.48 (	_	0.60 (			<u>5.25^/</u>		۵۴			$\vdash$		126 (			+	143 (	┢		Al*	-	145 (			144 (		
	ت ت	27.50 (							26.80 (		32.10 (	34.40				c			29.7	_	34.2		+	350+ 5		5			$\vdash$	_	15.7			21.5	+	+		c	-		-		30.3	_	
	SO4	1510 2							1280 20		1260 3.	1170 3.				SO4			1369 2	_	1558 3			1000++		so.			$\vdash$		2960 1			4250 2	+	+		SO4		4250 3			4149 3		
	TDS S	2430 1:							2100 1:			2010 1				TDS				_	2426 1:		+	1500^ 10		TDS				_	5790 2			+	5570 3	+		TDS S		5900 4		$\left  \right $	5900 4		
	Cond T us/cm) T					2780 23					2560 22					Cond T us/cm) T		2840 24		_	2840 24		+	2200 15		Cond T	us/cm) 56 5430 56		$\vdash$		5490 57			5550 55	+	┝		Cond T		5550 55			5546 59		
	pH Co	5.94 21							6.00 25		5.95 25	_				pH Co (μs/		_	5.97 25	_	_	5.94	+	6.5-8.0 22		о Н					3.49 54			4.00 55	+	+		pH Co		4.10 55		$\left  \right $	55	3.50	
Bore AP09		5.5	_											0000	Bore AP09		5	6.	5.:	5.:		+	4	_	Bore AP17						ei e	n r			+		Bore AP17		3.5	4	3.		e		
77. Groundwater Bore AP09	Sample Date	18/04/2018	17/05/2018	20/06/2018	18/07/2018	15/08/2018	19/09/2018	17/10/2018	21/11/2018	13/12/2018	16/01/2019	20/02/2019	14/03/2019	-	77. Groundwater Bore AP09	Sample Date	Minimum	Maximum	Mean	Median	95th Percentile	20th Percentile	SUTN Percentile	Surface Water WQGV	78. Groundwater Bore AP17	Sample Date	19/04/2018	18/05/2018	21/06/2018	19/07/2018	16/08/2018	19/10/2018	22/11/2018	13/12/2018	21/02/2019	14/03/2019	78. Groundwater Bore AP17	Sample Date	Minimum	Maximum	Mean	Median	95th Percentile	20th Percentile	

	zn*	3.540	3.540	4.200	3.740	3.760	1.860	2.760	4.640	4.160	3.330	4.730	4.710		Zn*	i	1.86	3.75	3.75	4.72			0.153		Zn*	0 100	0.087	0.128	0.123	0.128	0.038	0.053	0.060	0.049	0.048	c/n.n		Zn*	0.04	0.13	0.08	0.07	0.13		
	Se	0.0064	0.0073	0.0576	0.0058	0.0081	0.0044	0.0357	0.0669	0.0505	0.0206	0.0465	0.0598		aS		0.0044	0.0308	0.0282	0.0638			0.005		Se	~0000	<0.0002	0.0004	<0.0002	0.0002	<0.0002	<0.0002	<0.0002	<0.0002	<0.000	0.001		Se	<0.0002	0.0011	0.0006	0.0004	0.0010		
	٩d	0.004	0.004	0.002	0.004	0.004	0.003	0.002	0.002	0.003	0.003	0.002	0.002		Чd		0.002	0.003	0.003	0.004			0.005		Чd	0000	0.002	0.007	0.002	0.002	<0.001	<0.001	<0.001	<0.001	100.0>	0.010		РР	<0.001	0.010	0.004	0.002	0.009		
	N	2.430	2.400	1.900	2.470	2.440	1.260	1.090	1.700	1.860	1.780	2.180	2.060		ïz		1.09	1 96 1 96	1 98	2.46			0.05		ïz	0.071	0.067	0.069	0.078	0.071	0.036	0.034	0.036	0.030	0.030	0CN-N		ï	0.03	0.08	0.05	0.05	0.07		
	Мо	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	0.002	0.002	<0.001	<0.001	<0.001	<0.001		Mo		<0.001	0.002	-0.001	<0.001			0.01+		Mo	-0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	100.0>	700°0		Mo	<0.001	0.002	0.002	<0.001	<0.001		
	Mn	23.900	20.700	18.200	21.600	21.000	17.400	10.100	17.400	17.700	17.100	19.900	19.200		Mn		10.10 23 an	18.68	18.70	22.89			1.9		Mn	0.646	0.623	0.652	0.670	0.650	0.267	0.286	0.274	0.228	0.248	0.472		Mn	0.23	0.67	0.44	0.38	0.66		
	Hg	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004		면		<0.00004	-00000	-00000	<0.00004			0.00006		면	-0.0004	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	10000		Hg	<0.00004	<0.00004	<0.00004	<0.00004	<0.0004		
	Fe-F	43.400	44.600	27.000	46.600	39.700	21.000	9.510	20.700	29.300	42.200	33.400	23.400		Fe-F		9.51 46.60	31.73	31.35	45.72			0.3+++		Fe-F	0.648	0.589	0.556	0.269	0.638	0.018	0.065	0.025	0.029	0.026	0.077		Fe-F	0.01	0.88	0.31	0.17	0.78		
	Ľ	25.8	28.7	66.9	27.9	40.8	14.8	53.4	51.0	40.2	30.8	43.6	44.3		u		14.80 66 an	39.02	40.50	60.96			1.5+++		u	000	0.01	0.02	0.03	<0.050	<0.050	0.01	<0.020	<0.010	10.0	<0.010		Ľ	<0.010	0.05	0.02	0.01	0.05		
	Cu	0.005	0.004	0.065	0.005	0.005	0.012	0.054	0.087	0.056	0.039	0.057	0.064		G		0.004	0.038	0.047	0.077			0.005		Cu	-000	<0.001	0.004	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	100.0>	u.uu4		Cu	<0.001	0.004	0.004	<0.001	<0.001		
	ŗ	<0.001	<0.001	0.030	<0.001	<0.001	<0.001	0.030	0.048	0:030	0.013	0.032	0.035		č		<0.001	-0.01	-0.001	<0.001			0.005		c	<0.001	<0.001	0.004	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	100.0>	c.uu.u		ċ	<0.001	0.001	0.002	<0.001	<0.001		
	PO	0.0033	0.0031	0.0739	0.0039	0.0037	0.0036	0.0580	0.1080	0.0672	0.0342	0.0728	0.0795		Cd		0.0031	0.0426	0.0461	0.0955			0.0015		Cd	-0.0001	<0.0001	0.0001	<0.0001	<0.0001	<0.0001	<0.0001	0.0002	<0.0001	1000.0	0.000		B	0.0001	0.0002	0.0001	0.0001	0.0002		
	å,	12.200	12.400	19.300	12.200	12.000	6.280	13.400	19.400	17.800	13.700	18.700	18.600		ů		6.28 10.40	14.67	13.55	19,36			1.25		å	0.250	0.260	0.200	0.260	0.260	0.120 <0.05	<0.05	<0.05	<0.05	0.060	0.120		å	<0.05	0.26	0.19	0.23	0.26	-	
	Be	QN	QN	Q	DN	QN	QN	ND	DN	Q	DN	QN	QN		Be		2 2	2 9	2	2 2			0.1		Be	g	2 2	Q	Q	g 2		g	Q	g !		N		Be	g	Q	Q	QN	g		
	Ba	0.004	0.006	0.010	0.005	0.004	0.011	0.017	0.011	0.010	0.016	0.006	0.009		Ba		0.004	0.000	0.010	0.017			0.7+++		Ba	0.028	0.023	0.060	0.024	0.023	720.0	0.025	0.026	0.024	GZ0.0	0.000		Ba	0.023	0.060	0.031	0.025	0.060	-	
	Ag	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001		Ac		<0.001	-0.001	-0.001	<0.001			0.00005		Ad	-0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	100.0>	100.0>		Ag	<0.001	<0.001	<0.001	<0.001	<0.001		
	As	0.003	0.003	0.033	0.005	0.003	0.003	0.024	0.051	0.029	0.017	0.047	0.043		As		0.003	6600	0.021	0.049			0.024		As	-0.00	<0.001	0.002	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	100.0>			As	<0.001	0.002	0.002	0.002	0.002		
	AI*	38.30	39.60	265.00	43.70	40.30	21.20	210.00	381.00	247.00	137.00	281.00	295.00		AI*		21.20	166.5Q	173.50	343.16			5.25^^		AI*	121	0.19	3.22	0.26	0.29	0.16	0.11	0.13	0.11	0.16	02.1		Al*	0.11	3.22	0.58	0.18	2.67		
	Ū	39.80	38.20	25.30	36.00	_	35.90	_	26.70		26.10	28.30	27.70		5		17.4 30.8	30.9	+	39.1	┢		350+		C	38.30	39.10	38.70	30.00	37.30	zu.zu 13.30	18.00	17.60	12.20	19.70	00.12		ō	12.2	39.1	26.0	24.0	38.9		
	SO4	2460	2840	3850	2630	2830	2090	2700	4520	4020	2680	4320	4930		so,		2090	3323	2835	4750			1000++		soa	181	190	200	155	189	122	121	110	96	93	144		SO4	93	200	145	142	196		
	TDS	3970	2220	6400	3490	3980	2560	3940	7270	5490	4300	5840	6470		TDS		2220	4661	4140	6918			1500^		TDS	384	375	384	354	346	202	218	226	189	190	200		TDS	189	388	289	286	386		
	Cond (us/cm)	4470	4500	5570	4460	4480	3580	3810	4650	4970	4190	5520	5690		Cond	(ms/cm)	3580	4658	┼	5637			2200		Cond	(μs/cm) 640	680	670	680	670	339	330	318	293	GU5	421		Cond ()	293	680	477	397	680		
	, Hq	$\vdash$	3.07	3.33	3.12	3.06	3.22	3.54	3.37	3.25	3.18	3.20	3.25		На		3.01	2 00 E	3.21		3.08	3.31	6.5-8.0	M1/D2	На	3 46	3.46	3.45	3.49	3.43	4.30	4.37	4.50	4.75	4.51	04.4	M1/D2	⊢	+	4.75	4.05	4.36		3.46	
94. KVAD Seepage	Sample Date	19/04/2018	17/05/2018	20/06/2018	18/07/2018	15/08/2018	19/09/2018	17/10/2018	21/11/2018	13/12/2018	16/01/2019	20/02/2019	14/03/2019	94. KVAD Seenade	Sample Date		Maximum	Mean	Median	95th Percentile	20th Percentile		۶V ک	33. Groundwater Bore WGM1/D2	Sample Date	19/04/2018	18/05/2018	21/06/2018	19/07/2018	16/08/2018	17/10/2018	22/11/2018	13/12/2018	17/01/2019	21/02/2019	8102/00/01	33. Groundwater Bore WGM1/D2	Sample Date	Minimum	Maximum	Mean	Median	95th Percentile	20th Percentile	

	Zn*	0.685	0.493	4.530	3.540	3.880	2.610	1.430	0.719	0.538	0.419	0.506	0.283			Zn*	0.28	4.53	1.64	0.70	4.24			0.153		Zn*	0.032	0.027	0.030	0.038	0.024	0.032	0.036	0.036	0.034	0.034	+00.0		Zn*	0.02	0.04	0.03	0.03	0.04		
	Se	0.0007	0.0002	0.0152	0.0138	0.0250	0.0085	0.0021	0.0009	0.0005	0.0005	0.0004	0.0004			Se	0.0002	0.0250	0.0057	0.0008	0.0207			0.005		Se	<0.0002	<0.0002	<0.0002	<0.0002	<0.0002	<0.0002	<0.0002	<0.0002	<0.0002	2000.02	2000.02		Se	<0.0002	<0.0002	<0.0002	<0.0002	<0.0002		
	Pb	0.003	0.001	0.011	0.012	0.015	0.010	0.007	0.003	0.002	0.002	0.002	<0.001			Pb	<0.001	0.015	0.006	0.003	0.014			0.005		Pb	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	-0.001	20,001		Pb	<0.001	<0.001	<0.001	<0.001	<0.001		
	ïz	0.729	0.555	4.630	3.360	3.330	2.310	1.300	0.734	0.494	0.398	0.470	0.329			ïz	0.33	4.63	1.55	0.73	4.07			0.05		ïz	0.026	0.026	0.026	0.032	0.026	0.028	0.028	0.028	0.027	020.0	120.0		ïN	0.03	0.03	0.03	0.03	0.03		
	Mo	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	0.002	<0.001			Mo	<0.001	0.002	0.002	0.002	0.002			0.01+		Mo	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	100.02	100.02		Mo	<0.001	<0.001	<0.001	<0.001	<0.001		
	Mn	2.020	2.040	14.000	11.200	13.300	8.180	4.240	3.670	1.640	1.290	1.710	1.810		Ī	ЧN	1.29	14.00	5.43	2.86	13.69			1.9		Mn	13.300	11.200	12.200	12.800	13.600	11.800	13.400	11.500	11.700	002.21	12.000		Mn	11.20	13.80	12.51	12.40	13.71		
	Hg	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004			Hg	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004			0.00006		Hg	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004	<0.000.04	<0.00004		Hg	<0.00004	<0.00004	<0.00004	<0.00004	<0.00004		
	Fe-F	0.488	8.830	48.600	45.600	48.200	3.150	1.730	25.200	0.287	0.283	0.639	18.500		Ī	Fe-F	0.28	48.60	16.79	5.99	48.42			0.3+++		Fe-F	46.8	34.1	47.8	47.9	49./ F0.4	27.3	52.7	33.4	51.4	40./	7 17		Fe-F	21.2	52.7	42.4	47.3	52.1		
	u.	9.0	0.5	<0.010	12.3	15.9	7.8	3.8	1.2	0.9	0.5	0.7	0.6			u.	<0.010	15.90	4.06	0.94	14.46			1.5+++		u.	0.04	0.02	0.10	0.47	<0.100	0.05	0.06	<0.100	<0.100	<0.100	<0.100		u	<0.100	0.47	0.11	0.05	0.38		
	Cu	0.005	<0.001	0.019	0.036	0.017	0.009	0.012	0.008	0.018	0.014	0.012	0.002			Cu	0.002	0.036	0.014	0.012	0.029			0.005		Cu	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	-0.001	SU-UUI		Cu	<0.001	<0.001	<0.001	<0.001	<0.001		
	ŗ	<0.001	<0.001	0.002	0.002	0.004	0.002	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001		Ī	ŗ	<0.001	0.001	<0.001	<0.001	<0.001			0.005		ŗ	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	100.02	SUJUL		ŗ	<0.001	0.001	<0.001	<0.001	<0.001		
	Cd	0.0044	0.0032	0.0355	0.0299	0.0282	0.0255	0.0211	0.0083	0.0096	0.0047	0.0038	0.0014		Ī	Cd	0.0014	0.0355	0.0146	0.0090	0.0330			0.0015		Cd	<0.0001	<0.0001	<0.0001	<0.0001	<0.0001	<0.0001	<0.0001	<0.0001	<0.0001	-0.001	1000.05		Cd	<0.0001	<0.0001	<0.0001	<0.0001	<0.0001		
	å	0.730	0.640	8.310	9.010	10.500	6.400	3.750	1.910	1.440	0.940	1.030	0.890		Ī	å	0.64	10.50	3.80	1.68	9.84			1.25		å	1.690	1.680	1.630	1.900	1.520	1.560	1.610	1.600	1.630	1.790	067.1		å	1.52	1.90	1.66	1.63	1.83		
	Be	Q	DN	QN	Q	Q	g	Q	Q	Q	Q	Q	Q			Be	Q	ΠN	ND	QN	QN			0.1		Be	QN	QN	QN	Q.	2 2	2 2	QN	QN	9		2		Be	g	Q	g	Q	QN		
	Ba	0.037	0.055	0.060	0:050	0.045	0.036	0.044	0.027	0.025	0.023	0.022	0.018			Ba	0.018	0.060	0.037	0.037	0.058			0.7+++		Ba	0.014	0.014	0.014	0.017	0.015	0.017	0.016	0.020	0.017	0.010	0.010		Ba	0.014	0.020	0.016	0.016	0.019		
	Ag	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001		Ī	Ag	<0.001	<0.001	<0.001	<0.001	<0.001			0.00005		Ag	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	100.02			Ag	<0.001	<0.001	<0.001	<0.001	<0.001		
	As	0.002	<0.001	0.006	0.012	0.014	0.008	0.002	0.001	0.001	<0.001	0.002	<0.001		Ī	As	<0.001	0.014	0.005	0.002	0.013			0.024		As	0.002	<0.001	0.002	0.002	0.002	<0.001	0.002	0.002	0.002	200.0	20,001		As	<0.001	0.002	0.002	0.002	0.002		
	AI*	1.04	0.53	75.50	97.30	129.00	51.90	18.80	6.39	3.51	2.32	2.80	1.38		Ī	Al	0.53	129.00	32.54	4.95	115.05			5.25^^		AI*	0.03	<0.01	0.02	0.02	0.02	0.01	0.01	0.01	<0.01	10.02	- AUAI		Al*	<0.01	0.03	0.02	0.02	0.03		
	ū	14.40	27.70	25.60	23.60	22.70	15.00	13.20	24.40	11.80	10.30	12.60	36.10			Ū	10.3	36.1	19.8	18.9	32.4			350+		ū	25.50	26.20	31.20	27.10	24.10	36.30	25.50	46.90	33.60	00.42	23.00		ū	23.6	46.9	29.4	26.7	42.2		
	SO4	321	468	2740	2800	3440	1540	839	749	331	260	293	532			SO4	260	3440	1193	641	3158			1000++		SO4	698	727	895	867	73.4	802	660	960	757	077	000		SO4	660	960	763	731	931		
	TDS	490	682	4130	3270	4840	1970	1200	1130	434	385	454	859			TDS	385	4840	1654	995	4528			<u>1500^</u>		TDS	1100	1080	1060	1060	1130	1230	1140	1260	1250	1030	0//		TDS	778	1260	1112	1115	1256		
	Cond (us/cm)	730	1010	4050	3810	4310	2420	1580	1490	730	630	069	1120			Cond (µs/cm)	630	4310	1881	1305	4196			2200		Cond (us/cm)	1510	1530	1490	1510	1510	1670	1500	1890	1620	1400	0641		Cond	1490	1890	1564	1510	1793		
VGM1/D3	Hq	4.67	5.28	4.17	4.17	3.98	3.99	4.08	4.56	4.31	4.38	4.36	4.92	CON11 DO		Hd	3.98	5.28	4.41	4.34		4.10	4.65	6.5-8.0	VGM1/D4	Hq	6.18	6.17	6.20	6.23	6.21 6.17	6.17	6.17	6.10	6.13	0.10	0.10	VGM1/D4	Hq	6.10	6.23	6.17	6.17		6.14	
34. Groundwater Bore WGM1/D3	Sample Date	19/04/2018	18/05/2018	21/06/2018	19/07/2018	16/08/2018	20/09/2018	19/10/2018	22/11/2018	13/12/2018	17/01/2019	21/02/2019	14/03/2019	Contraductor Board	34. Groundwater bore WGM 1/U3	Sample Date	Minimum	Maximum	Mean	Median	95th Percentile	20th Percentile	80th Percentile	Surface Water WQGV	35. Groundwater Bore WGM1/D4	Sample Date	19/04/2018	17/05/2018	20/06/2018	18/07/2018	15/08/2018 19/09/2018	17/10/2018	21/11/2018	13/12/2018	16/01/2019	14/02/2010	6102/00/41	35. Groundwater Bore WGM1/D4	Sample Date	Minimum	Maximum	Mean	Median	95th Percentile	20th Percentile	

Appendix D D1 – D6 Borehole Logs

INCLINATION: 90 AZIMUTH: ISG CD-ORDINATES: 217828E COLLAR R.L.: 947.8 SHEET 1 OF 1 LOCATION PLAN NO. DE202722C DE300 CONTRACTOR GALAGE DE300 CONTRACTOR CONTRACTOR CONTRACTOR DE300 CONTRACTOR CONTRACTOR CONTRACTOR DE300 CONTRACTOR CONTRACTOR CONTRACTOR DE300 CONTRACTOR CONTRACTOR DE300 CONTRACTOR CONTRACTOR CONTRACTOR DE300 CONTRACTOR CONTRACTOR CONTRACTOR DE300 CONTRACTOR CONTRACTOR CONTRACTOR DE300 CONTRACTOR CONTRACTOR DE	ELE	CTRICITY COM OF N.S.W. geotechnical L	· ·		LLERAWANG P.S WATER MONITORING	W.GM1/D 1
TARGENESS:         DEPT IN         Solution         PAULYS:         CAUSAGE         Solution		0-00			£ .	LOCATION PLAN NO. DE202722C
1         1           1         1           1         1           1         1           1         1           2         1           3         1           3         1           3         1           3         1           3         1           3         1           3         1           3         1           3         1           3         1		ROCK TYPE, COLOUR. GRAIN MINERAL COMPOSITION, TE HARDNESS. R.L.	E 00 ON LUI SIZE. 1H LUI XIURE. HAVE DEPTH	X CORE LOSS       REDUCED LEVEL       AND METHOD       DEPTH (METRES)       DEPTH (METRES)	ESTIMATED L M H VH POINT LOAD MPA POINT LOAD MPA POINT LOAD POINT LOAD MPA POINT LOAD POINT LOAD MPA POINT LOAD POINT LOAD MPA POINT LOAD POINT LO	SAMPTEST SAMPTEST
		SAND. MOTTLED GREY-DRANGE MEDIUM SAND. WITH PEBBLES IN. MINOR GLAY BINDE 946.3SLIGHILY MOISI (IS.F NON CORE DRILLING. 945.3 GLAYEY SAND. MOTTLED GREY MEDIUM SAND. WITH PEBBLES IN. MOISI. (2S.F) 945.3 NON CORE DRILLING. 944.8 SAND. MOTTLED ORANGE-BROU WITH PEBBLES TO 10MM. MIT CLAY BINDER. SLIGHIL 944.3MOISI. (3S.F) NON CORE DRILLING. 943.8 CLAYEY SAND. LIGHT GREY. PEBBLES TO 10MM. MOISI. F COARSE GRAINED. (4S. 943.8 CLAYEY SAND. LIGHT GREY. PEBBLES TO 10MM. MOISI. (4S. 943.8 CLAYEY SAND. LIGHT GREY. PEBBLES TO 10MM. MOISI. (4S. 943.8 CLAYEY SAND. LIGHT GREY. PEBBLES TO 10MM. MOISI. (4S. 943.8 CLAYEY SAND. WITH PEBBLES TO SANG WITH PEBBLES TO SANG F DRILLING. 942.8 CLAYEY SAND. WITH PEBBLES TO SANG FINES OF MEDIUM TO 942.8 CLAYEY SAND. MOITLED ORAN FINES OF MEDIUM TO 941.8 CLAYEY SAND. MOITLED ORAN FINE SAND. WITH PEBBLES MOISI. (6S.F). 941.3 NON CORE DRILLING. 940.8 940.6 SAND. TO WEI. MOISI. DATLED OR AND THE SAND. WITH PEBBLES MOISI. (6S.F). 941.3 NON CORE DRILLING. 940.8 940.8 940.8 940.8 938.8	1.00 TO 5 R TO 5 . 1.45 2.00 -ORANGE / TO 5 / 2.45 / 2.45 / 3.00  3.45 4.00  4.00  5.00  5.00  5.00  5.00  5.00  5.00  5.00  5.00  5.00  5.00  5.00  5.00  5.00  5.00  6.00  5.45 / 6.45 / 5.45 / 6.45 / 6.45 / 7.00 0. 7.15 / 8.4E. 9.00	VID 4 5 5 6 9 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	7.30 V-BIT REFUSAL	
COMPLETED: 29/10/85 DRILLER: J.SHAW LOGGED BY: G WILSON CHECKED BY:			DRILLER*	J.SHAW	LOGGED BY: G WILSON	CHECKED BY:

and a second second

ELECTRICITY OF N. Geotechni	S.W.		LLERAWANG P.S WATER MONITORING	W .GM1/D
INCLINATION: 90 AZIMUTH:	ISG CO-ORDINATES:	215588E 1303352Ň	COLLAR R.L.: 919.9 DATUM: AHD	SHEET 1 O LOCATION PLA
DESCRIPTION	DF CORE	LIFT AND CORE LOSS UCED LEV UCED LEV UC	STRENGTH STIMATED L M H VH OINT LOAD MPA PC Q Q Q FAULTS. CRUSHED Z	SHOOTHHESS.
NON CORE DRILLING.		e.	1.00 - 1.45 SILTY TO S CLAY, MOITLED GREY DRANG CW MUDSTONE? (15.F)	
		2 - 2	2.00 - 2.45 DRANGE CLA TO CLAY, MOIST (2S.F), 3.00 - 3.45 DRANGE-GRE	
		4	4.00 ~ 4.45 GREY CLAY. CLAYSTONE?.SOFT. MOIST	CV CV
SUBE LOSS.	5+60	315 211 211 211 211 211	S.00 - S.25 MIXED SAMP GRAINED SLIGHTLY CLAYE WEAKLY BOUND. PLUS PUR CW MUDSTONE (SS.F).	
913.4 SOAL BLACK. CATSTONE, MOTTLE	6-48	6.	5.80 - 7.01 DUMINANT J DEG.MINDR IRONSTAINING 6.31 INTERSECTING IRON JOINTS AT 15 AND 80 DE	
912-9 COALY SILTSTONE.	7.01		7.01 ~ 8.28 CLEAT AT O DEG. PART FRAGMENTED B	N-80 AND 90
911.6 CARBONACEDUS SAND GREY-BROWN' WITH GRADES TO SILTSTOJ 911.0 SANDSTDNE INTERBE MUDSTDNE (SOX). M BROWN, BEDDING <6 BROWN, BEDDING <6	8.85		8.28 - 9.56 CDRE PIECE	:S 10 TO
SANDSTONE INTERBE MUDSIDNE (SOX) - 6 BROWN - BEDDING (S CARBDMACEDUS MUDS LESSEN TO TOP.	DTTLED GREY-		9.56 - 10.43 WEATHERED O DEG	) JOINTS AT

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GEOTECHNICAL LOG			(	GROUND WATER MONITORING					M1/D	
INCLINATIC AZIMUTH:	DN: 90 ISG CO-ORDIN	ATES:				COLL DATU	AR R.L.: 919.9 M: AHD	LOCATI	T 2 OF ON PL'AN 2027	IN 27
BUSH ROCK TI	ESCRIPTION OF CORE YPE, COLDUR, GRAIN SIZE, L COMPOSITION, TEXTURE, HARDNESS.	RAPHI	X CORE LOSS REDUCED LEVEL	AND METHOD	CASING	STRENGTH STIMATEI L M H VI OINT LOA MPA	D STRUCTURES	AMS,	0.015 UNIT DRILL WATER DRILL WATER DRILL WATER WATER LEVEL	SAMPLE NUMBER
909.3	E. LIGHT BROWN. FINE 10.5 ANDSTDNE, LIGHT GREY, BLES TO 30MM. INCLUDES GRAINED BANDS.				——————————————————————————————————————		B.56 - 10.43 WEATHERED AT 0 DEG 10.43 - 15.35 CORE PIECE 600NM	JOINTS		
903-1	ACK. 15.6 INTERBEDDED WITH E 15027, MOTTLED GREY- ITH PEBBLES TO SMM. <6NM. ISOLATED E BANDS INCLUDED 16.7 GLOMERATE. 16.2 GLOMERATE. 16.2		6	-16	• • • • • • •		15.35 - 15.62 CLEAT AT DEG 15.62 - 16.90 CDRE PIEC 270MM 16.00 - 18.03 CLEAT AT DEG 17.22 - 17.50 FRAGMENTE DRILLING	ES 50 TO		
9.109	18,0	<u>5</u>		EN		F HOL	E			

	CTRICITY OF N. GEDTECHNI	S.W.		G					VANG P.S R MONITORING	W .C	GM1/	1D	
INCL I AZIMU	INATION: 90 JTH:	ISG CO-ORDINA		130	370	\$			R R.L.: 930.0 : AHD	LOCAT	ET 1 ION P 202 <sup>-</sup>	PLAN 7고	
FR DEGREE SW OF NM OF CW NEATHERING CW		UR. GRAIN SIZE. TION. TEXTURE. ESS. DEPTH	GRAPHIC LOG	LIFT AND X CORE LOSS REDUCED LEVEL AND METHOD	DEPTH (METRES)	CASTNG 1 1 1 1 1 1 1 1 1 1 1 1 1	STRENG STIMAT L N H OINT L MPA	TED VH .OAD	STRUCTURES JOINTS (SPACING, ATTITUDE, SMO APERTURE, COATING, INFILLIN BEDDING, VEINS, SEA FAULTS, CRUSHED ZONS	OTHKESS. SP.	ACTURE ACTING ACTING ACTING IO.0	LOSS WATER LEVEL	SAMPLE NUMBER
	NON CORE DRILLING		9	aliev - v					1.00 - 1.45 BROWN TO ORAN BROWN CLAYEY SAND/SILTY SAND.MOIST (15.F). 2.00 - 2.45 LIGHT GREY-BF SAND. FINE GRAINED (25.F) 3.00 - 3.45 BLACK CARBON/ MUDSTONE AND COAL. CW TD (35.F).	ROWN			
	CORE LDSS. 925.9 MUDSTONE INTERBED SANDSTONE (SO2). GREY. BEDDING <6M 925.4 SANDSTONE INTERBE MUDSTONE (S2). DEVELOPMENT 5.23-1 924.7 MUDSTONE INTERBED 924.4 SANDSTONE INTERBED 924.4 SANDSTONE INTERBED 924.6 SANDSTONE INTERBED 924.0 SANDSTONE INTERBED 924.0 SANDSTONE INTERBED	4-65 DDED WITH OTTLED GREY- SENN- IRONSIDNE S-34- S-34- DDED WITH SO(2) - S-64 DDED WITH		0 97 97	5				4.15 ~ 6.54 JUINTS AND C BREAKS ON BEDDING AT O TI	JRE J 5 DEG		<u>.</u>	
	MUDSTÖNE INTERBED SANDSTONE (152) BEDDING <6MM - SAN FINE GRAINED, 910 922.5 SAUDSTONE, GREY. MUDSTONE, GREY.	DED WITH MOTITED GREY. NOSIONE IS VERY OTURBATED 7.52 7.69			5				6.54 ~ 6.94 IRONSTAINED JOINT AT 85 TO 90 DEG 6.94 ~ 8.06 JOINTS AND F AT 0 TO 5 DEG			<u>, , , , , , , , , , , , , , , , , , , </u>	
	921.9 COAL. BLACK. 921.5 MUDSTONE. GREY. C BASE. 921.0 921.0 921.0 920.4 MUDSTONE. GREY. 1 CLAYSTONE LAMINAE 920.4 920.2 MUDSTONE. GREY. C 920.2 MUDSTONE. GREY. C	9-02 BROWN 9-19 INCLUDES FEW E- 9-63 - 9.79 CARBONACEOUS AT 10.00		920	9				8.06 - 8.48 BROKEN DN CL AND 85 TO 90 DEG 8.90 ~ 8.95 SMOOTH JOINT DEG 9.95 - 17.45 JOINTS AND FRACTURES AT 0 TO 5 DEG			L	
COMME	MUDSTONE. GREY. C 920-011.27-11-49. ENCED: 29/10. LETED: 30/10.	/85 CONTR	RACTOR			<u>  </u> )TT			TYPE: PIO 160 D BY: G WILSON			<u> </u>	_

ELE	CTRICITY OF N GEOTECHNI	S.W.	SION	G		ALLERA VATE		P.S TORING	W	- GN	11 /	D	
INCL AZIM	INATION: 90 UTH:	ISG CO-ORDIN	ATES:			COLLA DATUM		.: 930.( AHD	LO	HEET CATIC	N PL		ר פ
ST FR DEGREE SW DEGREE HW VEATHERING		R. GRAIN SIZE. 10N. TEXTURE. SS. DEPTH	CRAPHIC LOG	X CORE LOSS REDUCED LEVEL AND METHOD	DEPTH (METRES) CASING	STRENGTH ESTIMATED L M H VH POINT LOAD MPA	BEDD FAUL	STRUCTURES SPACING. ATITIDOS. URE. COATING. INFI ING. VEINS. S IS. CRUSHED 3 7.45 JOINTS A AT 0 T0 5 DE	EAMS, ZONES	-0:50 -0:50	REG 10.0	WATER LEVEL	SAMPLE NUMBER
	917.4 SANDSTONE, LIGHT G DOMINANT GRAIN SIZ INCLUDES FEW FINE LAMINAE. 913.7 SANDSTONE INTERBEL MUDSTONE (302), H BROWN, DOMINANT GR BROWN, DOMINANT GR DOG-0.2MM. BEDDIN TRANSITIONAL BAND.	12.60 REY-BROWNI E 0.06-0.2MM. MUDSTONE		915									
	912-9 MUDSTONE INTERBED SANDSTONE (30 912-5REDDING <8MM	17-15 ED WITH 22) - 17-45			END	DF HOLE							

GEC NCLINATIO ZIMUTH: ZIMUTH: BUE ROCKT MINERA EGETOR-L NON CORE		DG ISG RDINATES: stze.	x CORE LOSS REDUCED LEVEL AND METHOD	SO87E 4304N	COLLA	STRUCTURES JOINTS (SPACING, ATTITUDE, SU APERTURE, COATING, INFILL BEDDING, VEINS, SEE	MS.
904.7 CLAY. BF MINOR OF 904.2 NON CORE 903.7 CLAYEY S MOIST 7 903.2 NON CORE 902.7 SAND. L COARSE C 902.2F	E DRILLING. IGHT GREY, WET, FII GRAINED, ROCK FRAG	2.00 SAND / / / / 2.45 3.00 5 (38 // 3.45 / /	sóo ← RR × AUGV só5	2 3 4 5 6 7 7		4.60 V-BIT REFUSAL	
COMMENCED : COMPLETED :		CONTRACTOR: DRILLER:	MCDI J.SI	HAW	_	TYPE: PIO 160 ED BY: G WILSON	CHECKED BY

FIF	CTRICITY	COMMISS	Г <u></u> ЛN		 1./		AWANG P.S			
	OF N.	S.W.					R MONITORING	W	GM1	/D
INCLI AZIMU	INATION: 90 JTH:	ISG CO-ORDINA	TES:		,	E COLL. N DATU	AR R.L.: 904. M: AHD	' LOC	HEET 1 CATION	PLAN
FR DEGREE SV DEGREE SV DF HW WEATHERING CW	DESCRIPTIO ROCK TYPE, COLO MINERAL COMPOSI HARDNI R.L.	JR. GRAIN SIZE, TION, TEXTURE.	GRAPHIC LOG LIFT AND	Z CORE LOSS REDUCED LEVEL	DEPTH (METRES) CASING	STRENGTH ESTIMATED L M H VH POINT LOAN MPA	D STRUCTURES D JOINTS GRACING. ATTITUD APERTURE. COATING. IN BEDDING. VEINS.	S. SHOOTHNESS. FILLINO SEAMS.	FRACTURE SPACING (M)	1 17
	NON CORE DRILLING	3.60	ð				1.00 - 1.45 BROWN CL, MINOR ORGANIC CONTEN 2.00 - 2.45 ORANGE C SAND.MDIST. SAND IS GRAINED.CW SANDSTONE 3.00 - 3.45 COAL.BLA HW. WET (35.F)	AYEY DARSE ?. (2S.F).		
	900.4CORE LOSS. SANDSTONE INTERDE MUDSTONE (202) BROWN. BEDDING <6 GRAINED. TRONSTAI 3.72-3.83. SANDSTONE. LIGHT GRAINED, GRADES TO BELOW 8.4M.	5-05		900			3.72 - 10-31 JULNIS BREAKS AT O TO 5 DE PIECES 10 TO 550MM	ND-DRILLIN		
	894-1	10-00		895	× 7					

NCLINATION: 90 ISG CO-ORDINATES: ZIMUTH: DESCRIPTION OF CORE RICK TYPE. COLOUR. GRAIN SIZE. HARONESS. DESCRIPTION OF CORE STRENOTH RICK TYPE. COLOUR. GRAIN SIZE. HARONESS. DEPTH SANDSTONE. LICHT GREY. COARSE SANDSTONE. LICHT GREY. COARSE SANDSTONE. LICHT GREY. COARSE SANDSTONE INTERDEDDED WITH WUSSTONE SOUTHED BELOW, B.4H10.31 COAL. BLACK. STRENCT INFIDURES STRENCT INFIDURES STRENCT INFIDURES SANDSTONE INTERDEDDED WITH WUSSTONE SOUTHED GREY. COAL. BLACK. STRENCT INFIDURES STRENCT INFIDURES STREN
Image: Second control of the second contrel of the second
SANDSTONE. LIGHT GREY. COARSE GRAINED.GRADES TO 893.8CORGLOMERATE BELOW 8.4M10.31 COAL. BLACK.
891.6     12.49       SANDSTONE INTERBEDDED WITH MUDSTONE (SOX). MOTHED GREY- BROWN. BEDDING <6MM. FINE COALY LAMINAE INCLUDED AT 12.49-12.56.     12.49 - 14.30 CORE PIECES TO       890.1     13.95       SANDSTONE. LIGHT ORANGE. IRON STATINING WELL-SPREAD.     0       90.1     13.95       12.49     14.30

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ELECTRICITY OF N. GEOTECHNI	S.W.		LLERAWANG P.S WATER MONITORING W.GM1/D 6
INCLINATION: 90 AZIMUTH:	ISG CO-ORDINATES:	215332E 1303997N้	DE 201722
DESCRIPTION	N OF CORE	CORE LOSS CORE LOSS UCED LEVE D METHOD HETHOD HATRE CASING CASING	STRENGTH STINATED L M H VH JOINTS GEACING, ATTITUDE, SHOOTHWESS, MPA BEDDING, COATING, INFILLING BEDDING, COATING, INFILLING PAULTS, CRUSHED ZONES COACTING, COATING, INFILLING COACTING, INF
964-1	3-45	ABUN SUB	1.00 - 1.45 MIXED SAMPLE, LIGHT DRANGE-RED SOFT CLAY AND DARK GREY TO BLACK CU-HW CARBONACEOUS MUDSTONE (1S.F) 2.00 - 2.45 BLACK COAL.CW TO HW.SOFT (2S.F). 2.11 7
MUDSTONE LISS MUDSTONE INTERBED SANDSTONE (202). <6MM. 902.8 SANDSTONE, LIGHT INCLUBES MUDSTONE 4.0-4.17M.COARSE	DED WITH GREY. BEDDING 	5	2-50 - 3-25 JUINIS AT 0 DEG 3.25 - 3.53 THREE JOINTS AT 40 DEG 3.53 - 3.63 JOINTS AT 35 AND 50 DEG 4.08 - 4.16 ROUGH JOINT AT 50 DEG 4.16 IRONSTAINED JOINT AT 90 DEG 4.16 IRONSTAINED JOINT AT 90 DEG 1300MM
SANDSTONE, MOTILE SANDSTONE, MOTILE WITH PEBBLES TO 4 STAINING WELL-SPR GRAINED.	4.75 D GREY-ORANGET OMM- IRON EAD- COARSE	900 2	
897.8 COAL, BLACK-SILI INCLUDED AT 8-86- 896.6	10-00		B-80 - 11.00 CLEAT AT 0.70 TO 90
COMMENCED: 06/11. COMPLETED: 07/11.		MCDERMOTT J.SHAW	DRILL TYPE: PIO 160 LOGGED BY: G WILSON CHECKED BY:

ELE	CTRICITY OF N. Geotechni				AWANG P.: R MONITO	-	W.G	M1/D	6
INCLI AZIMU	NATION: 90 Th:	ISG CO-ORDINATES	S =	32E COLL 97N DATU	AR R.L.: M:	906.6 AHD	LOCATI	T 2 0 ON PLA 2027	N NO.
FR DEGREE FS DEGREE SW OF HW WEATHERING CW	DESCRIPTION ROCK TYPE, COLOU MINERAL COMPOSI HARDNE R.L.	R. GRAIN SIZE, SI TION. TEXTURE, AV SS. 22	LIFT AND % CORE LOSS REDUCED LEVEL AND METHOD		D SI H JOINTS CEPACT APERTURE. BEDDING	IRUCTURES ING. ATTITUDE. SHO COATING. INFILLIN VEINS. SEAN CRUSHED ZONE	() (C	TURE SSOT	SAMPLE NUMBER AND SPT. WATER PRESSURE TEST (LUGEONS)
	R-L. COAL. BLACK. SILTO INCLUDED AT 8.86- MUDSTONE INTERBEDI SANDSTONE INTERBEDI SANDSTONE INCREASE BEDDING < CARBONACEOUS AT 11 SANDSTONE INCREASE 894.0 SANDSTONE. LIGHT ( PEBBLES TO 10MM. ( 891.7	DEPTH 11-00 DED WITH 10TTLED GREY- .00- 11.10M, S TO BASE. 	892	4- ND OF HOL	B.80 - 11.0 90 DEG 11.00 - 12.0 CONTROLLED B DEG 12.00 - 12.7 DEG 12.75 - 14.9 750MM	D WEATHERING Y JOINTS AT C	70 T0 0 T0 10 5 AT 50		S N
	NCED: 06/11/	/85 CONTRACTO			L TYPE: F	210 160			
ICUMMES						10 100			

### Document prepared by

### Aurecon Australasia Pty Ltd

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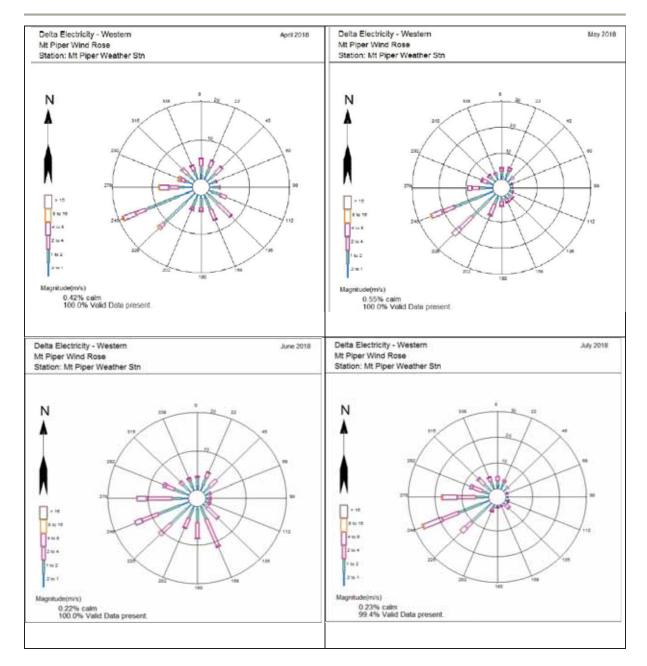
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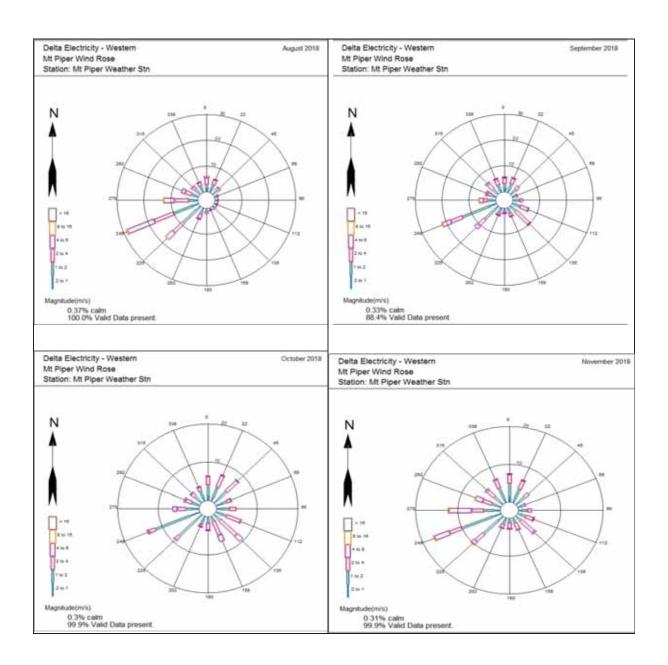


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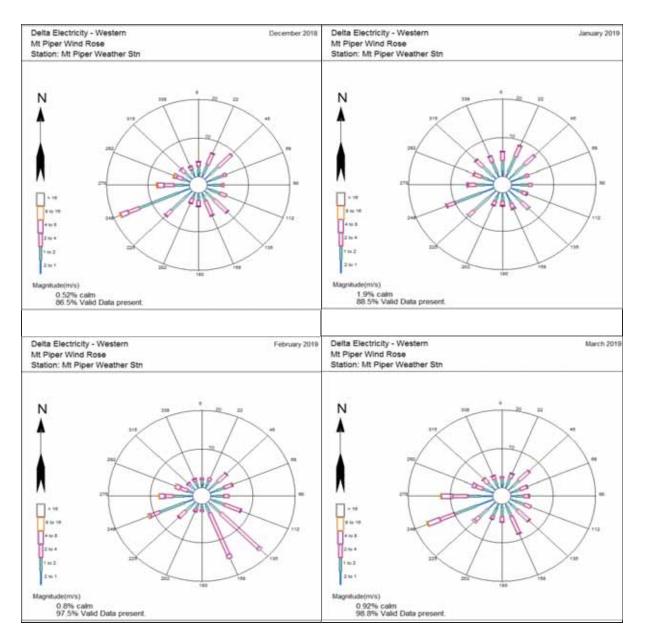
#### Aurecon offices are located in: Angola, Australia, Botswana, China, Ghana, Hong Kong, Indonesia, Keny Mozambique, Namibia, New Zealand, Nigeria, Philippines, Qatar, Rwa South Africa, Swaziland, Tanzania, Thailand, Uganda, United Arab

# Appendix E EnergyAustralia NSW Windrose April 2018- March 2019





2018 - 2019



# Appendix F EnergyAustralia NSW Community Sponsorships and Donations:2018-19

Recipient	Reason	Month/Year
Anzac Day Ceremony Wallerawang	Wreath	May 2018
See Bees	Event Lake Lyell	May 2018
Red Cross Calling	Matching staff donation	June 2018
Lithgow Bears	Improvements to Bears Dressing Shed	July 2018
Wallerawang/Lidsdale Progress	Pyrotechnic Display New Years Eve 2018 Lake Wallace	July 2018
Central Tablelands Mountains Bike Club	Prize Money for NSW State Downhill Event	July 2018
Biggest Morning Tea	Matching staff donation	July 2018
Capertee Public School	Assist with Sensory Garden	August 2018
Mingaan Corporation	Replace office equipment	August 2018
Daffodils at Rydal	Event	August 2018
Dry July	Matching staff donation	August 2018
Jeans for Genes	Matching staff donation	August 2018
La Salle Academy Lithgow	Presentation Day	September 2018
Lithgow High School	Presentation Day	September 2018
Mobile Community Pantry Fresh Food Sunday	Assist purchase equipment/shelving	September 2018
Cullen Bullen Tidy Town	Seal road Invicible Heritage Skip Line Display	September 2018
Lithgow City Council	Halloween	October 2018
Mingaan Aboriginal Corporation	Support local event	October 2018
Rydal Show Society	Rydal Show	November 2018
St Josephs School Portland	Presentation Day	November 2018
Legacy	Matching staff donation	November 2018
Barton Park Giant Tree Arboretum	Projects at the Arboretum – Lake Wallace	December 2018
Lithgow & District Community Nursery	Assitance with propagation/provision of plants for local environment	December 2018
Lithgow Oberon Landcare	Local Environmental Projects	December 2018
Lithgow Show Society	Lithgow Show	December 2018
Capertee Public School	Presentation Day	December 2018
Cooerwull Public School	Presentation Day	December 2018
Cullen Bullen Public School	Presentation Day	December 2018
Hampton Public School	Presentation Day	December 2018

Lithgow Public School	Presentation Day	December 2018
Meadow Flat Public School	Presentation Day	December 2018
Portland Central School	Presentation Day	December 2018
St Patricks School	Presentation Day	December 2018
Wallerawang Public School	Presentation Day	December 2018
Zig Zag Public School	Presentation Day	December 2018
Rydal Show Society Youth Council	Purchase PA System	December 2018
Beehive Re-Creative Centre	Replace Chairs	December 2018
Lithgow High	Mandiyaba Yadhaa project	December 2018
Wallerawang/Lidsdale Progress Assn	Lake Wallace BBQ Cover & Avenue of Trees	December 2018
Lithgow Small Arms Factory	Museum projects	December 2018
Lithgow Tidy Towns	Distortion Mirrors Project	December 2018
Science at the Local	Promote science	December 2018
WallerawangCentralAcclimatisation Society	Gone Fishing Day	December 2018
Rangers Soccer Club	Geotech Report	December 2018
Lithgow Swimming Club	Twilight Swim Meet	December 2018
Portland Art Show	Sponsorship of event	March 2019